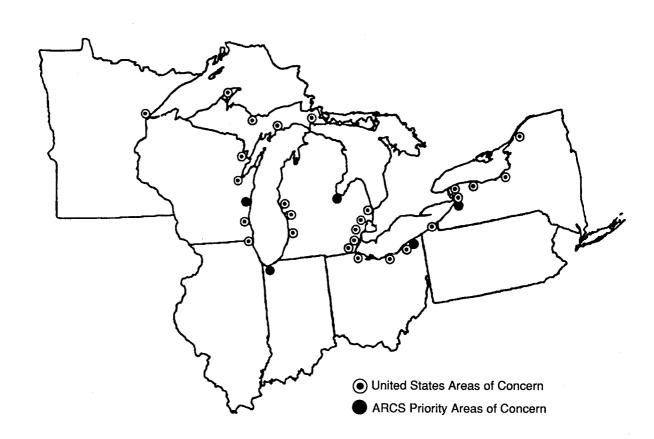
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# Assessment and Remediation Of Contaminated Sediments (ARCS) Program



PILOT-SCALE DEMONSTRATION OF THERMAL DESORPTION FOR THE TREATMENT OF BUFFALO RIVER SEDIMENTS



# Pilot-Scale Demonstration of Thermal Desorption for the Treatment of Buffalo River Sediments

Final Report

Prepared by

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For the

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# PILOT-SCALE DEMONSTRATION OF THERMAL DESORPTION FOR THE TREATMENT OF BUFFALO RIVER SEDIMENTS

### ABSTRACT

This report presents the results of a pilot scale demonstration to remediate contaminated sediments from the Buffalo River. A thermal desorption unit was evaluated for its effectiveness in remediating Buffalo River sediments contaminated with polycyclic aromatic hydrocarbons (PAHs). Sediments were processed at various water contents, thermal unit residence times, and temperatures to evaluate the effect of these process variables on treatment efficiency and materials handling. A portion of the residual solids from the thermal treatment process was mixed with various proportions of Portland cement to evaluate the ability of one solidification/stabilization process to bind metal contaminants.

With sediments remaining in the thermal desorption unit from 30 to 90 minutes and sediment temperatures reaching 300 to 480°F; 43.2 to 97.9 percent of total PAHs were removed while 9.1 to 100 percent of total PCBs (Aroclors 1248 and 1254) were removed. Although this thermal process had little effect on most metals, 16.7 to 100 percent of mercury was removed from sediments during processing. Removal rates for constituents of concern did not correlate well with treatment times or temperatures.

This paper has been reviewed in accordance with the U.S. Environmental Protection Agency's peer and administrative review policies and approved for presentation and publication.

### FINAL REPORT

# PILOT-SCALE DEMONSTRATION OF THERMAL DESORPTION FOR THE TREATMENT OF BUFFALO RIVER SEDIMENTS

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Sample Calculations

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### LIST OF ABBREVIATIONS AND SYMBOLS

**ABBREVIATIONS** amp ampere AOC Area of Concern Assessment and Remediation of Contaminated Sediments ARCS British Thermal Unit per hour BTU/hr CDF Confined Disposal Facility Dry Standard Cubic Meter DSCM Environmental Assessment EA **ETWG** Engineering Technology Work Group FONSI Finding of No Significant Impact Gram **GLNPO** Great Lakes National Program Office gallons per minute gpm high molecular weight HMW International Joint Commission IJC kilograms per hour kg/hr killowatt kw L liter lbs pounds pounds per hour lb/hr lbs/sq in pounds per square inch low molecular weight LMW min minute milligram mg ng nanogram ng/g nanogram per gram New York State Department of Environmental Conservation NYSDEC PAH polycyclic aromatic hydrocarbon PCB polychlorinated biphenyl parts per billion ppb parts per million ppm Resource Conservation and Recovery Act RCRA Remediation Technologies, Inc. RETEC SBLT sequential batch leach test scfm standard cubic feet per minute Toxicity Characteristic Leaching Procedure TCLP total organic carbon TOC Toxic Substances Control Act **TSCA** unconfined compressive strength USC microgram per gram ug/g microgram per liter ug/l United States Environmental Protection Agency USEPA um microgram v volt Waterways Experiment Station WES SYMBOLS chromium Cr Cu copper °F degrees Fahrenheit Hq mercury nitrogen gas  $N_2$ ક્ષ percent

zinc

correlation coefficient

- log {H<sup>+</sup>}

lead

Pb

Hq

r Zn

viii

### **DISCLAIMER**

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# PILOT-SCALE DEMONSTRATION OF THERMAL DESORPTION FOR THE TREATMENT OF BUFFALO RIVER SEDIMENTS

### 1.0 INTRODUCTION

The 1987 amendments to the Clean Water Act, Section 118(c)(3), authorized the United States Environmental Protection Agency's (USEPA) Great Lakes National Program Office (GLNPO) to conduct a 5-year study and demonstration project on the control and removal of toxic pollutants in the Great Lakes, with emphasis on the removal of toxic pollutants from bottom sediments (U.S. Environmental Protection Agency, 1990). The Great Lakes Water Quality Board of the International Joint Commission (IJC) identified 43 Areas of Concern (AOC) in the Great Lakes Basin where one or more of the objectives of the 1978 Great Lakes Water Quality Agreement and other jurisdictional standards, criteria, or guidelines are exceeded. GLNPO initiated the Assessment and Remediation of Contaminated Sediments (ARCS) Program to assess the nature and extent of bottom sediment contamination at the selected AOCs, evaluate and demonstrate remedial options, and provide guidance on the assessment of contaminated sediment problems and the selection and implementation of necessary remedial actions in the AOCs and other locations in the Great Lakes. The Buffalo River AOC, Buffalo, New York, was one area specified in the Clean Water Act as requiring priority consideration in locating and conducting on-site demonstration projects.

Past industrial and municipal discharges to the Buffalo River have polluted the river and its sediments. As a result, the river exhibits environmental degradation and impairment of beneficial uses of water and biota (New York State DEC, 1989). A pilot-scale demonstration was conducted in Buffalo, New York in the fall of 1991 to evaluate the ability of a thermal desorption process to remediate Buffalo River sediments contaminated with polynuclear aromatic hydrocarbons (PAHs).

### 1.1 OBJECTIVE

The objective of the Buffalo River pilot scale treatment technology demonstration was to evaluate thermal desorption as a treatment technology for sediments from the Buffalo River Area of Concern. Specific objectives of the pilot-scale demonstration included determining: the thermal desorption process' efficiencies in removing organic contaminants from sediments; the operating parameters that affect the removal efficiencies; the equipment necessary to achieve those removal efficiencies; the pretreatment handling and processing requirements of the sediments; and the characteristics of each of the process residual streams and the proper method of disposal for each residual. Another objective of the demonstration was to provide technology-specific information to be used in the development of

cost estimates for full scale remediation projects. In addition, a solidification process was evaluated by mixing treated sediments from the thermal desorption process with various proportions of cementitious material. The solidified blocks were sampled, and analyzed to determine the effectiveness of the solidification.

### 1.2 DESCRIPTION OF THE BUFFALO RIVER AREA OF CONCERN

### 1.2.1 Watershed Description

The watershed of Buffalo River and its tributaries, Cayuga, Buffalo, and Cazenovia creeks is located in the west central portion of New York State (Figure 1). The land area is roughly triangular in shape. Buffalo and Cayuga creeks originate in the Allegheny Plateau and flow northwest toward Lake Erie. Buffalo Creek rises near the town of Java and flows northwesterly to its confluence with Cayuga Creek in the town of West Seneca. The drainage area of Buffalo Creek is 150 square miles (New York State DEC, 1989). Cayuga Creek, with a drainage area of 128 square miles, rises near North Java Station and flows westerly through the northern part of the Buffalo River watershed. The confluence of Cayuga Creek and Buffalo Creek form the head of the Buffalo River.

Cazenovia Creek generally flows north from its head waters near Springville, New York to its confluence with the Buffalo River within the Buffalo, New York city limits. The drainage area of Cazenovia Creek is 138 square miles. From Cazenovia Creek, the Buffalo River flows westerly to its mouth at the eastern end of Lake Erie. Overall, the Buffalo River is 8.1 miles in length and its drainage area is approximately 446 square miles.

The Buffalo River and its sediments have been polluted by over 50 years of industrial and municipal discharge and disposal of waste. Fishing and quality of aquatic life within the Area of Concern (Figure 2) have been impaired by heavy metals and polycyclic aromatic hydrocarbons (PAHs) in sediments. wildlife habitat have been degraded by alterations to the river including modifications to the shoreline such as bulkheading. Levels of metals and cyanides in the sediment prevent open lake disposal of sediments dredged from the river. Other potential sources of pollution to the Buffalo River include inactive hazardous waste sites, combined sewer overflows, and other point and non-point sources of pollution. While the Buffalo River sediments are contaminated, they are not considered "toxic" or "hazardous" based on strict regulatory definitions, and are therefore not subject to the appropriate regulations of the Toxic Substances Control Act (TSCA) or the Resource Conservation and Recovery Act (RCRA).

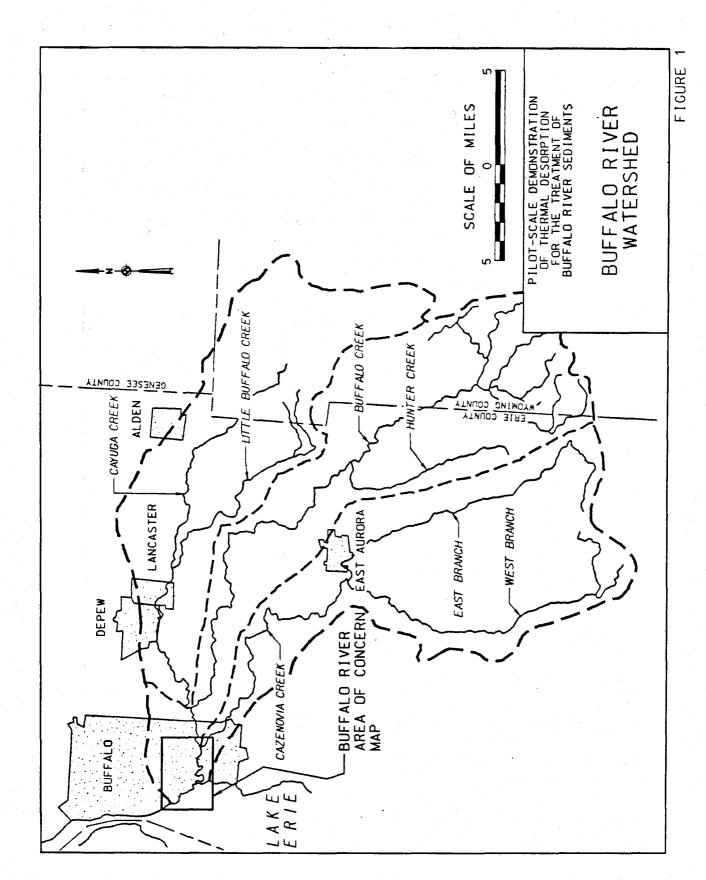


FIGURE 2

### 1.2.2 Status of Remedial Action Plan

New York State Department of Environmental Conservation (NYSDEC) and other Federal, State, and local agencies have and continue to carry out remediation of environmental problems along the Buffalo River. NYSDEC completed and issued the Buffalo River Remedial Action Plan (RAP) in November 1989. The RAP contained initial agency commitments to implement the remedial action strategy. To track implementation of the RAP, NYSDEC has issued annual reports to illustrate the progress on remediation by listing accomplishments of the past year and describing commitments for the current year.

To assist NYSDEC in the remediation process, a Remedial Advisory Committee (RAC) was formed in 1990. The RAC is representative of concerned groups within the community that have an interest in the Buffalo River. These groups include government officials, public interest groups, economic interests, and private citizens.

The following is a brief summary of RAC activities on the Buffalo River. A flow activated sampling station was established by NYSDEC to assist in stream water quality monitoring (New York State Department of Environmental Conservation, 1992). Event related sampling has been undertaken and will be continued into Sediment transport modeling is being conducted by the USEPA under the ARCS program. A dredging demonstration was conducted in 1992 by the Corps of Engineers to evaluate the efficiencies of several dredge types. Phase I investigations for all 36 inactive hazardous waste sites have been completed, while all but seven Phase II investigations have been completed. Remedial Investigation/Feasibility Studies (RI/FS) were completed for three sites in 1991-92, while two additional RI/FS's are underway. A combined sewer system model has been developed and verified for the main interceptors of the Buffalo Sewer Authority Operational simulations have been undertaken collection system. and cost estimates of alternatives for overflow reduction/treatment have been developed. A plan to assess fish and wildlife habitat conditions and improvement potential has been developed. Habitat assessment field work has been initiated by NYSDEC and will be completed in 1993.

### 1.2.3 Sediment Physical/Chemical Character

### 1.2.3.1 Sources of Sediments--

The major source of sediment in the Buffalo River is in runoff from the surrounding watershed. Depending on factors such as river velocities and discharge, channel topography, bank erosion and wind, much of the sediment originating in runoff is either deposited in the river channel bottom or is carried to areas further downstream. A large portion of this sediment accumulates in the Buffalo River Federal Navigation Channel.

### 1.2.3.2 Sediment Pollution--

The Buffalo River watershed is comprised of three major streams which converge at or along its mainstem: Cayuga, Buffalo, and Cazenovia creeks. Within the watershed major land usage is industrial and commercial, with some agricultural usage. Flows into the Buffalo River watershed originate in part from a variety of point and non-point source industrial activities in the watershed, including inactive hazardous waste sites and combined sewer outflows/municipal waste discharges (New York State D.E.C., 1989). These sources contribute to the bottom sediment contamination in the river. Polynuclear aromatic hydrocarbons and metals are contaminants of particular concern in Buffalo River sediments.

### 1.2.3.3 Sediment Characteristics and Quality--

Historic and recent sediment particle size analyses indicate that bottom sediments within the Buffalo River are comprised of silts and clays, with scme sands. Particle size and chemical (inorganic and organic) analyses and 96-hour acute toxicity tests (bioassays) were performed on surface grab samples obtained from the Buffalo River Federal Navigation Channel in 1989 (Aqua Tech Environmental Consultants, 1989). Particle size analysis of the sediment samples indicates they consist primarily of silts and clays (approximately 65 to 99 percent), with some sands (approximately 1 to 35 percent). Regarding inorganic sediment contamination, the results of bulk inorganic analysis performed under the 1989 program showed that most of the sediments were contaminated with elevated levels of numerous metals, including arsenic, barium, copper, iron, manganese, nickel, and zinc (Table The 1989 sediment testing program included analyses for volatile organics, PAHs and polychlorinated biphenyls (PCBs). Table 2 summarizes volatile organics data on sediments. Generally, volatile organics were not detected in sediments with the exception of low levels of 1,3-Dichlorobenzene and high levels of toluene on portions of the Buffalo River. PAH levels, shown in Table 3, ranged from non-detectable to about 2.4 micrograms per gram (ug/g) (benzo(b)fluoranthene). Total PAHs ranged from 5.44 to 12.15 ug/g. PCB and pesticide data summarized in Table 4 show non-detectable levels in the sediments.

The USEPA's Large Lakes Research Station of Grosse Ile, Michigan sampled sediments along the Buffalo River and Buffalo Ship Canal in 1989, 1990, and 1991 with a 4-inch diameter vibracore unit. Results from testing performed on samples collected outside the navigation channel in 1989 show concentration levels for 12 metals at 10 sites along the Buffalo River (Figure 3 and Table 5). Concentration levels for chromium (Cr) ranged from less than 13 ug/g to 312 ug/g while concentration levels for mercury (Hg) ranged from 0.0109 to 1.93 ug/g. Lead (Pb) concentrations ranged from 28 to 314 ug/g while zinc (Zn) concentrations ranged from 32 to 900 ug/g. In general, the highest concentration levels of metals were in the terminal end of the Buffalo Ship Canal and in the middle third reach of the Buffalo River. Test results

TABLE 1
INORGANIC ANALYSIS OF SURFACE SEDIMENT GRAB SAMPLES ug/g (dry)

Bulk inorganic analysis of surface sediment grab samples collected from Buffalo River, Erie County, New York. Sediment sampling areas are shown in Figure 4.

			Sediment	: Sampling Areas		
				Blue Tower		
Inorganic	Deadman's	Creek	Hamburg Street	Turning Basin	Mobil	oil
Parameter		·				
ARSENIC, TOTAL, AS	13	11	10	9	10	7
BARIUM, TOTAL, BA	90	84	. 79	91	78	81
CADMIUM, TOTAL, CD	0.5	1	1	0.6	1	<0.6
CHROMIUM, TOTAL, CR	18	13	13	9	2	. 4
COPPER, TOTAL, CU	49	46	48	40	35	35
IRON, TOTAL, FE	30300	29200	28400	30800	24300	20500
LEAD, TOTAL PB	82	66	62	55	60	25
MANGANESE, TOTAL, MN	490	490	460	480	520	530
MERCURY, TOTAL, HG	0.40	0.37	0.34	0.28	0.24	0.06
NICKEL, TOTAL, NI	31	30	29	32	25	. 22
RESIDUE, TOTAL (TS), %	48.7	53.4	55.2	50.6	57.0	40.3
SELENIUM, TOTAL, SE	, <b>&lt;1</b>	<2	<2	<2	<2	<2
SILVER, TOTAL, AG	<0.5	<0.5	<0.6	<0.6	<0.6	<0.6
SODIUM, TOTAL, NA	440	450	440	500	430	360
SPECIFIC GRAVITY	1.41	1.5	1.48	1.48	1.56	1.22
CARBON, TOTAL ORGANIC, C	1400	1200	1000	1200	1100	2200
ZINC, TOTAL, ZN	210	210	180	170	120	940

DATA SOURCE: Referenced Aqua Tech Report

TABLE 2

VOLATILE ORGANICS DATA FOR SURFACE SEDIMENT GRAB SAMPLES ug/g (dry)

Volatile Organics data on surface sediment grab samples

Volatile Organics data on surface sediment grab samples collected from Buffalo River, Erie County, New York. Sediment sampling areas are shown in Figure 4.

			Sedim	ent Sampling Areas		
				Blue Tower		
Volatile .	Deadma	n's Cr <del>e</del> ek	Hamburg Street	. Turning Basin	Mobil	Oil
Organic	<del></del>					
Acrolein	< 0.100	< 0.100	< 0.100	< 0.100	< 0.100	< 0.100
Acrylonitrile	< 0.100	< 0.100	< 0.100	< 0.100	< 0.100	< 0.100
Benzene	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Bromoform	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010
Carbon Tetrachloride	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Chlorobenzene	0.040	< 0.005	0.019	< 0.005	0.034	< 0.005
Chlorodibromomethane	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050
Chloroethane	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050
2-Chloroethyl Vinyl Ether	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010
Chloroform	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Dichlorobromomethane	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Dichlorodifluoromethane	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050
1,1-Dichloroethane	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010
1,2-Dichloroethane	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010
1,1-Dichloroethene	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010
1,2-Dichloropropane	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010
cis-1,3-Dichloropropene	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010
trans-1,2-Dichloropropene	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Ethyl Benzene	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Methyl Bromide	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Methyl Chloride	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Methylene Chloride	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050
1,1,2,2-Tetrachloroethane	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050
Tetrachloroethene	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Toluene	< 0.010	< 0.010	< 0.010	< 0.010	9.77	12.9
cis-1,2-Dichloroethene	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
trans-1,2-Dichloroethene	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
1,1,1-Trichloroethane	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
1,1,2-Trichloroethane	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Trichloroethene	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005
Trichlorofluoromethane	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020
Vinyl Chloride	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050
Total Xylenes	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010	< 0.010
1,3-Dichlorobenzene	0.249	0.374	0.048	0.383	0.263	< 0.005
Other Volatile						
Hydrocarbons *	3.52	2.65	1.41	1.83	4.09	4.28

<sup>\*</sup> Concentration estimate based on response of internal standard.

DATA SOURCE: Referenced Aqua Tech Report

TABLE 3 PAH DATA FOR SURFACE SEDIMENT GRAB SAMPLES

ug/g (dry)

PAH data on surface sediment grab samples collected from Buffalo River, Erie County, New York. Sediment sampling areas are shown in Figure 4.

			<u>Sedimer</u>	nt Sampling Areas	4	
				Blue Tower		
	Deadman	's Creek	Hamburg Street	Turning Basin	Mobil	Oil
PAH	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·				
Acenaphthene	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20
Acenaphthylene	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20
Anthracene	0.13	0.34	0.16	0.13	0.14	0.12
Benzo(a)Anthracene	0.58	0.93	0.51	0.45	0.46	0.39
Benzo(a)Pyrene	0.79	1.37	0.81	0.86	0.74	0.68
Benzo(b)fluoranthene	1.58	2.38	1.45	1.49	1.21	1.11
Benzo(ghi)Perylen <del>e</del>	<0.40	0.49	<0.40	<0.40	<0.40	<0.40
Benzo(k)fluoranthene	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20
Chrysene	0.73	0.98	0.57	0.63	0.52	0.43
Dibenzo(a,h)Anthracene	<0.40	<0.40	<0.40	<0.40	<0.40	<0.40
Fluoranthene	1.36	2.33	1.30	1.21	1.05	1.21
Fluorene	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30
Indeno(1,2,3-cd)Pyrene	0.44	0.61	0.41	<0.30	<0.30	<0.30
Naph tha Lene	<0.30	<0.30	<0.30	<0.30	<0.30	<0.30
Phenanthrene	0.58	1.34	0.59	0.59	0.60	0.78
Pyrene	0.83	1.38	0.72	0.76	0.83	0.72
Total PAHs	7.02	12.15	6.52	6.12	5.55	5.44

DATA SOURCE: Referenced Aqua Tech Report

TABLE 4 PESTICIDE AND PCB DATA FOR SURFACE SEDIMENT GRAB SAMPLES ug/g (dry)

Pesticide and PCB data on surface sediment grab samples collected from Buffalo River, Erie County, New York. Sediment sampling areas are shown in Figure 4.

			Sed filler	nt Sampling Areas	<del></del>	
			· · · · · · · · · · · · · · · · · · ·	Blue Tower		
Pesticides and	Deadman	's Creek	Hamburg Street	Turning Basin	Mobil	Oil
PCB						
Aldrin	<0.02	<0.02	<0.02	<0.02	<0.02	<0.02
alpha-BHC	<0.02	<0.02	<0.02	<0.02	<0.02	<0.02
beta-BHC	<0.02	<0.02	<0.02	<0.02	<0.02	<0.02
gamma-BHC	<0.02	<0.02	<0.02	<0.02	<0.02	<0.02
delta-BHC	<0.02	<0.02	<0.02	<0.02	<0.02	<0.02
Chlordane	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
4,41-DDD	<0.02	<0.02	<0.02	<0.02	<0.02	<0.02
4,4'-DDE	<0.03	<0.03	<0.03	<0.03	<0.03	<0.03
4,4'-DDT	<0.03	<0.03	<0.03	<0.03	<0.03	<0.03
Dieldrin	<0.02	<0.02	<0.02	<0.02	<0.02	<0.02
Endosulfan I	<0.03	<0.03	<0.03	<0.03	<0.03	<0.03
Endosulfan II	<0.03	<0.03	<0.03	<0.03	<0.03	<0.03
Endosulfan Sulfate	<0.03	<0.03	<0.03	<0.03	<0.03	<0.03
Endrin	<0.05	<0.05	<0.05	<0.05	<0.05	<0.05
Endrin Aldehyde	<0.05	<0.05	0.06	<0.05	<0.05	<0.05
Heptachlor	<0.03	<0.03	<0.03	<0.03	<0.03	<0.03
Heptachlor Epoxide	<0.03	<0.03	<0.03	<0.03	<0.03	0.05
Toxaphene	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
PCB-1016	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
PCB-1221	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
PCB-1232	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
PCB-1242	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
PCB-1248	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
PC8-1254	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10
PCB-1260	<0.10	<0.10	<0.10	<0.10	<0.10	<0.10

DATA SOURCE: Referenced Aqua Tech Report

FIGURE

TABLE 5

CONCENTRATIONS OF METALS IN TEN BUFFALO RIVER SEDIMENT SAMPLES (OCTOBER, 1989)

ug/g (dry) (except % Fe)

SAMPLING LOCATIONS ARE SHOWN IN FIGURE 3

Sample	Ag	As	PO	Cr	ng	%Fe	Hg	Mn	Ni	Pb	Se	uZ_
0101	97.0	34	4.0	312	148	5.5	1.93	1,386	57	286	3.8	006
0201	<0.03	<1.4	0.035	<13	8.2	0.33	0.019	40	5.2	28	<0.49	32
0301	0.44	13	1.4	113	<b>19</b>	4.4	0.624	685	45	107	<0.92	286
0401	0.22	12	1.0	17 1	20	4.2	0.186	190	20	<b>19</b>	<0.85	220
0501	0.16	<4.5	1.6	100	09	5.4	0.329	673	47	314	<1.0	371
0601, Rep 1 (a)	0.21	13	1.2	110	06	4.2	1.62	630	52	140	0.93	390
0601, Rep 2 (a)	0.24	12	1.2	130	93	4.2	1.76	630	97	150	<b>68.0</b>	390
0701	0.13	12	06.0	92	67	4.1	0.233	730	77	70	<0.86	200
0801	0.13	12	0.70	20	97	3.7	0.132	730	43	51	<0.88	170
1060	0.12	11	69.0	26	41	3.4	990.0	730	0.7	67	<b>60.84</b>	160
1001	0.12	8.2	0.57	94	35	3.0	0.082	260	34	43	<0.83	140

(a) Duplicate Samples Collected at Buffalo River Station 0601 DATA SOURCE: Environmental Protection Agency (Unpublished)

for 20 organic parameters (PAHs) analyzed at 9 of the 10 sampling sites are given in Table 6. Generally the highest concentration of PAHs were at sample site 0601 in the Buffalo River and 0101 at the terminal end of the Buffalo Ship Canal. Benzo(a)pyrene concentrations ranged from undetectable at 54 nanogram per gram (ng/g) to 2500 (ng/g) at sample site 0601.

In 1990 and 1991 sediment vibracore samples were collected by USEPA in the Buffalo River. Generally, approximately 1 to 3 meter core samples were taken and analyzed. Analytical results indicated that sediment contamination is either (1) relatively low and consistent with respect to depth, or (2) increases with respect to depth to a maximum level at which point a relatively clean, natural lacustrine clay layer is reached (U.S. Army Engineer District, Buffalo, 1992).

Areas sampled during the 1991 program are shown on Figure 4. Results of the 1991 sampling revealed that, in general, lightly to moderately polluted sediments overlay heavily polluted sediments as shown in concentrations of chromium, lead, zinc, and PAHs. Some of the core samples extended through the heavily polluted sediments into underlying moderately and lightly polluted sediments at core depths of roughly 3 to 4 meters. Many of the vibracore samples met refusal at a depth of 3 meters or less and did not appear to penetrate deep enough to extend through the heavily polluted sediments and into the underlying moderately and lightly polluted sediments.

### 2.0 DEMONSTRATION APPROACH

### 2.1 TECHNOLOGY SELECTION

A literature review of treatment technologies was performed for the ARCS Program by the Corps of Engineers Waterways Experiment Station (WES) and was used to screen process options for biological, chemical, extraction, immobilization, radiant energy, and thermal technologies (Averett, 1990b). Each process option was assessed on the basis of effectiveness, implementability, and cost. A number of the higher cost thermal processes were eliminated from consideration due to the expense of these processes while numerous other processes were eliminated from further consideration because of the lack of research and development for application to a specific sediment and associated contaminant matrix. The availability of a mobile pilot scale unit was essential for implementing an on-site pilot demonstration. Based on these criteria, a list of those processes that should be retained for demonstration consideration was developed.

A matrix was developed for the processes recommended for consideration for the pilot scale demonstrations, the principal contaminants treatable by each process, and the Areas of Concern

TABLE 6

CONCENTRATIONS OF POLYCYCLIC AROMATIC HYDROCARBONS IN TEN BUFFALO RIVER SEDIMENT SAMPLES (ng/g) SAMPLING LOCATIONS ARE SHOWN IN FIGURE 3

			7000	0401	0501	0601	0701	0801	0901	1001
Polycyclic Aromatic Hydrocarbons:								•		
Naphthalene	8600	) US7 (	a)	U35	140	830	150	U38	030°	(p)
2-methylnaphthalene	1000			U35	150	2200	U42	U38	U30	
Acenaphthylene	)/9			U37	U45	U45	045	040	U31	
Acenapthene	300		U50	U37	U45	750	045	040	U31	
Fluorene	77(			U37	300	3600	160	040	U31	
Phenanthrene	2600			300	2100	11000	750	370	380	
Anthracene	720			88	200	4500	260	96	<b>U35</b>	
Fluoranthene	3200		_	620	2100	2400	1100	610	840	
Pyrene	2600		_	760	1900	7100	1200	260	230	
Senzo(a)anthracene	1500			240	069	1900	520	210	220	
Chrysene	1700			320	980	2700	770	360	330	
Benzo(b)fluoranthene	3000			330	1100	1600	740	440	430	
Benzo(k)fluoranthene	000			340	970	1600	099	300	3.20	
Benzo(a)pyrene	2500			320	930	1300	069	280	310	
Indeno(1,2,3-c,d)pyrene	1600			U54	200	1000	270	090	160	
Dibenzo(a,h)anthracene	35(			U41	U50	020	020	U45	<b>U35</b>	
Benzo(g,h,i)perylene	1600			191	370	1100	290	U74	170	

 <sup>(</sup>a) - U57 Indicates a Sample Concentration Below the Detection Limit of 57 PPB
 (b) - Data Not Yet Available
 DATA SOURCE: Environmental Protection Agency (Unpublished)

F I GURE 4

where such contaminants are present and the processes are applicable (Averett, 1990a). A list of potential pilot projects was then prepared and these alternatives were ranked for consideration based on factors affecting their selection.

All five priority sites, Ashtabula River, Ohio; Buffalo River, New York; Grand Calumet River, Indiana; Saginaw River, Michigan; and Sheboygan Harbor, Wisconsin are contaminated by organic compounds. Most of these sites have areas of elevated contamination that could be used for a demonstration project. Rather than strictly following the numeric ranking of the potential pilot scale demonstrations, the ARCS Engineering/Technology Work Group (ETWG), responsible for recommending and implementing the demonstration, determined that a variety of the technology groups (biological, chemical, extraction, immobilization, thermal) should be selected for demonstration. With this in mind, thermal desorption, a technology suitable for treating materials contaminated with organics, was selected for a pilot scale demonstration to be conducted at the Buffalo River Area of Concern.

### 2.2 PLANNING DOCUMENT

Buffalo District initiated its planning for the pilot-scale demonstration in the fall of 1990. Coordination efforts associated with the demonstration involved meetings, correspondence, and telephone conversations with representatives of USEPA Region II, NYSDEC, members of the Buffalo River Remedial Action Committee, as well as the Corps of Engineers Regulatory personnel. A meeting was held with NYSDEC personnel in September 1990, while the October 1990 meeting of the ARCS ETWG was held at the NYSDEC Region 9 headquarters in Buffalo, New York. Topics discussed in these meetings included the thermal desorption technology, the scope and proposed location of the demonstration, anticipated treatment process residuals and their disposal and regulatory requirements. A document entitled" Work Plan for Pilot-Scale Demonstration for Remediation of Contaminated Sediments at the Buffalo River Area of Concern," was completed in February 1991. This report addressed sediment quality, description of the Buffalo River AOC, selection of the treatment technology, description of the demonstration, ranging from sediment removal and transport to residuals management and an estimate of all costs associated with the project. Also included was a description of activities associated with the demonstration ranging from regulatory and contractual requirements to monitoring requirements and report preparation. Members of the ETWG, including USEPA Region II, State and local representatives, were given the opportunity to review and comment on the document. Comments were reflected in the final document which was approved by the ETWG.

### 2.3 ENVIRONMENTAL ASSESSMENT

In early 1991, the Corps of Engineers Buffalo District initiated work on an Environmental Assessment (EA). assessment provided background information and addressed the environmental impacts and statutory compliance of the project. Social impacts were discussed as were the effects of the project on natural resources including air and water quality, aquatic and terrestrial habitat, and threatened and endangered species. brief description of the various environmental regulations and statutes applicable to the demonstration project and the degree to which the project was in compliance with those statutes and regulations was provided. Since no new dredged materials were to be discharged below Low Water Datum and given the small scope of the project, it was determined that the dredging of the sediments to be remediated fell within the limits specified under Section 10 of the Clean Water Act (Nationwide Permit No. 19) and complied with the provisions of Section 404(b) of the Clean Water Act. 404(b)(1) Evaluation was not necessary since the discharge of dredged material from the Buffalo Harbor into confined disposal facility No. 4 is covered under the 404(b)(1) Evaluation and Water Quality Certificate prepared for the construction of the disposal facility and any subsequent dredging connected with the facility. The project was also found to be in compliance with the River and Harbor Act of 1970, the Endangered Species Act of 1973, as amended, and numerous other applicable acts. With the dissemination and distribution of the EA and its associated Finding of No Significant Impact (FONSI) to numerous Federal, State, and local agencies and individuals, the project was found to be in full compliance with the National Environmental Policy The FONSI was completed and signed on August 19, 1991.

### 2.4 SCOPE OF WORK/CONTRACT

A scope of work was prepared for a pilot scale demonstration of the remediation of contaminated sediments at the Buffalo River Area of Concern utilizing thermal desorption. This scope of work provided background information, stated the objective of the demonstration, and provided a detailed description of the services required. The scope of work was made a part of the request for proposals that was provided to 36 interested firms responding to an announcement published in the Commerce Business The two proposals submitted in response to the request for proposals were reviewed by members of the ETWG to determine the prospective firms abilities to conduct the required services. The technical proposals were evaluated using a rating system based on the technical evaluation criteria developed by the ETWG and presented in the Commerce Business Daily announcement. Contract award was based on a firm's ability to meet the technical requirements of the testing involved, the company's qualifications and experience in conducting similar studies, the uniqueness and innovativeness of the technology in treating Great Lakes sediments, a comparison of cost estimates,

and the feasibility of conducting a full scale remediation project with the contractor's technology. After this evaluation was performed, a contract was awarded to Remediation Technologies, Inc. (RETEC) of Concord, Massachusetts.

### 2.5 SAMPLE LOCATION AND EXCAVATION

Based on available sediment sampling and analysis data obtained by the USEPA from 1989 and 1990 sampling operations, there were two areas of the Buffalo River Area of Concern where the sediments generally had higher concentrations of PAHs, than remaining portions of the river. These two areas were near the terminal end of the Buffalo Ship Canal and in an area of the upper portion of the Buffalo River Federal Navigation Channel. The contaminated sediments for the pilot scale demonstration came from the Buffalo River since this area had been sampled and tested in much more detail than the Buffalo Ship Canal, and, therefore it was anticipated that a sediment sample could be located and collected with greater assurance that it would contain significant concentrations of PAHs. It was desirable to treat more highly contaminated sediments during this demonstration since these are the sediments that are likely to be treated during any full scale remediation.

Sediments collected from the Buffalo River were used to evaluate the treatment technology rather than using sediments already deposited in the Corps of Engineers Confined Disposal Facility (CDF) No. 4 in Buffalo Harbor. Some of the PAHs contaminating the Buffalo River sediments are volatile and may escape the sediments when exposed to the atmosphere for significant lengths of time, or when they are rehandled several times, as sediments from the CDF would have been. Therefore, fresh sediments were collected for the pilot demonstration to ensure that significant amounts of the PAH contaminants did not volatilize prior to treatment.

The excavation of the contaminated sediments from the Buffalo River was accomplished by using floating plant consisting of a barge mounted crane and tug boat owned by Manson Construction Co. Inc. and under contract to the Corps of Engineers. An open clamshell bucket dredged approximately 15 cubic yards of sediments to be treated in the thermal desorption unit. Four to six feet of sediment was excavated in 10 to 12 feet of water at USEPA sample point 2501 and placed in four waste disposal bins (dumpsters) labeled "A" through "D" on the barge deck. Preliminary analytical results indicated that sediments at this location contained elevated levels of extractable residues from the surface of the sediments to 6 to 8 feet below the surface of the sediments.

### 2.6 SITE DESCRIPTION

While other sites along the Buffalo River were considered, the demonstration was conducted within the confines of Buffalo District's CDF No. 4 due to several advantages of this site over privately owned or public lands that may have been available within the Area of Concern. Issues of liability and access were greatly simplified since the facility is owned by the Corps of Engineers. In addition, regulatory requirements had already been satisfied for using this facility to confine contaminated dredged sediments. The CDF had been designed and constructed in the mid 1970s to contain polluted sediments dredged from the Buffalo River and Buffalo Harbor. Community concerns would be eased if the demonstration were conducted within CDF No. 4 since it is located in an area removed from any housing or public access. Finally, the remoteness of the area minimized security problems.

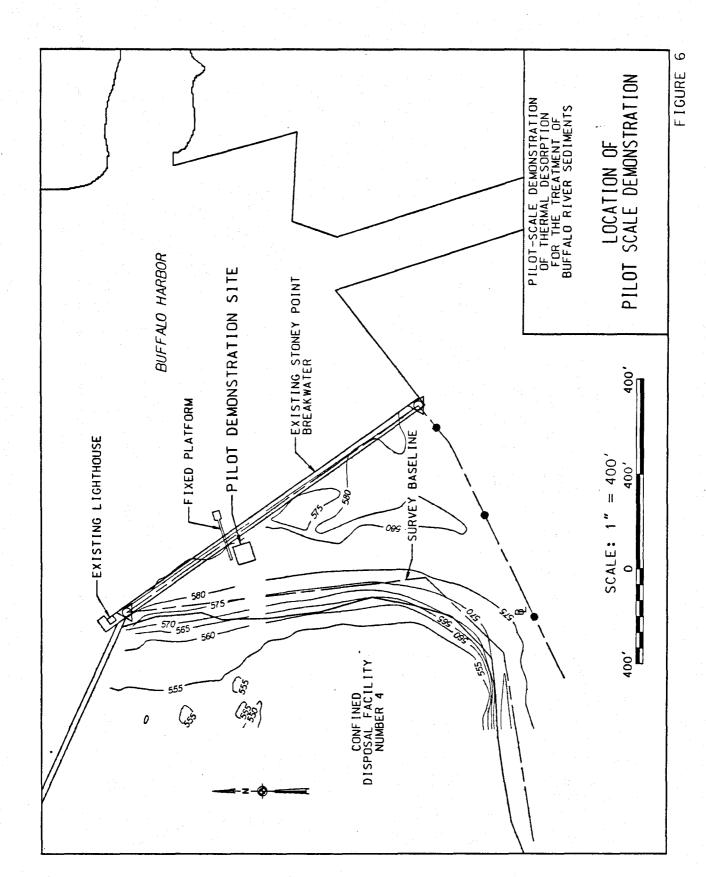
Excavated sediments were transported by barge to CDF No. 4 (Figure 5). Contamination of the surrounding water bodies due to spillage was controlled by avoiding overloading the waste bins with sediment material. Transfer of the bins from the barge to the CDF was accomplished through the use of the barge mounted crane. The floating plant was secured in Buffalo Harbor, adjacent to the CDF, while the waste bins containing the dredged sediments were off-loaded onto Stoney Point Breakwater, the eastern boundary of the disposal facility (Figure 6).

CDF No. 4 is located at the southern end of the Buffalo Harbor, adjacent to the Bethlehem Steel Corporation's Lackawanna plant. Access to the CDF is available though the Bethlehem Steel plant. The pilot scale demonstration took place along the east side of the disposal facility, adjacent to the Stoney Point Breakwater (Figure 6). An existing access road along this portion of the dike was capable of carrying vehicular traffic, including tractor trailers loaded with demonstration equipment. Several acres were available within the disposal facility upon which the demonstration could be conducted. This included an area of 2 to 3 acres adjacent to the roughly 300-foot long pumpout pipe. This area was generally clear of trees and shrubs and was relatively level, though it did contain approximately 1 to 3 foot undulations in the surface contours.

### 2.6.1 Site Preparation

Prior to their mobile pilot scale unit arriving on site, Remediation Technologies, Inc. (RETEC) prepared the site. An area of roughly 10,000 square feet was cleared and prepared for the mobile thermal processor and support equipment which included: chiller, electric generator, water tank, inert gas tank (Nitrogen gas), office trailer, storage trailer, publicity tent, and drum storage area (Figure 7). Sufficient area was also available to provide parking for several vehicles. The demonstration area was constructed using a bulldozer to remove the surficial soils and stockpile them along

FIGURE 9



the western edge of the site. Approximately 300 tons of slag was applied to the cleared area to provide a firm working surface and improve water drainage. The slag material, purchased by Remediation Technologies, Inc. from the adjacent Bethlehem Steel plant, was spread with a bulldozer and compacted with a vibratory roller. RETEC performed site preparation and mobilized the pilot scale thermal desorption processor and support equipment to the site from October 7 through October 18, 1991.

### 2.7 MATERIAL HANDLING

### 2.7.1 Transport

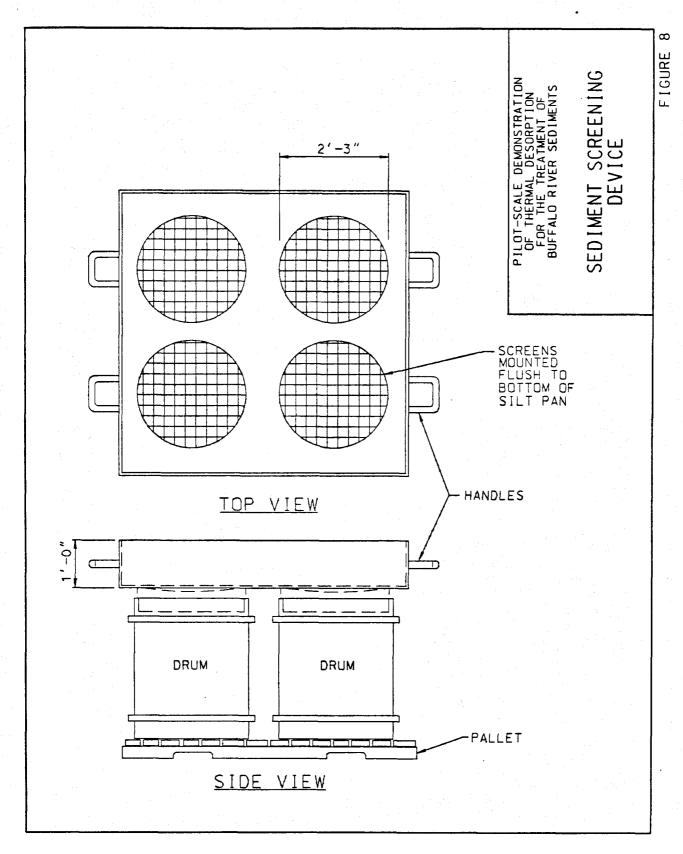
The dredged sediments were placed into four dumpsters aboard the floating plant and transported to CDF No. 4 by Manson Construction Co. on October 7, 1991. Approximately 4 cubic yards of sediments were placed in each of four bins labeled "A" through "D" in order to track the sediments during the treatability study. Transfer of the dumpsters from the deck of the floating plant to CDF No. 4 was accomplished through the use of Manson's barge mounted crane. At this point, the sediments were turned over to the remediation contractor, RETEC, for pretreatment and treatment operations.

### 2.7.2 Screening

Prior to pilot scale treatment of the excavated sediment using the thermal desorption technology, it was necessary to remove particles and debris greater than 0.75 inches in size from the feed sediments. RETEC fabricated a sediment screening device which provided the capability of simultaneously filling four 55-gallon drums (Figure 8). The device covered an area 16 square feet in size and had four holes cut into it, each the size of a 55-gallon drum. An inflexible wire mesh was welded to each hole to screen objects greater than 0.75 inches in size. The screening device had 1 foot high walls and was capable of holding several cubic feet of material, the equivalent of a small backhoe bucket.

A backhoe was used to remove approximately 12 cubic yards of the sediments from the four dumpsters and place it in the screening device. Three cubic yards of sediment that could not be removed by backhoe were later removed by hand and disposed of in the CDF. The screening device was designed to allow undersized material to pass the wire mesh and fall into the 55-gallon drums by gravity. However, the cohesive nature of the sediments dredged from the Buffalo River for this demonstration prevented the material from passing through the screen by gravity. RETEC personnel then tried to use shovels to force the sediments through the screen with little success. They then used a backhoe bucket to force the sediments through the screen. This approach turned out to be time consuming and extremely inefficient. Screening by hand was the most efficient means found to screen the oversized material





from the sediments during the demonstration project. Each backhoe bucket full of sediments was handled by RETEC personnel outfitted in protective tyvek suits and gloves. Oversized material screened from the sediments consisted mostly of gravel and tree branches and amounted to well under 1 percent (by weight and volume) of the screened sediments. Oversized material was disposed of within the confined disposal facility while the screened material was stored in covered 55-gallon drums prior to being treated using the RETEC thermal desorption process.

### 2.7.3 Storage

The 12 cubic yards of screened sediments were stored in 48 covered 55-gallon drums from the time they were screened, October 8 and 9, until the sediment was treated in the thermal desorption unit, between October 21 and November 25, 1991. Approximately 3 cubic yards of sediment were screened from each of the four bins (labeled A thru D) into twelve 55-gallon drums. The twelve drums from each bin of sediment were split into three groups of four drums each and labeled A1 (four drums), A2, A3, B1, B2, B3, C1, C2, C3, D1, D2, and D3.

### 2.7.4 Addition of Water

Just prior to feeding the sediments for a particular run into the thermal unit, RETEC personnel mixed water with the four drums of sediment to be treated. The water content of the dredged sediments was relatively consistent, ranging from 40 to 45 percent. A relatively small amount of water, 2 to 3 percent, was added to the sediments from bin "A" in order to assist the feed operations by increasing the "pumpability" of the feed material. The water was added to each 55-gallon drum of sediment while the sediments were being mixed with an electric powered paddle mixer. The water content of the sediments from bins "B," "C," and "D" were similarly adjusted to approximately 45, 50, and 60 percent, respectively.

### 2.7.5 Feed Operations

The normal material handling system for the thermal desorption unit was a bucket conveyor designed for bulk solid material, which appeared ineffective for feeding the high moisture, cohesive sediments dredged for the pilot scale demonstration. The contractor, RETEC, based this judgment on a simple field test, whether or not the sediments stuck to a spoon when the spoon was inverted. The Buffalo River sediments remained stuck to the spoon and, therefore, feeding the material into the thermal unit with the bucket conveyor was not attempted. For this demonstration, the sediments were fed into the processor by means of a diesel-powered peristaltic pump. The peristaltic pump was designed to provide a continuous and steady delivery of material to the thermal unit. The manufacturer described the pump as capable of processing up to 80 percent solids and particle sizes up to 0.75 inches in size. It was rated to have a

maximum delivery rate of 110 gallons per minute at a suction head of 29 feet. Initial project delays were encountered while waiting for site delivery of the pump from the manufacturer and in defining the proper material of construction for the peristaltic hose. A natural rubber material was finally selected on the basis of its resiliency. RETEC found the pump unsuccessful in pumping the screened sediments until a small amount of water was added as described above. Sediments were pumped into the thermal system just below the slide gate (air lock) on the processor to minimize infiltration of ambient air into the processing chamber.

### 2.8 THERMAL DESORPTION

Thermal desorption refers to the separation of contaminants from a solid matrix by heating to volatilize organic contaminants. The desorption process can be used in conjunction with separate processes, such as incineration, condensation, or adsorption, for subsequent control of the volatilized constituents. According to Remediation Technologies, Inc. the fact that, for some contaminants, efficient removals can be achieved at relatively low treatment temperatures makes thermal desorption a less costly approach than incineration for the remediation of solids contaminated with organic constituents. The desorption process is not effective in treating materials contaminated with inorganic contaminants.

The desorption process can be accomplished using various types of direct or indirect fired equipment. Applications using indirectly-fired methods are preferred in many cases since they generate a significantly smaller volume of off-gas than traditional drying or incineration systems. As a result, the capital and operating costs for the system can be significantly reduced.

### 2.8.1 System Description

Remediation Technologies, Inc. has developed a thermal desorption technology that reportedly has demonstrated applications as both a pre-treatment operation (dewatering, removal of volatile constituents) and final treatment operations for waste water treatment sludges from petroleum refineries as well as soils contaminated with organics (Remediation Technologies, Inc., 1992). RETEC's application of the technology relies on condensation to capture most of the organics volatilized by the thermal processor. Volatilized organics are condensed into a concentrated liquid stream which can subsequently be managed either on-site using further treatment systems or off-site at a permitted treatment/storage/disposal facility. The benefits of the system include lower capital costs relative to traditional thermal technologies, and permitting requirements that are less stringent than for incineration systems.

RETEC's system is based upon the use of an established, indirectly-heated thermal desorption/dryer system, the Holo-Flite Screw Processor, manufactured by the Denver Equipment Company, Colorado Springs, Colorado. The Holo-Flite processor is an indirect-heat exchanger commonly used to heat, cool, and dry bulk solids and slurries. The treatment system consists of a jacketed trough which houses a heated double-screw mechanism. The rotation of the screws promotes the forward movement of the material through the processor. The rotating augers are arranged in the trough so that the flights of the two screws mesh, facilitating the movement of material and improving the heat transfer.

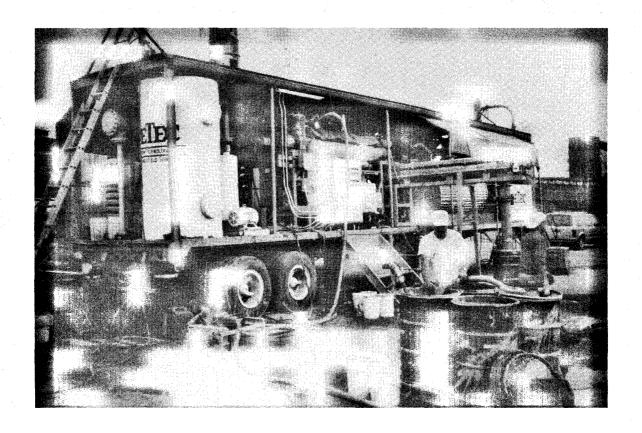
The RETEC processor uses a contained, non-contact circulating heat transfer media to elevate the temperature of the solids. The heated media continuously circulates through the hollow flights of the screw augers, travels the full length of the screws, and returns through the center of each shaft to the heater. The heat transfer fluid is also circulated through the trough jacket to provide additional heat transfer surfaces for improved volatilization. RETEC's system employs a unique heat transfer medium, a molten salt eutectic consisting of 53 percent potassium nitrate, 40 percent sodium nitrite, and 7 percent sodium nitrate. The use of this media provides the ability to achieve processing temperatures up to 850°F to effect appropriate removals of heavier organic species and increase the efficiency of the system in treating more complex solid matrices. addition to the enhanced thermal properties, the salt eutectic provides significant safety benefits; the salt melt is noncombustible, it provides no risk of explosion, and potential vapors are non-toxic (Remediation Technologies, Inc., 1992). inert atmosphere was maintained in the thermal treatment chamber through the controlled introduction of nitrogen gas to ensure that oxidation of the volatilized material did not occur.

Remediation Technologies, Inc. utilized its transportable demonstration system for the performance of this project (Figure 8A). The system, contained on a single 8-foot by 45-foot flat bed trailer, consisted of material feed equipment, thermal processor, indirect condensing system, and an activated carbon unit for the control of volatile organic constituents. A process flow diagram for this pilot scale system is shown in Figure 9. The design of the demonstration unit utilizes manual general control systems that are not equipped with feed interlocks.

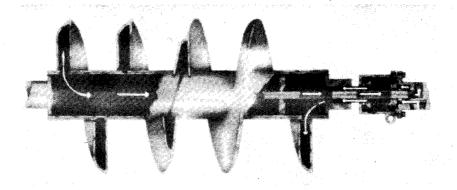
### 2.8.1.1 Material Handling--

Generally, material to be processed by RETEC in their thermal desorption system is placed in a live bottom feed storage hopper with a 1.5 cubic yard capacity. The material is sized and conveyed to a bucket elevator using twin 6-inch diameter screws equipped with ribbon flights. The bucket elevator raises the material to a height of 17 feet to a feed auger which uses a single 6-inch ribbon flight screw to convey the material to the processor via a double slide gate (air lock). The slide gate is to prevent the leakage of ambient air into the processor.

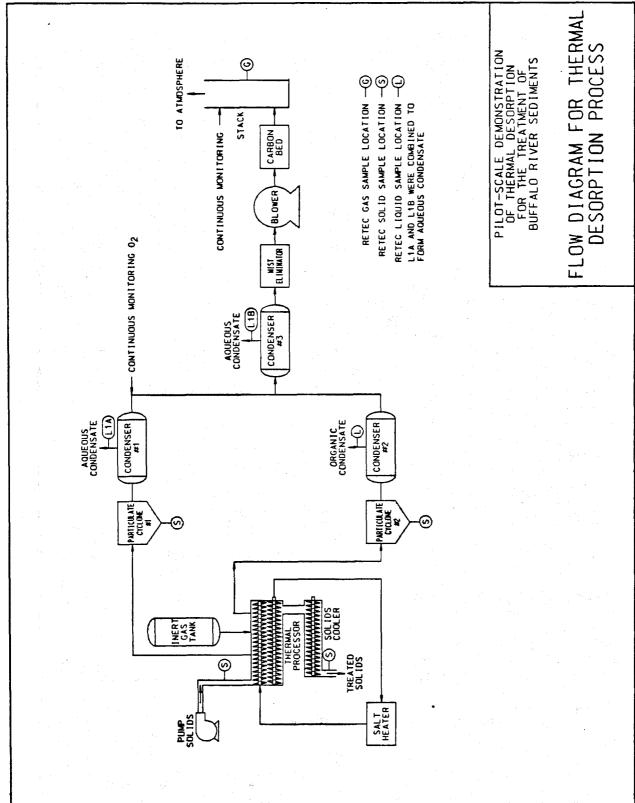
Figure 8A: Thermal desorption unit and screw processor



Thermal desorption unit at Buffalo River pilot demonstration site



Holo-flite screw processor



As stated previously, due to the cohesive nature of the Buffalo River sediments, a diesel powered peristaltic pump was used to deliver the screened Buffalo River sediments to the thermal processor during this demonstration project. The pump consisted of a 5 horsepower air cooled diesel engine attached to a high capacity peristaltic pump head. The flow rate of the pump was rated at 110 gallons per minute maximum. During this demonstration, the sediments were drawn through the pump at an average feed rate of 1 gallon per minute. A 2-inch diameter hose was used to draw the feed material from the 55 gallon drums and deliver them to the thermal processor. The pump discharge line was connected to the processor after the double slide gates (air lock).

### 2.8.1.2 Thermal Processor--

The Holo-Flite thermal processor contained two 7-inch intermeshing screw conveyors and had the nominal capacity to treat 0.5 tons per hour of material (Figure 8A). The system was operated at media temperatures and solids residence times that allowed the solids to achieve temperatures in the range of 300 to 540°F. At these temperatures, organic constituents and moisture present in the waste material were volatilized and drawn away under negative pressure to the off-gas control system. Solids residence times in the processor were varied from 30 to 90 minutes through the use of a variable speed drive for the rotating augers.

The atmosphere in the treatment chamber was controlled during all treatment activities. The pressure inside the processor was maintained at -0.1 to -0.5 inches of water column and an "inert" atmosphere was maintained in the treatment chamber through the controlled introduction of nitrogen. RETEC used a commercially provided tank as the source of inert gas. The nitrogen ( $N_2$ ) gas was delivered to the processor at a flow rate of 5 to 30 cubic feet per minute. The oxygen content of the gas stream was monitored continuously during the operation of the treatment system to ensure that oxidation of the volatilized materials would not occur. Oxygen levels were consistently maintained below 17.5 percent.

Treated solids were fed by gravity to a second process auger designed to cool the solids prior to exiting the desorption unit. The "cooling screw" was also of the Holo-Flite design and used a single auger with chilled water as the cooling media. The cooling screw required approximately 12 gallons per minute (gpm) of water less than 90°F to cool the treated solids to a temperature of approximately 140°F. The temperature of the water was maintained using a closed-loop chiller system. The treated solids were discharged from the cooler through a rotary air lock into 55-gallon drums.

### 2.8.1.3 Media Heater--

The salt eutectic was stored and heated in an enclosed, insulated stainless steel vessel having a capacity of approximately 600 gallons. The eutectic was heated electrically using 27 immersion heaters capable of providing one million BTU per hour of heating capacity to the unit and media temperatures of approximately 1,000°F. The heat medium was delivered to the thermal processor by means of a vertical pump with a submersible head. The pump had the capability to deliver up to 50 gpm of molten salt eutectic to the processor.

### 2.8.1.4 Off-Gas Control--

The off-gas control system was designed to accommodate an off-gas flow rate of approximately 150 standard cubic feet per minute (scfm) and a "worst case" moisture and organic loading of 400 pounds per hour and 150 pounds per hour, respectively. particulate cyclones were used to remove any fine solid particles (greater than 10 microns) which may have been entrained with the off-gases. These solids were removed on a daily basis and combined with the treated solids for subsequent disposal. indirect heat exchangers, having a combined surface area of 200 square feet, were used to reduce the temperature of the gas leaving the processor to approximately 120°F and condense the majority of the entrained moisture and organics. An after cooler, condenser number 3, was placed in line to remove the remaining moisture and volatile organics from the off-gas stream (Figure 8). The exchanger was designed to achieve an exit gas temperature of 50°F. Cooling water was recirculated in a closed loop through a chiller having a capacity of 240,000 BTU per hour. Condensates were collected in two separate vessels prior to transfer from the system. The system was driven by a variable speed rotary blower capable of developing 300 scfm of flow at a vacuum of 3 inches of mercury.

The thermal system was equipped with an activated carbon system to control noncondensible organics prior to release to the atmosphere. The carbon system was charged with 1,500 pounds of carbon (Remediation Technologies, Inc., 1992). Volatile organic emissions from the system were monitored in the stack on a continuous basis .

### 2.8.2 Pilot Scale Demonstration

Sediments from bins A and B were treated on-site in Buffalo, New York from October 21 through 31, 1991. Due to freezing temperatures and heavy snowfall in early November, the thermal desorption unit and its support equipment were transferred to RETEC's treatability laboratory in Acton, Massachusetts. Sediments from bins C and D were treated with the unit set up at this facility from November 18 through 25, 1991.

Remediation Technologies, Inc. monitored all pertinent process parameters at routine intervals during the demonstration. This approach was used to help optimize the removal efficiency of the thermal desorption demonstration unit as well as to develop data for the design of full scale equipment. The data collected included material feed rate, revolutions per minute of the thermal processor augers, temperature of the heat transfer media entering and exiting the processor, residence time of the solid in the processor, temperature of solids entering and exiting the thermal processor, flow rate of the carrier gas, inlet temperature of the carrier gas, off-gas temperature, and mass rates of all process streams. Off-gas concentrations of oxygen and hydrocarbons were monitored continuously while other data was recorded at approximately 30 minute intervals during operation of the unit.

Process temperatures were monitored at 21 locations using thermocouples. Temperature signals were transmitted to a panel readout and subsequently recorded on field data sheets (Remediation Technologies, Inc., 1992). Gas pressures were monitored in the processing system using magnahelic gauges. Pressures were monitored within the headspace of the processor and across the principal components of the off-gas system to ensure proper operation of the system and to help anticipate maintenance problems such as poor heat transfer. The flow rate of inert gas into the processor was monitored by a standard flow meter while the off-gas flow rate from the thermal system was monitored in the off-gas stack by measuring the flow with a hot wire anemometer. The sediment feed rate to the processor was monitored by recording the volumetric displacement of the feed system per unit of time in conjunction with associated measurements of the density of the feed material. The accuracy of these observations was validated in the field using notations of the speed and capacities of the processing and cooling augers.

Upon review of the data RETEC determined that there was significant variability in both the pumping rate and density of feed material. Therefore, the average material feed rates were calculated by dividing the total mass of feed material for each test (weighted in the field) by the duration of time that material was fed into the processor.

### 2.8.2.1 Sediment A--

Sediment from bin A was treated in the thermal desorption unit from October 21 thru October 24, 1991. The material was processed after mixing with a small amount of Buffalo Harbor water (2% to 3%) to improve the "pumpability" of the material. The feed rate and residence time were varied for the feed material designated A1, A2, and A3. Tables 7A and 7B present the process data for each treatment run as recorded by RETEC. Sediment from the three runs, A1, A2, and A3, was treated at feed rates ranging from 346 to 716 pounds per hour (wet weight) and residence times ranging from 30 to 90 minutes. The process temperatures ranged from 933°F to 938°F for the heat transfer media entering the processor, 902°F to 911°F for the heat transfer fluid leaving the processor, and 380°F to 535°F for the treated solids exiting the processor.

TABLE 7A
PROCESS PARAMETER VALUES AS MEASURED BY RETEC, INC.
(English Units)

A2	A3	81	85	83	5	23	63	10	D2	03
10/21 10/23	10/24	10/25	10/30	10/31	11/18	11/19	11/20	11/21		11/25
09 06	30	45	8	8	8	99	45	8	99	45
346 502	716	860	777	334	787	635	862	388		724
938 937	933	937	296	951	921	832	834	888	872	198
911 905	905	806	929	920	881	804	802	853	843	824
09 09	8	8	9	99	9	99	09	9	9	9
535 480	380	300	362	344	392	415	7.27	367	423	303
917 950	860	530	929	756	854	7/6	006	226	965	975
367,390 435,420	421,820	421,820	449,030	421,800	554,280	381,000	435,000	476,250	394,600	503,460
m = 5 to 5 = 5	937 905 60 480 950 950	937 905 60 480 950 435,420	937 933 905 902 60 60 480 380 950 860 435,420 421,820	937     933     937       905     902     908       60     60     60       480     380     300       950     860     230       435,420     421,820     421,820	937     933     937     962       905     902     908     929       60     60     60     60       480     380     300     362       950     860     230     656       435,420     421,820     421,820     449,030	937         933         937         962         951           905         902         908         929         920           60         60         60         60         60           480         380         300         362         344           950         860         230         656         756           435,420         421,820         449,030         421,800	937         933         937         962         951         921           905         902         908         929         920         881           60         60         60         60         60         60           480         380         300         362         344         392           950         860         230         656         756         854           435,420         421,820         449,030         421,800         554,280	937         933         937         962         951         921         832           905         902         908         929         920         881         804           60         60         60         60         60         60         60           480         380         300         362         344         392         415           950         860         230         656         756         854         974           435,420         421,820         449,030         421,800         554,280         381,000	937         933         937         962         951         921         832         834           905         902         908         929         920         881         804         802           60         60         60         60         60         60         60         60           480         380         30         362         344         392         415         474           950         860         230         656         756         854         974         900           435,420         421,820         421,820         421,800         554,280         381,000         435,000	937         933         937         962         951         921         832         834         888           905         902         908         929         920         881         804         802         853           60         60         60         60         60         60         60         60         60           480         380         360         362         344         392         415         474         367           950         860         230         656         756         854         974         900         977           435,420         421,820         421,800         554,280         381,000         435,000         476,250

TABLE 78
PROCESS PARAMETER VALUES AS MEASURED BY RETEC, INC.
(SI Units)

					Run			i				
PARAMETER	A1	42	A3	81	82	83	13	C2	C3	10	02	03
Date (1991)	10/21	10/23	10/24	10/25	10/30	10/31	11/18	11/19	11/20	11/21	11/22	11/25
Residence Time (min)	8	99	30	45	9	8	. 8	9	45	8	9	45
Feed Rate (kg/hr)*	157	228	325	390	292	151	220	288	391	176	261	328
Temperatures (°C)*												
Heat Transfer Media In	503	203	501	205	517	511	767	577	977	925	767	461
Heat Transfer Media Out	488	485	483	787	867	493	7.15	625	428	456	451	077
Sediment In	16	16	16	9	16	9	16	4	16	16	16	91
Sediment Out	279	549	193	149	183	173	200	213	546	186	217	151
Inert Off-Gas	765	510	760	110	347	705	457	523	785	525	518	524

<sup>\*</sup> These data are converted from English Units and are rounded to the nearest whole number. DATA SOURCE: Referenced RETEC, Inc. Report

Some operational problems were encountered during the processing of the sediment. Initial feed to the unit was erratic due to RETEC's unfamiliarity with the peristaltic pump and because the pump was delivered from the manufacturer with a peristaltic hose that was not compatible with the sediment material (Remediation Technologies, Inc., 1992). A consistent flow was established once the pump hose was changed from a high density polyethylene to a natural rubber material. In addition, some fouling of the processor was encountered between the processing of samples A2 and A3. RETEC reported that the fouling was the result of caking of dried sediments around the processing augers. The processor was partially disassembled and the caked solids were manually removed from around the augers. The buildup of dried material was thought to have been due to the cohesive nature of the fine grained sediments fed into the processor.

### 2.8.2.2 Sediment B--

Material from bin B was treated in the thermal desorption unit from October 25 thru October 31, 1991. The sediment was processed after mixing with Buffalo Harbor water to achieve a target moisture content of 45 percent prior to treatment. The feed rate and residence time were varied for the feed material designated B1, B2, and B3. Tables 7A and 7B present the process data for each treatment run as recorded by RETEC. Sediment from the three runs, designated B1, B2, and B3, was treated at feed rates ranging from 334 to 860 pounds per hour (wet weight) and process residence times ranging from 45 to 90 minutes. The process temperatures ranged from 937°F to 962°F for the heat transfer media entering the processor, 908°F to 929°F for the heat transfer fluid leaving the processor, and 300°F to 362°F for treated solids exiting the processor, as measured by RETEC personnel.

As in the case of the treatment of sediment from bin A, there was a significant buildup of dried material in the thermal processor. While treating sediment sample B3 the buildup became so severe that the processing augers could no longer rotate and a shear pin on the auger system broke. The thermal system was disassembled, the caked solids were manually cleaned out, and the shear pin was replaced.

### 2.8.2.3 Sediment C--

On November 3 and 4, 1991 a snow storm left approximately 1 foot of snow covering the project area and the air temperature dropped to between 25 and 30°F. The unprocessed Buffalo River sediments from bins C and D as well as hydraulic lines on the thermal desorption unit froze. This made it impossible to operate the thermal desorption unit or to feed the sediments through the peristaltic pump into the processor until warmer temperatures returned. Rather than waiting for warmer temperatures to return, the Corps of Engineers and Remediation Technologies, Inc. agreed that the pilot scale demonstration should be completed at RETEC's indoor treatability facility in

Acton, Massachusetts. During the weeks of November 4 and November 11, 1991, RETEC personnel demobilized the pilot scale unit and set the unit up in their Acton facility. They also transported the untreated sediments from bins C and D from Buffalo, New York to Acton, Massachusetts.

Sediments from bin C were processed through the thermal desorption unit on November 18, 19, and 20, 1991. Tap water was mixed with the sediments to achieve a target moisture content of approximately 50 percent prior to treatment. The feed rate and residence time of the sediment in the thermal unit were varied for the material designated as C1, C2, and C3. Tables 7A and 7B present the processed data for each treatment run as recorded by RETEC. Sediment from the three runs, C1, C2, and C3, was treated at feed rates ranging from 484 to 862 pounds per hour (wet weight) and process residence times ranging from 45 to 90 minutes. The process temperatures ranged from 832°F to 921°F for the heat transfer media entering the processor, 802°F to 881°F for the heat transfer fluid leaving the processor and 392°F to 474°F for treated solids exiting the processor.

### 2.8.2.4 Sediment D--

Sediment from bin D was treated in the thermal unit November 21, 22, and 25, 1991 in Acton, Massachusetts. Tap water was mixed with the sediments to achieve a moisture content of approximately 60 percent prior to treatment. The feed rate and residence time of the sediment in the thermal unit were varied for the process runs using sediment samples D1, D2, and D3. Tables 7A and 7B present the process data for each treatment run as recorded by RETEC. Sediment from the three runs was treated at feed rates ranging from 388 to 724 pounds per hour (wet weight). Process temperatures ranged from 861°F to 888°F for the heat transfer media entering the unit, 824°F to 853°F for the heat transfer fluid leaving the processor, and 303°F to 423°F for the treated solids exiting the processor.

#### 2.9 RESIDUALS MANAGEMENT

Most of the residuals from the pilot scale demonstration were disposed of by Remediation Technologies, Inc. While operating in Buffalo, New York, residual solids and liquids from the bin A and B treated sediments were collected in 55-gallon drums. Treated solids from the sediment A1 run were disposed within the Corps Confined Disposal Facility. The remaining treated solids, including the cyclone material, were used in a solidification/stabilization demonstration. RETEC sealed the organic condensate in 55-gallon drums and transported it to Acton, Massachusetts for proper disposal when the thermal unit was demobilized from Buffalo, New York. The aqueous condensate was emptied from the 55-gallon drums into the confines of Confined Disposal Facility Number 4.

All residuals from the treatment of sediments from bins C and D, as well as the organic condensate from the A and B process runs performed in Buffalo, were disposed of by RETEC at a licensed disposal facility in the New England region.

### 2.10 SOLIDIFICATION OF SOLID RESIDUE

A portion of the residual solids from the treatment process were solidified/stabilized. The solidification/stabilization technology immobilizes certain contaminants by binding them into a concrete-like, leach resistant mass. The formation of the solidified product is achieved during a hydration reaction in which free water is bound to the setting agent. The physical and chemical stability of the resulting product are functions of the sediment/residual characteristics, type of setting agent, and additives used. Cement processes reduce the mobility of heavy metals due to their conversion to insoluble hydroxides or carbonates because of the elevated pH of cement.

Under the ARCS Program, the Corps of Engineers evaluated solidification/stabilization at bench-scale for potential treatment of contaminated sediments from the Buffalo River. The evaluation was conducted to determine whether physical and chemical properties of the sediment would be improved. Results are reported in "An Evaluation of Solidification/Stabilization Technology for Buffalo River Sediments" (Fleming, Averett, Chennell, Perry, 1991) and are summarized here. Based on analyses of the untreated sediment, five metals were selected for evaluation: chromium, copper, lead, nickel, and zinc.

Initial screening tests for the laboratory were conducted on the sediment to narrow the range of binder-to-soil ratios to be prepared in the detailed evaluation. Three binder materials were evaluated: cement, kiln dust, and lime/fly ash. Based on the results of the initial screening tests, binder-to-soil ratios were selected for the detailed evaluation. Specimens were prepared by mixing sediment and binder materials and molding the mixture. The specimens were cured for 28 days at 23°C and 98-percent relative humidity.

Physical tests including unconfined compressive strength (UCS), freeze/thaw durability, and wet/dry durability were run to determine if the physical handling properties of the sediment were improved. Contaminant release tests were conducted to determine the effectiveness of the binder materials on immobilization of the contaminants. Based on the results of the UCS tests, specimens were selected for evaluation of contaminant release properties. The solidification/stabilization specimens were subjected to the U.S. Army Engineers Waterways Experiment Station serial leach test and the toxicity characteristic

leaching procedure (TCLP). The serial leach test results were compared to the drinking water standards, and the TCLP results were compared to the regulatory thresholds.

Based on the TCLP results for crushed specimens, the cement and kiln dust solidification/stabilization processes were effective in reducing the leachability for lead, nickel, and zinc. Leachability of copper and chromium was increased by the processes when compared with untreated sediment for both the TCLP and the serial leach test. Heavy metal releases from test specimens may have been increased during the tests by the destruction of the physical integrity of the specimens. If physical stabilization of Buffalo River sediment is to be performed, cement was recommended as the appropriate binder on the basis of strength, durability, and leachability.

As a result of this investigation it was decided that a Type I Portland cement would be used for the pilot scale demonstration and that a binder (cement) to treated solids ratio of from 0.1 to 0.6 would be used. The solidification/stabilization tests were initiated on October 30 and November 1, 1991. The treated solids from process runs B1 and B3 were combined and mixed with Type I Portland cement to achieve a cement to treated solids ratio of approximately 0.1. A total of 110 pounds of cement were mixed with 1,000 pounds of treated solids and 380 pounds of water in two batches in a 9 cubic foot gas powered concrete mixer (Table 8). The resulting mass was placed and vibrated in a 3-foot diameter sonotube (mold) form for curing. The form was set on plastic sheeting prior to placement while the top of the sonotube was covered with plastic sheeting shortly after placement of the mix.

TABLE 8
SOLIDIFICATION/STABILIZATION MIXES

Nominal Cement	Source of	Pounds	of Mate	erial	
to Treated	Treated Solids	Treated Solids	Cement	Water	Total
Solids Ratio	(Process Run)				
0.1	B1, B3	1000	110	380	1490
0.2	A2	900	179	355	1434
0.4	, · <b>A3</b>	950	376	495	1821
0.6	<b>B2</b>	1036	619	545	2200

The treated solids from process run A2 were mixed with Portland cement to achieve a cement to treated solids ratio of approximately 0.2. A total of 179 pounds of cement were mixed with 900 pounds of treated solids and 355 pounds of water in two batches in the concrete mixer. Solids resulting from the processing of A3 sediment were mixed with cement to achieve a cement to treated solids ratio of approximately 0.4. hundred seventy six pounds of cement were mixed with 950 pounds of treated solids and 495 pounds of water in two batches in the concrete mixer. Residual solids from the processing of B2 sediments were mixed with Portland cement to achieve a cement to treated solids ratio of approximately 0.6. Six hundred nineteen pounds of cement were mixed with 1,036 pounds of treated solids and 545 pounds of water in two batches. In each case the resulting mass was placed and vibrated in a sonotube form for curing in a manner similar to that described in the above paragraph. The plastic sheeting was removed from the top and the sonotube form was stripped from the four solidified masses 5 to 7 days after mixing operations. The plastic sheeting was then placed on top of the four masses and later removed after an additional four weeks of curing in the field.

### 2.11 EXECUTION AND COSTS

Sediments were dredged from the upper Buffalo River with a barge mounted crane and transported to CDF No. 4 by Manson Construction Co. on October 7, 1991. Sediments were screened through a 0.75 inch wire mesh on October 8 and 9 by RETEC personnel to remove oversized material. The screened sediments were then stored in covered 55 gallon drums while RETEC performed site preparations and mobilized the pilot scale thermal desorption processor and support equipment to the site from October 7 through October 18, 1991. Startup of the desorption unit occurred on October 21 with sediments being treated on a 5 days per week, one shift per day basis through October 31. early November, freezing temperatures and heavy snowfall necessitated that the treatment unit and its support equipment be transferred to RETEC's treatability laboratory in Acton, Massachusetts. The remaining sediments were treated on a one shift per day, 5 days per week basis with the unit set up at this facility from November 18 through 25, 1991.

Costs for the entire project were estimated in the work plan to be \$665,500, including the cost of project management, preparation of a sampling and analysis plan and health and safety plan, site preparation, sediment excavation and remediation, project monitoring, including extensive sampling, sample analysis, and preparation of this report. Actual cost of the demonstration, shown in Table 9, was approximately \$636,000. It should be noted that laboratory analytical work performed on samples collected during the demonstration cost more than the actual remediation of the sediments. This is not uncommon for a pilot scale demonstration of this nature.

TABLE 9
COST OF THERMAL DESORPTION PILOT SCALE DEMONSTRATION

Activity	Cost
Project Management	\$75,000
Health and Safety Plan	5,000
Sampling and Analysis Plan	15,000
Sediment Excavation (Incl. Misc. Equip. & Supplies)	15,000
Site Preparation	23,100
Thermal Desorption Demonstration	173,000
Demonstration Monitoring/Sample Collection (Incl. Stack Gas Monitoring)	65,000
Sample Analysis	225,000
Solidification/Stabilization	5,000
Report Preparation	35,000
Total	\$636,100

### 2.12 MONITORING

## 2.12.1 <u>Process Monitoring by Remediation Technologies, Inc.</u> (RETEC)

Evaluation of this project was conducted by performing detailed characterization of the contaminated sediment. Sediment collected from the river was sampled as soon as practical after placement in the four bins to provide an initial determination of the organics and heavy metals in the sediment. A second series of samples was collected following transport and screening to remove oversized material in order to evaluate losses subsequent to the sediments being dredged. Material passing the screen was stored in barrels and became the feed to the thermal processor. A third set of samples was collected just prior to the material being fed to the processor. Treated solids discharged from the processor were sampled for comparison to the feed and determination of the efficiency of the thermal process in removing contaminants of concern. Other process residuals were also characterized to evaluate contaminant losses from the overall process.

The critical contaminants for the evaluation were PAHs. Other organic compounds, including PCBs, were also present. Heavy metals were important contaminants in the sediment, but their concentrations were not expected to be significantly affected by the pretreatment and treatment processes. The effectiveness of the solidification/stabilization process was evaluated on the basis of changes in leachate quality for the solidified material compared to the treated solids.

Sediments from the four bins were managed to produce a range of water contents for the Buffalo River sediment fed to the thermal processor. One bin of sediments was maintained close to the water content of the as-dredged sediment and was the first material fed to the processor. For barrels of sediment from the three remaining bins, succeedingly increasing amounts of water were added to the feed. Three operating conditions were run for each water content, i.e., for each bin of sediment, yielding a total of 12 runs for the pilot project.

The pilot scale demonstration was conducted by the USEPA's Great Lakes National Program Office. The U.S. Army Corps of Engineers, Buffalo District acted as project manager on this demonstration in support of the USEPA. The District was responsible for supervision of the project, including coordination with contractors, and oversight of the field demonstration, including field sampling. The Corps of Engineers, Waterways Experiment Station provided technical support to the Buffalo District in field sampling activities and implementation of the Quality Assurance Project Plan. Laboratory analytical work was performed by Battelle Marine Science Laboratory. RETEC was responsible for collection and recording of all operational data (U.S. Army Engineer Waterways Experiment Station, 1991).

Remediation Technologies, Inc. monitored all pertinent process parameters at routine intervals during the demonstration. Regular monitoring was done to help optimize the removal efficiency of the thermal desorption demonstration unit and to develop data for full scale design. The data collected included feed rate, revolutions per minute of the thermal processor augers, input and output temperatures of the heat transfer media. residence time of the solids in the processor, temperature of solids entering and exiting the thermal processor, carrier gas flow rate, carrier gas inlet temperature, off-gas temperature, and mass rates of principal process streams. Off-gas concentrations of oxygen and hydrocarbons were monitored continuously, while other data was recorded at approximately 30 minute intervals during operation. A complete presentation of RETEC's methods and results are given in: "Field Demonstration of RETEC Thermal Unit for Remediation of Buffalo River Sediments, Buffalo River Area of Concern," RETEC, Inc., March 1992.

In summary, process temperatures were monitored at 21 locations using thermocouples. Temperature signals were transmitted to a panel readout and subsequently recorded on field data sheets (Remediation Technologies, Inc., 1992). Gas pressures were measured in the processing system with magnahelic gauges. Pressures were monitored within the processor headspace and across the principal components of the off-gas system to ensure proper operation of the system and to help anticipate maintenance problems such as poor heat transfer. Inert gas flow rate into the processor was monitored by standard flow meter while flow rate in the off-gas stack was measured with a hot wire anemometer. The sediment feed rate to the processor was determined by recording the volumetric displacement of the feed system per unit time and converting to mass flow rate using the measured density of the feed material. The validity of these observations was assessed by comparing them against known capacities of the processing and cooling augers at the associated operating conditions. Based on these data, RETEC determined that there was significant variability in both the pumping rate and density of feed material. Therefore, average material feed rates were calculated for each run by dividing the total mass of feed material by the feed duration.

### 2.12.2 Air Monitoring

# 2.12.2.1 Air Monitoring by Remediation Technologies, Inc. (RETEC) --

RETEC, Inc. monitored process exhaust gas for total hydrocarbon content and for concentration of four specific volatile hydrocarbons. These measurements were performed as an instantaneous assessment of process performance, and were used with moisture data to optimize process efficiency. Total hydrocarbon concentration was measured using a flame ionization detector and a propane standard. This result was converted to an emissions rate using the stack gas flow rate. Overall emissions ranged from zero to 1178 ppm as propane, with an average of 10 ppm as propane. The average discharge rate was 0.02 pounds per hour. Average emissions rates represent the total organic compound emissions for processing Buffalo River sediment under the operating conditions of the pilot demonstration.

Additionally, specific analyses were performed for benzene, toluene, ethylbenzene, and xylene (BTEX) using a modified NIOSH procedure employing activated charcoal tubes. Exhaust concentrations of benzene averaged 0.61 mg per cubic meter (0.137 grams per hour). Concentrations of ethylbenzene, toluene, and xylene averaged 0.06, 0.02, and 0.02 mg per cubic meter, respectively (Table 10). Again, these average rates represent expected BTEX emissions for thermal desorption of Buffalo River sediment under conditions of periodic optimization.

Details of RETEC's air sampling procedures and their use in process optimization are given in "Field Demonstration of RETEC Thermal Unit for Remediation of Buffalo River Sediments, Buffalo River Area of Concern," RETEC, Inc., March 1992.

TABLE 10 RESULTS OF VAPOR MONITORING BY RETEC, INC.

(30/91   Date: 10/31/91   Date: 11/21/91   Date: 11/22/91   Date: 11/25/91   Date: 11/25/91
g/hr   mg/m <sup>3</sup> g/hr   mg/m <sup>3</sup>
0.126   0.52 0.115
NA I NA NA
NA NA NA
NA I NA NA
NA NA NA
·

NA = Not Analyzed
DATA SOURCE: Referenced RETEC, Inc. Report: Results are for 8 hour time integrated samples averaged over 8 hour gas
flow rate or 8 hour time period as indicated.

2.12.2.2 Air Monitoring by E-Three, Inc. --

E-Three, Inc. sampled stack emissions for concentration of total particulates, polychlorinated biphenyls (PCBs), and polycyclic aromatic hydrocarbons (PAHs). Sampling was performed in several 2-3 hour increments over a period of 10 days. Data generated by E-Three, Inc. was not used for on-site process optimization. Rather, the E-Three data was used to quantify emissions of semi volatiles and particulates for the process conditions used by RETEC. Sampling and analytical methods numbers are presented in Table 11, and a summary of analytical results is given in Table 12. Results are for time integrated samples taken over 3 hours and averaged over the number of dry standard cubic meters (DSCM) of air discharged from the system in that time. While these emissions are referred to as "air emissions," the actual composition is not strictly that expected for air. The processing system is blanketed with nitrogen to prevent combustion of organic constituents in the sediment, and the resulting emissions are 7 percent oxygen. Complete test results are available in "Stack Emission Test Report: Demonstration Thermal Desorption Project, Buffalo River Sediments, " E-Three, Inc., Buffalo, NY.

### 2.12.3 Corps of Engineers Monitoring

The Corps of Engineers performed general project oversite including direction of all contractors involved in field operations. Additionally, the Corps of Engineers conducted an intensive sampling and analysis program as described below and as delineated in the referenced Quality Assurance Project Plan. Results of this program are summarized in the following text, and the complete data set for this effort is presented in Appendix B. Process data was provided by RETEC, Inc., and appears previously in Table 7A and 7B.

### 2.12.3.1 Sampling--

The Corps of Engineers sampled solid and liquid streams both into and out of each process step and submitted these samples to Battelle Laboratories for analysis. Analytical methods employed for these analyses are given in Table 13 for sediments and in Table 14 for water samples (U.S. Army Engineer Waterways Experiment Station, 1991). The primary intent of this sampling and analysis program was to determine process stream changes, and therefore remediation effectiveness, at each stage of the pilot operation. Other goals for sampling and analysis were to (a) obtain information for process scaleup, (b) assess reductions in contaminant concentrations of the sediment during remediation, and (c) assess effectiveness of cementitious stabilization as a treatment for process residuals. A process flow diagram depicting Corps of Engineers sampling points is given in Figure 10.

TABLE 11

SUMMARY OF AIR SAMPLING AND ANALYTICAL PROCEDURES:
E-THREE/BATTELLE

Parameter	Sampling Method	Analytical Method
Particulates PCB/PAH CO2, O2, N2 CO Moisture Volumetric Flow Dioxins	EPA Method 5 EPA Method 23 EPA Methods 3 and 3A EPA Method 10 EPA Method 4 EPA Method 1 & 2 EPA Method 23	Gravimetric High Resolution GC/MS Orsat/CEM GFC-NDIR  High Resolution GC/MS

DATA SOURCE: Referenced E-Three, Inc. Report

TABLE 12A
AIR EMISSIONS OF POLYCHLORINATED BIPHENYLS
IN MICROGRAMS PER DRY STANDARD CUBIC METER

PCB Homolog	Minimum Emissions ug/DSCM @ 7% 0 <sub>2</sub>	Maximum Emissions ug/DSCM @ 7% 0 <sub>2</sub>
Monochlorobiphenyl	<0.33	<1.81
Dichlorobiphenyl	<0.33	<1.81
Trichlorobiphenyl	<0.33	<1.81
Tetrachlorobiphenyl	<0.66	<3.62
Pentachlorobiphenyl	<0.66	<3.62
Hexachlorobiphenyl	<0.66	<3.62
Heptachlorobiphenyl	<1.01	<5.55
Octachlorobiphenyl	<1.01	<5.55
Nonachlorobiphenyl	<1.01	<5.55
Decachlorobiphenyl	<1.67	<9.18

These values are all below detection limits. Detection limits are varying due to (a) compound - specific nature of detection limits and (b) solids content of the sample.

TABLE 12B
AIR EMISSIONS OF PARTICULATES IN MICROGRAMS
PER DRY STANDARD CUBIC METER

	Minimum Emissions ug/DSCM @ 7% 0 <sub>2</sub>	Maximum Emissions ug/DSCM @ 7% 0 <sub>2</sub>	
Particulates	0.0019	0.0027	-

TABLE 12C
AIR EMISSIONS OF POLYCYCLIC AROMATIC HYDROCARBONS
IN MICROGRAMS PER DRY STANDARD CUBIC METER

PAH	Minimum Emiss ug/DSCM @ 7%	Maximum Emiss ug/DSCM @ 7%	Average Emiss ug/DSCM @ 7%	
Naphtahalene	27.78	322.98	114.43	
Acenapthylene	0.25	3.34	1.31	
Acenaphthene	0.78	6.61	3.13	
Fluorene	1.23	3.04	4.36	
Phenanthren <b>e</b>	8.68	129.62	42.96	
Anthracene	0.84	12.89	4.61	
Fluoranthene	3.16	93.26	27.14	
Pyrene	1.81	34.67	13.62	
Benz(a)anthracene	0.36	24.30	9.05	
Chrysene	0.43	10.60	3.85	
Benzo(bjk)fluoranthrene	0.85	19.45	6.01	
Benzo(a)pyrene	0.21	2.42	1.12	1
<pre>Indo(1,2,3-cd)pyrene</pre>	0.21	3.66	1.40	
Dibenz(a,h)anthracene	0.20	0.32	1.65	
Benzo(g,h,i)perylene	0.23	1.45	0.80	
TOTA	L ·		235.44	

TABLE 12D
AIR EMISSIONS OF DIOXINS IN MICROGRAMS
PER DRY STANDARD CUBIC METER

Dioxin	Minimum Emissions ng/DSCM @ 7% 0 <sub>2</sub>	Maximum Emissions ng/DSCM @ 7% 0 <sub>2</sub>
2378-TCDD	0.03480	0.25800
12378-PeCDD	0.00727	0.26100
123478-HxCDD	0.00220	0.00347
123678-HxCDD	0.00304	0.00313
123789-HxCDD	0.00573	0.00318
1234678-HpCDD	0.00156	0.00373
OCDD	0.00122	0.00115

Emissions reported as 2378-TCDD Toxicity Equivalents (i.e., they are quantitiated based on a 2378-TCDD Standard)

# TABLE 12E AIR EMISSIONS OF FURANS IN MICROGRAMS PER DRY STANDARD CUBIC METER

Furan	Minimum Emissions ng/DSCM @ 7% 02	Maximum Emissions ng/DSCM @ 7% 0 <sub>2</sub>
2378-TCDF	0.0000	0.0013
12378-PeCDF	0.0000	0.0000
23478-PeCDF	0.0000	0.3530
123478-HxCDF	0.0000	0.0838
123678-HxCDF	0.0003	0.0686
234678-HxCDF	0.0000	0.0015
123789-HxCDF	0.0000	0.0217
1234678-HpCDF	0.0000	0.0237
1234789-HpCDF	0.0000	0.0000
OCDF	0.0000	0.0000

<sup>\*</sup> Emissions reported as 2378-TCDD Toxicity Equivalents (EPA 1989)

Zero values in Table 12E were the result of taking total weight of the compound collected on resin over the 2-3 hour sample period and dividing by the dry standard cubic meters (DSCM) of air emitted in that time.

DATA SOURCE: Referenced E-Three, Inc. Report

Processing was done under 12 sets of conditions, each involving 3 to 4 drums of dredged material. Composite samples were taken for each set of process conditions as follows: For the solid samples (1S, 2S, 3S, 4S, 7S, 8S on Figure 10), three grab samples were taken from each of the drums associated with the process conditions at that point and composited to form one representative sample. Feed samples were taken from the top, middle, and bottom of each drum, while samples of treated sediment and residuals were taken at approximately the beginning, middle, and end of each run. Each composite was submitted for analysis of solids, total organic carbon (TOC), mercury, chromium, lead, oil and grease, PCBs, and 17 individual polycyclic aromatic hydrocarbons (PAHs). Additionally liquid samples were taken at the two points where liquid is removed from the process, namely: a removal point just past the processor inlet (9L on Figure 10) and a removal point just prior to the processor outlet (10L on Figure 10). In each case, the removed liquid was condensed, collected in a receiver, and the receiver contents for the entire run were well mixed prior to sampling. Liquid samples were analyzed for the same chemical parameters as were the solid samples.

Corps of Engineers air sampling was contracted to E-Three, Inc., and the resulting analyses were performed by Battelle Laboratories. No air sampling was performed directly by the Corps of Engineers.

### TABLE 13 ANALYTICAL PARAMETERS FOR SEDIMENT SAMPLES

	ARCS		Battelle		[
	Required		Instrument	!	ļ
l .	Detection		Detection	Volume	
ļ	Limit		Limit	Required	1
Analysis	ug/g	Method	ug/g	l ml	Container
PAHs-16 Compounds			<u> </u>	1	
by GC/MS	0.2	NOAA 1985	0.02	100	4 oz
PCBs	1				i
(total Aroclors)	i0.02i	NOAA 1985	0.02	100	glass
Cr Cr	2 1	PNL-SP-19B	i		Spex Jar
Cu	1 2 1	PNL-SP-19B	1	Ī 50	or
Hg	0.1	MSL-M-11	0.02	Ī	32 oz
Pb	1 2 1	PNL-SP-19B	1	Ī	plastic
Total Organic			0.10%		_
Carbon	<u> 300 i</u>	EPA 9060	(100 ug/g)	50	<u>i</u> i
1	1		0.10%		4 oz
Total Solids	1000	EPA 160.3	(100 ug/g)	50	plastic
  Total Volatile			0.10%	! !	
Solids	1000	EPA 160.4	(100 ug/g)	50	
  16 Fractions					
	) 1 NT/A !	DCED 1004	1 00%	100	8 oz
Grain Size	N/A	PSEP 1986	1.00%	100	plastic
Oil and Grease	·				4 oz
(Solvent		EPA-LLRS-			. 52
Extractables)	N/A	GROSSE	N/A	50	glass

### References:

NOAA 1985 - NOAA 1985, Nation Oceanic and Atmospheric Administration, National Status and Trends Program, Standard Analytical Procedures.

. PAHs: GC/MS, using selective Ions mode (S.I.M)

. PCBs: GC/ECD using capillary columns

PNL-SP-19B - Energy Dispersive X-Ray Fluorescence Spectrometry (SOP # from Battelle Labs)

MSL-M-11 - Cold Vapor Atomic Absorption. (SOP # from Battelle Labs)

EPA 9060, TOC - U.S. Environmental Protection Agency (EPA). 1986. Test Methods for Evaluating Solid Waste: Physical/Chemical Methods. SW-846. U.S. Document No. 955-001-00000, USEPA, Washington, D.C.

EPA 160 - U.S. Environmental Protection Agency (EPA). 1983. Methods for Chemical Analysis of Water and Wastes, EPA-600/4-79-020, March, 1983, Method 413.2.

PSEP 1986 - Puget Sound Estuary Protocols.

ASTM-D422 - American Society of Testing Materials (ASTM). 1972. Standard Method for Particle-Size Analysis of Soil D-422. ASTM, Philadelphia, Pennsylvania.

EPA-LLRS-GROSSE - Procedure supplied by Great Lakes Large Lakes Lab, "Analysis of Solvent - Extractable Residue from Whole Sediment."

TABLE 14
ANALYTICAL PARAMETERS FOR WATER SAMPLES

			the state of the s		
Analysis	ARCS Required Detection Limit ug/g	Method	Battelle   Instrument   Detection   Limit   ug/l	Volume Required ml	       Container
PAHs-16 Compounds by GC/MS	2	NOAA 1985	0.02	1000	   1000 m1   glass
PCBs (total Aroclors)	0.01	NOAA 1985	0.01	1000	1000 m1   glass
Cr Cu Hg Pb	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PNL-SP-24 PNL-SP-24 MSL-M-24 PNL-SP-24	1 1 1 0,005		500 m1 Teflon
Total Organic Carbon	1000	EPA 415.2	1000	200	60 ml   glass
Total Solids	1000	EPA 160.3	1000	200	1 1000 m1
Total Suspended Solids	1000	EPA 160.1	1000	200	   poly
pH Sp. Conductance	   Full Range   Full Range				   200 m1   plastic
Oil & Grease	N/A	5520B	1.1 mg/1	1000	1000 ml glass

### Additional References:

PNL-SP-24 - Metals and trace elements in water by Inductively Coupled - Mass Spectrometry (ICP/MS)

MSL-M-27 - Total mercury in water by CVAA

EPA 415.1 - Total Organic Carbon in water.

Method 5520B - "Standard Methods for the Examination of Water and Wastewater," 18th Edition, AWWA/WPCF.

### 2.12.3.2 Analytical Protocol--

Samples were analyzed using the analytical methods referenced in Tables 13 and 14. These methods were applied within the framework of a Quality Assurance Project Plan (QAPP) prepared by the U.S. Army Corps of Engineers Waterways Experiment Station. In general, this QAPP provided for replication of 5 percent of all field samples, performance of matrix spikes/matrix spike duplicates, and processing of all blanks associated with standard analytical lab practice. Both the analytical methodology and the quality assurance procedures generally proceeded per plan as determined by the Waterways Experiment Station and the Buffalo District Corps of Engineers. Most of the detection limits for analytes of concern were at or below the target limits given in Tables 13 and 14. Exceptions were detection limits for PAHs and PCBs. Detection limits for PAHs were 0.06 ug/g for sediment (versus the target 0.02 ug/g) and 0.04 ug/l for water (versus the target 0.02 ug/l). Detection limits for PCBs met the target values for sediment, but were 0.05 to 0.5 ug/l for water (versus the target 0.01 ug/l). Detection limit problems were caused by matrix effects that necessitated dilution of the samples in question.

Complete results of these analyses and the associated quality assurance testing are available in "Report of Chemical Analyses: Volumes 1-3," prepared for the USEPA Great Lakes National Program Office by Battelle Marine Research Laboratory. Summaries of these data, and an assessment of process performance based on these results, appear in subsequent sections of this report.

### 3.0 RESULTS AND DISCUSSION

### 3.1 CORPS OF ENGINEERS RESULTS

Reduced analytical data for the Buffalo Thermal Desorption Pilot Demonstration appear in subsequent sections of this report. Data is provided separately for each constituent of concern. Based upon presented results, an assessment is made regarding process efficiency for removing each chemical contaminant.

### 3.1.1 Overall Mass Balance

An overall mass balance was performed on solids and liquids for this process. The intent was to measure the percent of feed material that could be accounted for after processing (i.e., percent closure). Results of this mass balance were reported by RETEC, and appear in Table 15. Closures of 100 percent ± 15 percent are desirable. For closures in this range, stream weights can be used with reasonable confidence to track individual compounds through the system and thus assess treatment effectiveness.

Based on acceptable closure constraints, all but Run B3 are suitable runs for determining process performance. Three additional runs were eliminated from consideration for other

TABLE 15
SOLIDS/LIQUIDS MASS BALANCE

	Feed		Treated(	b)	Total		Percent
Run No.	Material	(lbs)	Material	(lbs)	Condensate	(lbs)	Closure
A1	1896		970		765	7	93
A2	2010		1055		890		97
A3	2150		1235		688		89
B1	1355		845		620		108
B2	2175		1850		445		106
a B3	2180		585		465		48
C1	1640		880		840		105
C2	1905		955		880		96
C3	1940		950		850		93
D1	1515		700		950		109
D2	1150		480		550		90
D3	1630		955		790		107

- a. Closure is unacceptable for mass balance calculations
- b. This weight includes the weight of the solids which exited the cyclones.

DATA SOURCE: Referenced RETEC, Inc. Report

reasons. Run Al was considered a startup run, so only a partial data set was taken. Due to budget constraints, Runs D2 and D3 were archived without performing analytical tests. Thus, all subsequent data is reported for Runs A2, A3, B1, B2, C1, C2, C3, and D1.

### 3.1.2 Solids Content

Total solids data is given in Tables 16A and 16B and volatile solids data is presented in Table 17. Graphs of these parameters versus final solids temperatures are given in Figures 11 and 12 (Error bars shown are for the standard error of the mean). From these data, it is clear that feed material containing 44-56 percent solids was successfully pumped and dryed such that final solids content normally exceeded 95 percent. Maximum sediment temperatures employed to achieve these results varied from 300°F to 480°F and residence times varied from 30 to 90 minutes.

Because one project goal was to obtain information for design and operation of a full scale process, it was desired to determine whether removal efficiencies were a function of any of the process variables monitored for the study. To assess effects of process variables, correlation coefficients were determined relating removal to each measured process parameter. (The formula used to calculate the correlation coefficient is given in Appendix A).

TABLE 16A PERCENT TOTAL SOLIDS IN SEDIMENT

Run Number	A2	A3	B1	В2	C1	C2	С3	D1
PROCESS CONDITIONS				 				
Feed Rate 1bs/hr	346	716	860	644	484	635	862	388
Residence Time min.	60	30	45	60	90	60	45	90
Max. Sediment Temp. °F	480	380	300	   364	392	415	474	367
SAMPLE POINTS								
After Dredging (ls)	58.0	58.0	55.2	55.2	59.8	59.8	59.8	56.9
After Screening (2s)	63.0	60.2	63.2	62.0	63.8	63.9	64.8	58.2
Before Thermal Proc. (3s)	55.4	55.0	56.1	   54.6	52.1	50.8	48.3	44.6
After Thermal Proc. (4s)	99.8	99.5	98.6	99.8	99.8	99.9	95.2	99.9
Solids from 1st Cyclone (7s)	95.3	97.5	99.1	87.1	83.0	95. <b>3</b>	85.1	94.2
Solids from 2nd Cyclone (8s)	77.1	99.6	99.5	   99.5 	98.4	N/A	99.6	99.7

TABLE 16B PERCENT TOTAL SOLIDS IN CONDENSATE

Run Number	A2	A3	В1	В2	C1	C2	С3	Dl
SAMPLE POINTS *	<u> </u>	<del> </del>  -	1	1		!		
After 1st Condenser (9L)	1.1	   N/A	N/A	0.7	0.9	0.5	0.9	0.4
After 2nd Condenser (10L)	0.8	0.8	0.8	0.2	0.2	0.1	0.1	0.2

<sup>\*</sup> Process conditions same as for sediment

N/A = Not Analyzed

Highlighted values are average of multiple measurements. Averages were calculated using 3-5 individual measurements.

DATA SOURCE: Referenced Battelle Report

TABLE 17 PERCENT VOLATILE SOLIDS IN SEDIMENT

Run Number	A2	A3	B1	B2	C1	C2	C3	D1
PROCESS CONDITIONS	,	! !		ļ 1	<u> </u>	 	1	
Feed Rate lbs/hr	346	   716	860	644	484	635	862	388
Residence Time min.	60	i i 30	45	60	90	60	45	90
Max. Sediment Temp. °F	480	l   380	300	364	392	415	474	367
SAMPLE POINTS		 		 	!	! 		] 
After Dredging (ls)	6.4	6.4	6.2	6.2	5.1	5.1	5.1	5.5
After Screening (2s)	6.0	6.0	5.4	5.4	4.9	5.3	5.5	5.4
Before Thermal Proc. (3s)	5.6	5.6	5.5	5.5	5.4	5.6	5.0	4.9
After Thermal Proc. (4s)	3.4	4.2	3.7	4.3	4.3	3.7	4.1	3.4
Solids from 1st cyclone (7s)	4.7	5.4	5.1	3.8	4.9	4.9	5.2	5.1
Solids from 2nd Cyclone (8s)	2.3	4.7	5.0	1   3.8 	4.2	I N/A	   4.8	   4.5

<sup>%</sup> Volatile Solids =  $\frac{(A - D)}{A} \times 100$ 

WHERE: A = weight of residue after drying at 105°C for 1 hour
D = weight of residue after <u>dried</u> residue has been ignited at 550°C for 1 hour

Highlighted values are the averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

DATA SOURCE: Referenced Battelle Report

N/A = Not Analyzed.

FIGURE 11
% SOLIDS VERSUS EXIT TEMPERATURE OF SOLIDS
(NUMBERS IN PARENTHESES ARE NUMBERS OF DATA POINTS FROM WHICH THE STANDARD ERRORS WERE CALCULATED)

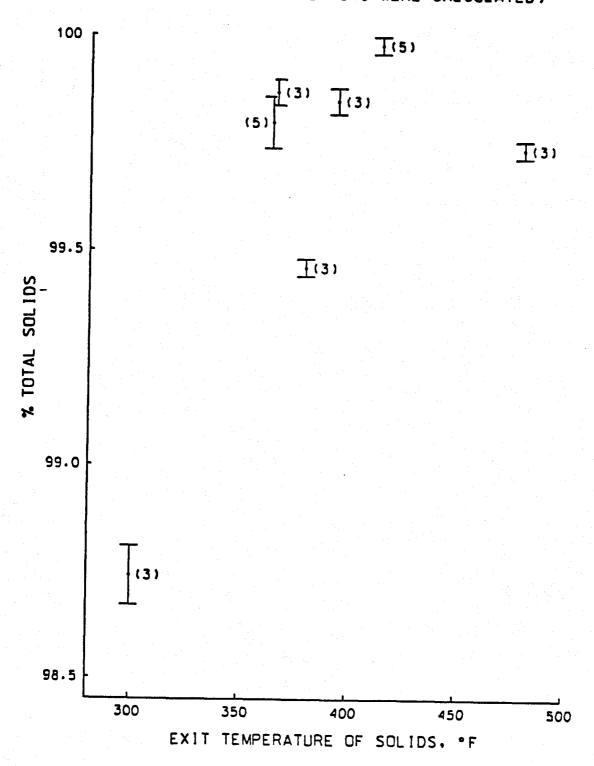
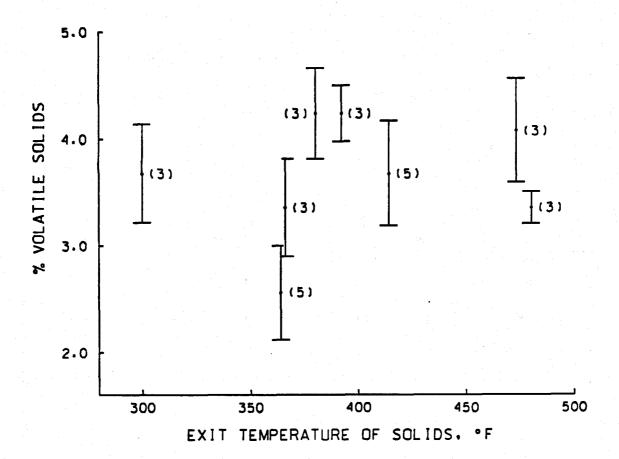


FIGURE 12
% VOLATILE SOLIDS VERSUS EXIT TEMPERATURE OF SOLIDS
(NUMBERS IN PARENTHESES ARE NUMBERS OF DATA POINTS
FROM WHICH THE STANDARD ERRORS WERE CALCULATED)



A correlation coefficient of ± 1.0 means that process performance can be perfectly predicted if the value of the process variable is known. An r value of 0 means that process performance and the process variable are completely unrelated. (Correlation coefficients ranging from 0 to +1.0 apply to variables related by a straight line with a positive slope and correlation coefficients from 0 to -1.0 apply to variables that are related by a straight line with a negative slope.) Correlation coefficient values with an absolute value higher than 0.9 are usually considered as acceptable for prediction of process performance. Correlation coefficients relating process parameters with volatiles removal are given in Table 18.

TABLE 18
CORRELATION COEFFICIENTS FOR VOLATILE SOLIDS REMOVAL

Parameter Correlated with Total Volatile Solids (TVS) Removal	Correlation Coefficient
Process Temperature Residence Time Initial Volatiles Solid Content	0.40 0.40 -0.34

Based on these results, it is clear that some other phenomenon besides initial liquids content and simple energy input is dictating extent of drying of sediment and therefore extent of contaminant removal. It is possible that some threshold energy input is required before complete removal of these materials is achieved, and that the threshold was not reached with the residence times and temperatures employed for this study. RETEC's thermal desorption process is capable of achieving maximum sediment temperatures of 700-800°F, at the expense of throughput rate. Should this process be tried again, it is suggested that trials at higher temperatures take place.

### 3.1.3 Metals

An overall material balance was performed on each run for each metal of concern. A sample calculation is provided for Run A3, for chromium, as follows:

### (a) Adjustment of Measured Stream Weights to a Dry Weight Basis

Mass of Input:

(2150 lbs) x (
$$0.550$$
 lbs dry solids) x ( $0.454$  kg) = 537 kg dry solids lb

Mass of Output/Solid Stream (Average percent solids in treated solids plus residue from cyclones):

(1235 lbs) x (
$$0.995$$
 lbs dry solids) x ( $0.454$  kg) = 557 kg dry solids lbs

Mass of Solid Output in Liquid Stream:

(688 lbs liquid) x (0.008 lb solids) x (0.454 kg) = 2.5 kg dry solids lb liquid lb

(b) Material Balance on Chromium for Run A3

(537,000 g solids) 
$$\times$$
 (68  $\times$  10<sup>-6</sup> g Cr) = 36.5 g Cr g solids

Since it is not known what percent of total solids came from the cyclones (they were combined and then analyzed), the following is assumed for these calculations:

cyclone 1: 4%

cyclone 2: negligible

Overall concentration of processed solids is therefore: 0.96(61) + 0.04(148) = 65 ug/g

Where 61 ug/g and 148 ug/g are analytical values

Cr in Treated Solids:

(557,000 g) x (
$$\frac{65 \times 10^{-6} \text{ g Cr}}{g}$$
) = 36.2 g

Cr in Condensate Solids:

$$(2,500 g) (\frac{148 \times 10^{-6} g Cr}{g}) = 0.37 g (negligible)$$

Cr in Condensate:

(688 lbs) x (
$$0.454 \text{ kg}$$
) = 312 kg

Percent Removed from Sediment:

$$(36.5 g - 36.2 g) \times 100 = 0.8%$$
removal 36.5 g

Analytical results for metals are summarized in Tables 19A and 19B thru 22A and 22B. From these results, it is clear that removal levels are somewhat metal specific. Copper, lead, and chromium are discussed together because they behave similarly under conditions employed for this study. Mercury is discussed separately because its behavior is distinctly different from the other metals.

### Copper, Lead, and Chromium

For copper, lead, and chromium, residue concentrations in ug/g did not change appreciably from those in the feed although

TABLE 19A LEAD IN SEDIMENT (ug/g Dry Weight)

Run Number	A2	А3	B1	В2	C1	C2	C3	D1
PROCESS CONDITIONS	<b>!</b>		ļ [	   	) !	   !	]   !	<u> </u> 
Feed Rate 1bs/hr	   346	716	   860	   644	   484 	635	   862	   388 
Residence Time min.	60	30	l   45	60	90	60	45	90
Max. Sediment Temp. °F	480	380	1   300	364	392	415	   474	   367
SAMPLE POINTS		 	[   		!   !	! 		<u> </u> 
After Dredging (1s)	72.2	72.2	   49.3	   49.3	   88.8	   88.8	88.8	49.7
After Screening (2s)	52.4	52.4	58.2	58.2	62.3	62.3	62.3	62.3
Before Thermal Proc. (3s)	53.7	52.4	64.3	61.7	l   68.4	71.9	56.3	73.5
After Thermal Proc. (4s)	52.1	52.7	65.7	67.0	70.6	67.2	58.3	64.7
Solids from 1st Cyclone (7s)	58.9	56.7	65.1	67.0	83.8	70.7	70.4	63.6
Solids from 2nd Cyclone (8s)	48.8   48.8	48.0	58.4	64.5	59.7	N/A	61.7	71.8

TABLE 19B
LEAD IN CONDENSATE
(Filtered)
(ug/L)

Run Number	A2	A3	B1	<u>B2</u>	<u>C1</u>	C2	C3	D1
SAMPLE POINTS *			   !	    -	! 	!   	! 	   
After 1st Condenser (9L)	N/A	N/A	N/A	   N/A	N/A	   N/A	N/A	I N/A
After 2nd Condenser (10L)	2.97	1.19	3.56	2.37	   1.78	14.0	17.8	8.90

### N/A Not Analyzed

Highlighted values are averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

<sup>\*</sup> Process conditions same as for sediment

TABLE 20A
CHROMIUM IN SEDIMENT
(ug/g Dry Weight)

Run Number	A2	A3	<u>B1</u>	В2	C1	C2	C3	Dl
PROCESS CONDITIONS	1	 	<u> </u>		 			 
Feed Rate lbs/hr	346	   716	860	644	484	635	862	1 388
Residence Time min.	60	1   30	1 45	60	90	60	45	90
Max. Sediment Temp. °F	480	380	300	364	392	415	474	367
SAMPLE POINTS	! !	 	! 	!	1		 	
After Dredging (1s)	l   73	l   73	1 63	63	1 80	l   80	80	74
After Screening (2s)	l   60	l   60	   51	51	71	71	71	60
Before Thermal Proc. (3s)	47	   68	   47	58	73	   59	69	55
After Thermal Proc. (4s)	70	61	1   56	1 44	67	58	62	62
Solids from 1st Cyclone (7s)	1 137	148	!   129	1 106	136	1 129	140	112
Solids from 2nd Cyclone (8s)	1   84	1   88 	1   121	1   77	129	   N/A	140	1118

# TABLE 20B CHROMIUM IN CONDENSATE (Filtered) (ug/L)

Run Number	A2	A3	B1	В2	C1	C2	С3	D1
SAMPLE POINTS *		1			1		[ ]	
After 1st Condenser (9L)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
After 2nd Condenser (10L)	4.2	2.9	2.52	1.76	2.78	1.80	1.01	1.64

### N/A Not Analyzed

Highlighted values are averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

<sup>\*</sup> Process conditions same as for sediment

TABLE 21A COPPER IN SEDIMENT (ug/g Dry Weight)

Run Number	A2	A3	B1	В2	_C1	C2	C3	D1
PROCESS CONDITIONS	 			 				*
Feed Rate lbs/hr	346	716	860	644	484	635	862	388
Residence Time min.	60	30	45	60	90	60	45	90
Max. Sediment Temp, °F	480	380	300	364	392	415	474	367
SAMPLE POINTS							-	
After Dredging (1s)	46.2	46.2	41.0	41.0	56.8	56.8	56.8	37.7
After Screening (2s)	45.8	45.8	43.0	43.0	47.8	47.8	47.8	45.0
Before Thermal Proc. (3s)	41.1	40.6	37.6	43.0	45.3	48.2	47.2	44.8
After Thermal Proc. (4s)	38.2	41.3	45.7	45.6	58.0	48.8	45.4	47.6
Solids from 1st Cyclone (7s)	51.3	47.1	48.2	46.8	54.8	56.1	62.4	51.3
Solids from 2nd Cyclone (8s)	42.3	43.1	46.2	47.1	62.1	N/A	52.5	53.7

TABLE 21B
COPPER IN CONDENSATE
(Filtered)
(ug/L)

Run Number	A2	_A3	B1	B2	C1	C2	C3	D1_
SAMPLE POINTS *		 	1	1	į			
After 1st Condenser (9L)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
After 2nd Condenser (10L)	830	410	340	450	720	120	70 <u> </u>	755

### N/A Not Analyzed

Highlighted values are averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

<sup>\*</sup> Process conditions same as for sediment

TABLE 22A
MERCURY IN SEDIMENT
(ug/g Dry Weight)

Run Number	A2	A3	B1	B2	C1	C2	C3	Dl
PROCESS CONDITIONS			 	 	 	 	 	<u> </u>
Feed Rate 1bs/hr	346	716	860	644	484	   635	862	   388
Residence Time min.		30	45	l   60	90	   60	   45	90
Max. Sediment Temp. °F	480	380	300	   364	   392	415	   474	367
SAMPLE POINTS			   	 	 	   	! 	
After Dredging (ls)	   0.18	0.18	0.17	0.17	0.34	0.34	0.34	0.11
After Screening (2s)	0.19	0.19	0.21	0.21	0.20	0.20	I   0.20	0.21
Before Thermal Proc. (3s)	0.17	0.18	0.20	0.20	0.20	0.21	0.18	0.19
After Thermal Proc. (4s)	0.00	0.05	0.11	0.00	l   0.07	0.05	0.15	0.01
Solids from 1st Cyclone (7s)	0.15	0.12	0.13	0.10	0.32	0.22	0.49	0.21
Solids from 2nd Cyclone (8s)	   0.02  	0.04	0.12	0.02	   0.30	   N/A	l   <b>0</b> .06	   0.03

TABLE 22B
MERCURY IN CONDENSATE
(Filtered)
(ug/L)

Run Number	A2	A3	B1	B2	C1	C2	C3	D1
SAMPLE POINTS *			 		[ [		[ ]	 
After 1st Condenser (9L)	(44.07)	3.26	N/A	   5.28	9.30	2.16	0.01	3.20
After 2nd Condenser (10L)	2.50	4.00	   0.95	1.44	1.34	3.66	   1.81	3.37

### N/A Not Analyzed

Highlighted values are averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

<sup>\*</sup> Process conditions same as for sediment

concentrations of lead and chromium decrease significantly from dredging to screening. Although not determined experimentally, it is postulated that some of the metals precipitated and adhered to the side-walls of the storage drum. During treatment, all three metals tend to remain with the treated residue, and are thus found either in the bulk of the treated residue or in the treated solids captured by the cyclones. For copper and lead, concentration of the cyclone solids is approximately the same as concentration of the bulk residue. For chromium, the concentration is greater in the cyclone solids than in the bulk residue, suggesting that chromium tends to associate with the finer particulates. Concentrations of Cu, Pb, and Cr in condensate are negligible. In summary, copper, chromium and lead tend to remain with the solids and are potential candidates for stabilization.

One of the goals for this study was to assess contaminant losses during processing. For this reason, a mass balance was performed on each metal for each process step to determine fate of the metals that were removed by processing. That is, if the constituent was desorbed from the residue, where did it go and how must it be captured to prevent further environmental contamination? A sample mass balance calculation is given in Appendix A. Table 23 summarizes the mass balance results for Cu, Pb, Cr, and Hg.

From these results it is clear that the majority of these metals remain with the residue. As can be seen from these results, mass balance closures are variable. Sometimes all material is not accounted for, while at other times the output of key constituents of concern appears to exceed the input. There are several reasons why this is true.

- (1) Most constituents of concern for this project were present in extremely small quantities. For example, the total quantity of chromium being tracked through the process for an entire run was in the range of 50 grams. For such small contaminant quantities, the sum of the extremely small errors inherent in the analytical procedures comprises a significant percentage of the total amount present.
- (2) Individual weights of the solid streams were not taken, rather all solids were combined and a single weight was obtained. Since compositions of these individual streams were not the same, the act of combining these streams resulted in an approximate rather than an exact material balance.
- (3) Air emissions analysis did not include analysis for metals, thus metal losses into the atmosphere or within the carbon adsorber were not quantified. Indeed, the carbon adsorber is a sink that was not accounted for in the sampling and analysis program.

#### TABLE 23A SUMMARY OF CALCULATIONS CHROMIUM

#### <--- GRAMS OUT --->

				PERCENT
BIN	GRAMS IN	RESIDUE	CONDENSATE	REMOVED
A2	23.7	34.8	5.2	0
A3	36.5	36.2	4.4	0.8
B1	16.2	22.3	0.5	0
B2	31.3	39.4	0.0	0
C1	28.3	27.9	0.3	1.4
C2	25.9	26.4	0.2	0
C3	29.3	26.7	0.4	8.8
D1	16.9	20.3	0.3	_0_
No sign	nificant chan	qe	AVG	1.4

#### TABLE 23B SUMMARY OF CALCULATIONS COPPER

#### <--- GRAMS OUT --->

BIN GRAMS IN RESIDUE CONDENSATE REI	RCENT MOVED
	11.1
A2 20.7 18.4 10.3	
A3 21.8 23.0 2.2	0
B1 13.0 17.3 0.2	0
B2 23.1 38.5 0.0	0
C1 17.5 23.0 1.4	0
C2 21.1 21.2 0.9	0
C3 20.0 18.9 0.8	5.5
D1 13.8 15.2 0.3	0
AVG	2.0
No significant change	

#### TABLE 23C SUMMARY OF CALCULATIONS LEAD

<--- GRAMS OUT --->

BIN	GRAMS IN	RESIDUE	CONDENSATE		REMOVED SEDIMENT
A2	27.1	25.0	5.1		7.7
<b>A</b> 3	28.1	29.5	2.2		0 2
B1	22.2	24.7	0.0		0
B2	33.3	56.1	0.0		0
Cl	26.5	28.3	0.3		0
C2	31.6	29.1	0.1		7.9
<b>C</b> 3	23.9	24.2	0.1		0
D1	22.6	20.5	0.2		9.3
				AVG	3.1
No si	gnificant cha	nge			

No significant change

#### TABLE 23D SUMMARY OF CALCULATIONS MERCURY

<--- GRAMS OUT --->

BIN	GRAMS IN	RESIDUE	CONDENSATE		T REMOVED SEDIMENT
A2	.086	.005	0.03		94.1
<b>A</b> 3	.094	.028	0		70.2
B1	.070	.042	0		40.0
B2	.107	0	<b>o</b>		100
C1	.078	.030	0		61.5
C2	.094	.010	<b>o</b> • • •		89.4
<b>C</b> 3	.074	.067	0		9.5
D1	.057	.007	0		87.7
				AVG	69.2

The process equipment used for this demonstration was, of necessity, portable equipment that is often transported, disassembled, and reassembled. For this reason, areas near seals were not as air-tight as they tend to be when assembly and disassembly are infrequent. Some fine particulate losses were observed at the seal where the conveyor dome bolts to the conveyor body. Since the constituents of concern tended to be either volatile or associated with fine particulates, these small losses could affect the material balance. It must be emphasized that losses of this nature did not result in measurable discharges of pollutants to the environment. The contaminant input to the process equipment was so small that is was barely measurable, thus losses that affected material balance closures were trace amounts indeed.

For future work, it is recommended that air emissions losses for metals be performed and that process streams are weighed separately before they are combined for disposal. This should help improve mass balance closure somewhat and should permit calculation of air emissions. As for the other sources of error, problem (4) will be greatly minimized for full scale, permanently installed equipment. The impact of problem (1) can be minimized for highly contaminated sediments, but cannot be corrected by process methodology.

#### Mercury

Following processing, the bulk of the treated residue was free of mercury as were the solids from the second cyclone and the condensate. Mercury content of solids from the first cyclone was approximately the same as the untreated solids. Based on mass balances, however, an average of 79 percent of the mercury in the feed was unaccounted for after processing. Reasons why the fate of mercury is largely unknown are the same as reasons why closure was not obtained for chromium, copper, and lead. As for these other metals, closure can be somewhat improved by weighing each process stream and by quantifying air emissions. Air emissions monitoring will be even more important for mercury, however, because it is a liquid at room temperature and has a relatively high vapor pressure. Again, equipment leaks and errors due to low initial concentrations are inherent in the process and cannot be eliminated in a pilot study of this nature.

#### 3.1.4 Polycyclic Aromatic Hydrocarbons (PAHs) --

Concentrations of 17 individual PAHs were measured both before and after processing, and an attempt was made to assess both removal efficiency and ultimate fate of the removed materials. (Although not confirmed experimentally, it is likely that PAH concentrations increased between dredging and screening due to concentration effects of liquid evaporation.) Where a concentration was reported as "less than detection limit," the detection limit itself was the concentration used in the summation. This approach was used to assure that sediment disposal questions addressed for process scaleup would provide maximum environmental protection. To facilitate this analysis, individual PAH results were summed in two groups.

- . Low molecular weight PAHs, i.e., those
  containing ≤ 3 aromatic rings (naphthalene,
  acenaphthylene, acenaphthene, fluorene, phenanthrene,
  anthracene).
- . High molecular weight PAHs, i.e., those containing > 3 aromatic rings (fluoranthene, pyrene, benzo(a)anthracene, chrysene, benzo(b)fluoranthene, benzo(k)fluoranthrene, benzo(a)pyrene, indeno(1,2,3-cd)-pyrene, dibenzo(a,h)-anthracene, and benzo(g,h,i)-perylene).

Individual compounds were grouped this way primarily because many PAHs with > 3 aromatic rings are either known or suspected carcinogens, thus their fate and removal efficiencies are of particular interest.

PAH removal efficiencies are discussed by group, as follows:

#### Low Molecular Weight PAHs (LMW PAHs)

Results of low molecular weight PAH removal are given in Tables 24A and 24B. A graph of LMW PAH concentration versus final solids temperature is given in Figure 13 (Error bars shown are for standard error of the mean). From these data it is determined that a range of 45 to 90 percent of the PAHs with  $\leq$  3 aromatic rings were removed from the feed material as a result of thermal desorption. Correlation of removal with process temperatures was not significant, as the correlation coefficient relating the two variables was 0.00. It is not known whether a larger energy input would remove the remaining LMW PAHs from the sediment. Future work involving low temperature thermal desorption should include some higher temperatures in order to assess the effect of this process parameter.

As for fate of the removed PAHs, concentration of LMW PAHs in the solids captured by the cyclones is approximately that found in the unprocessed feed. Negligible amounts of LMW PAHs are found in the condensate (average = 0.14 ug/g) and in the air emissions (range is 41.1-213.6 ug/DSCM). Net result is that approximately 74 percent of the PAHs originally present in the feed are not accounted for by mass balance (Table 26A). Closure was not obtained for LMW PAHs. The first three reasons for low percent closure given in section 3.1.3 apply here as well. Additionally, it is speculated that much of the unaccounted-for PAHs sorbed to the carbon. The LMW PAH compounds have an activated carbon: water partition coefficient (Pac) of 10E4.7 to 10E6.8 (Verscheuren, 1983). This range of Pac values suggests a strong tendency for carbon to adsorb airborne PAHs from the exhaust air. For any future work of this nature, it would be well to attempt identifying and quantifying the chemicals adsorbed by the carbon system. Desorption of these materials and their subsequent quantification may be impractical, but if investigation of the problem results in disclosure of a practical methodology, the resulting data will be valuable.

# TABLE 24A LOW MOLECULAR WEIGHT (≤ 3 RING) PAHS IN SEDIMENT (ng/g Dry Weight)

Run Number	A2	A3	B1	В2	C1	C2	С3	D1
PROCESS CONDITIONS	1				. 1		1	1
Feed Rate lbs/hr	346	716	   860	   644	484	635	   862	1 388
Residence Time min.	60	30	45	   60	   90	   60	   45	   90
Max. Sediment Temp. °F	480	380	300	364	392	415	474	1 367
AMPLE POINTS	 	1						
After Dredging (1s)	791	791	926	926	  1390	  1390	  1390	937
After Screening (2s)	11538	990	1 950	  1170	11577	1221	  1221	  9994
Before Thermal Proc. (3s)	1124	11177	842	1367	1428	11164	11039	  2018
After Thermal Proc. (4s)	122	210	349	1.107	211	260	425	   102
Solids from 1st Cyclone (7s)	1947	838	1417	1625	   N/A	   822	  4493	  2689
Solids from 2nd Cyclone (8s)	11105	1   327	  1430	613	  16 <b>63</b>	   N/A	   369	1   576

## TABLE 24B LOW MOLECULAR WEIGHT (≤ 3RINGS) PAHs IN CONDENSATE (ug/L)

Run Number	A2	A3	B1	В2	C1	C2	C3	D1
SAMPLE POINTS *	<u> </u>	!	 	<b>[</b>	 	 		 
After 1st Condenser (9L)	215	361	N/A	20	149	   205	45	65
After 2nd Condenser (10L)	230	1 147	209	68	   N/A	   55	   159	   35

<sup>\*</sup> Process conditions same as for sediment

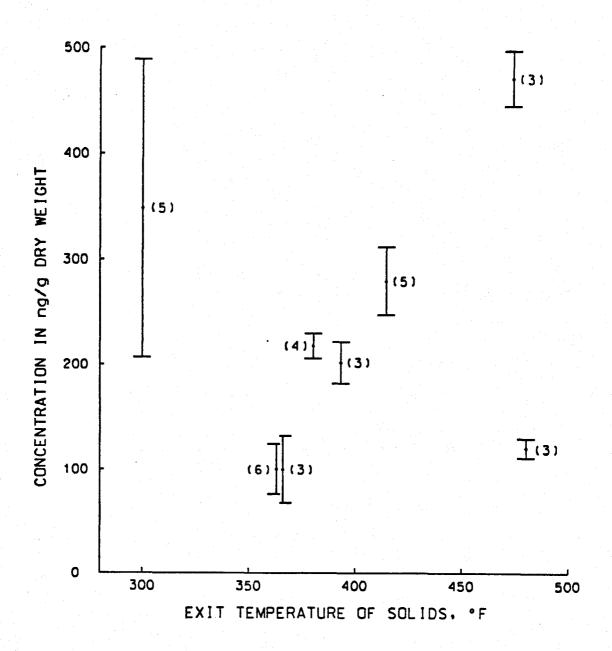
N/A Not Analyzed

Highlighted values are averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

FIGURE 13

CONCENTRATION OF LOW MOLECULAR WEIGHT PAH<sup>S</sup> IN SEDIMENT VERSUS EXIT TEMPERATURE OF SOLIDS

(NUMBERS IN PARENTHESES ARE NUMBERS OF DATA POINTS FROM WHICH THE STANDARD ERRORS WERE CALCULATED)



#### High Molecular Weight PAHs (HMW PAHs)

High molecular weight PAH removal results are given in Tables 25A and 25B. A graph of HMW PAH concentration versus final solids temperature is given in Figure 14 (Error bars shown are for standard error of the mean). Based on these results, it is concluded that 72 percent of all PAHs with carcinogenic potential have been removed by this process (Table 26B). As with other contaminants of concern, HMW PAH removal does not correlate well with maximum sediment temperature. The correlation coefficient relating these variables was 0.00. As was stated for LMW PAH removal, effect of higher temperature on removal should be assessed for future work.

As for the fate of removed HMW PAHs, concentration of these materials in the first cyclone is approximately that found in the unprocessed feed. Concentration of HMW PAHs in the second cyclone is between that in the unprocessed feed and that in the bulk of the treated residue. Negligible amounts of HMW PAHs are found in the condensate (average = 0.15 ug/g) and in the air emissions (range is 8.9E-07 to 2.3E-05 ug/DSCM). Net result is that 71.6 percent of the HMW PAHs in the feed are unaccounted-for by the overall mass balance (Table 25B). The same reasons for low percent closure that applied to LMW PAHs apply here, except that tendency to sorb to carbon is stronger for the HMW PAHs (Pac for HMW PAHs is 10E6.5 to 10E7.0).

#### Total PAHs

Total PAH removal results are given in Tables 27A and 27B. Based on these results, from 43-94 percent of the total PAH contaminants were removed by the thermal desorption process.

Fate of these materials has been discussed previously under sections pertaining to Low Molecular Weight PAHs and High Molecular Weight PAHs and is not repeated here. Tables showing removals of specific PAHs are given in Appendix A.

#### 3.1.5 Solvent Extractables (SE)

Results of solvent extractables removal, as measured by standard oil and grease analysis, are presented in Tables 28A and 28B. A graph of solvent extractable concentration versus solids temperature is given in Figure 15. Error bars shown are for standard error of the mean. From these data it is determined that 17-86 percent of the oil and grease was removed from the residue, with an average removal of 68 percent. SE removal did not correlate well with maximum sediment temperature, as the correlation coefficient relating temperature and removal was -0.45. It is not known whether use of higher temperatures could improve removal. While low correlation of removal with temperature was true for temperatures \leq 480°F, it may be true that some specific additional energy input is required before removal of SE can occur.

TABLE 25A
HIGH MOLECULAR WEIGHT (>3 RINGS)
PAHS IN SEDIMENT
(ng/g Dry Weight)

Run Number	A2	A3	B1	<u>B2</u>	C1	C2	C3	Dl
PROCESS CONDITIONS	1	1		!			!	
Feed Rate 1bs/hr	346	716	860	644	484	635	862	388
Residence Time min.	60	30	1 45	l   60	90	60	   45	l   90
Max. Sediment Temp. °F	1 480	380	300	364	392	415	474	367
SAMPLE POINTS	!	1	!	l . !			 	 
After Dredging (ls)	5424	5424	6604	  6604	  7652	  7652	7652	6479
After Screening (2s)	  7860	  6325	  5787	  7187	  7519	  6600	  6804	  41,871
Before Thermal Proc. (3s)	16990	  5529	5621	  6502	  7198	5985	5952	  9535
After Thermal Proc. (4s)	1 119	1 1425	1664	61	1608	1865	  3549	  450
Solids from 1st Cyclone (7s)	1  4354	   8811	111,679	  7610	   N/A	  8019	!  21,178	  25,499
Solids from 2nd Cyclone (8s)	  1588	] 3938	  2300	l  4349	  6943	N/A	  3043	  6744

## TABLE 25B HIGH MOLECULAR WEIGHT (>3 RINGS) PAHs IN CONDENSATE (ug/L)

Run Number	A2	А3	B1	В2	C1	C2	С3	D1
SAMPLE POINTS *	   	 	 	[ 	 	   	1	
After 1st Condenser (9L)	156	235	N/A	!   7	1 129	   218	82	111
After 2nd Condenser (10L)	   268 	   190 	   245 	l   59 	   N/A 	   75 	   220 	   42 

#### N/A Not Analyzed

Highlighted values are averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

<sup>\*</sup> Process conditions same as for sediment

#### TABLE 26A SUMMARY OF CALCULATIONS LOW MOLECULAR WEIGHT PAHS

#### <--- MILLIGRAMS OUT --->

BIN	MGMS IN	RESIDUE	CONDENSATE	PERCENT REMOVED
A2	568	93	0.08	83.7
AZ	300	73	0.00	93.7
A3	632	82	0.11	87.1
B1	290	145	0.06	50.0
B2	737	141	0.00	80.9
C1	554	107	0.06	80.6
C2	511	122	0.08	76.1
<b>C</b> 3	442	242	0.02	45.3
D1	620	65.1	0.02	89.5
	· · · · · · · · · · · · · · · · · · ·		AVG	74.2

#### TABLE 26B SUMMARY OF CALCULATIONS HIGH MOLECULAR WEIGHT PAHS

#### <--- MILLIGRAMS OUT --->

BIN_	MGMS IN	RESIDUE	CONDENSATE	PERCENT REMOVED
A2	3530	138	0.06	96.1
A3	2969	958	0.07	67.7
B1	1939	782	0.07	59.7
B2	3504	305	0.00	91.3
C1	2793	725	0.05	74.1
C2	2627	914	0.09	65.2
С3	2487	1436	0.03	42.2
D1	<b>2</b> 927	734	0.03	74.9
			AVG	71.4

FIGURE 14

CONCENTRATION OF HIGH MOLECULAR WEIGHT PAH<sup>S</sup> IN SEDIMENT VERSUS EXIT TEMPERATURE OF SOLIDS

(NUMBERS IN PARENTHESES ARE NUMBERS OF DATA POINTS FROM WHICH THE STANDARD ERRORS WERE CALCULATED)

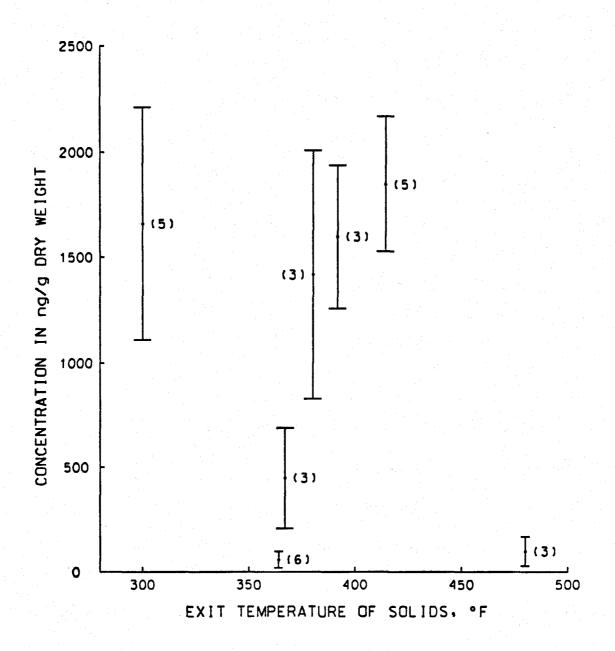


TABLE 27A
TOTAL PAHS IN SEDIMENT
(ng/g dry weight)

Run Number	A2	A3	B1	B2	C1	C2	C3	D1
PROCESS CONDITIONS	<u> </u>				 	! !		1
Feed Rate lbs/hr	   346	716	860	644	1 484	   635	862	   388
Residence Time min.	60	30	45	l   60	90	l   60	45	90
Max. Sediment Temp. °F	480	380	300	!   364	392	415	474	367
SAMPLE POINTS		, 	1	! 	! !	[   		
After Dredging (ls)	6215	6215	7530	7530	1   9042	9042	9042	7416
After Screening (2s)	9398	7315	6737	8357	1   9096	7821	8025	51865
Before Thermal Proc. (3s)	8114     8114	6706	6463	   7869	8626	7149	6991	11553
After Thermal Proc. (4s)	241	1635	2013	168	1   1819	2125	3974	552
Solids from 1st Cyclone (7s)	6301	9649	13096	9235	N/A	8841	25671	5238
Solids from 2nd Cyclone (8s)	2693    2693	4265	3730	4962	8606	N/A	3412	7320

TABLE 27B
TOTAL PAHS IN CONDENSATE
(ug/L)

Run Number	A2	A3	В1	В2	C1	C2	C3	D1
SAMPLE POINTS *		 		<u> </u>		i		1 !
Liq. from 1st Condenser (9L)	371	596	N/A	l   20	278	423	127	176
Liq. from 2nd Condenser (10L)	498	337	454	   127	N/A	130	379	   77

N/A - Not Analyzed

\* Process conditions same as for sediment

Highlighted values are averages of multiple (3-5) measurements.

TABLE 28A
SOLVENT EXTRACTABLES IN SEDIMENT (ug/g Dry Weight)

Run Number	A2	A3	B1	B2	C1	C2	С3	D1
PROCESS CONDITIONS	 	1		 	 	!	1	<u> </u> ! ;
Feed Rate 1bs/hr	346	716	860	644	   484	   635	862	388
Residence Time min.	60	30	1 45	60	   90	60	45	90
Max. Sediment Temp. °F	480	380	300	364	392	415	474	367
SAMPLE POINTS				1	!			
After Dredging (ls)	1415	1415	1619	1 1619	2261	2261	2261	1707
After Screening (2s)	11820	1766	2006	2082	  3995	1761	2399	2416
Before Thermal Proc. (3s)	2282	2250	2056	1754	2109	2011	4254	2391
After Thermal Proc. (4s)	234	550	474	220	562	510	3618	646
Solids from 1st Cyclone (7s)	2391	2443	3770	1231	N/A	2416	4389	5368
Solids from 2nd Cyclone (8s)	   696 	  1901 	  1899 	   449 	2539	   N/A	646	965

TABLE 28B
SOLVENT EXTRACTABLES IN CONDENSATE (mg/L)

Run Number	A2	А3	B1	В2	C1	C2	С3	D1
SAMPLE POINTS *		 			1	 	 	!
After 1st Condenser (9L)	284	112	l N/A	62	90	82	1113	57
After 2nd Condenser (10L)	1110	214	29	70	N/A	30	16	71

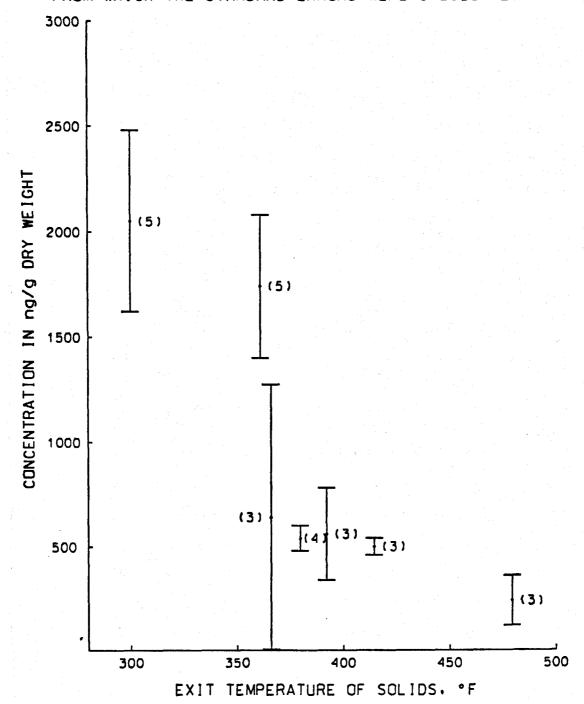
#### \* Process conditions same as for sediment

N/A - Not Analyzed

Highlighted values are averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

FIGURE 15
CONCENTRATION OF SOLVENT EXTRACTABLES IN SEDIMENT
VERSUS EXIT TEMPERATURE OF SOLIDS

(NUMBERS IN PARENTHESES ARE NUMBERS OF DATA POINTS FROM WHICH THE STANDARD ERRORS WERE CALCULATED)



As for the fate of oil and grease, it tends to be concentrated in the fines captured by the first cyclone. Still, 68 percent of the removed oil and grease is unaccounted for (Table 29). It is known that negligible amounts appear in the condensate and in the fines from the second cyclone, however, amounts sorbed on carbon and amounts in air emissions were not quantified.

Because solvent extractables analysis is a cheap, relative easy measurement, the possibility of using solvent extractables removal as a surrogate parameter to predict removal of polycyclic aromatic hydrocarbons was considered. If correlation between SE removal and PAH removal were high, a single measurement could replace 16 individual measurements for estimating PAH removal. Using the calculation protocol in 6.2.2.2, the correlation coefficient relating SE removal and total PAH removal was 0.77. This value suggests that use of SE removal as a surrogate parameter for PAH removal may be possible. Since 80 percent of solvent extractables are unaccounted for in the material balance, however, this concept requires further investigation.

#### 3.1.6 Total Organic Carbon (TOC)

Total organic carbon is a surrogate parameter that includes all organic carbon oxidizable by persulfate in the presence of UV light. The oxidized carbon is thus quantified by measuring the evolved carbon dioxide. Given this definition, it is clear that the total organic carbon (TOC) measured in the sample represents the carbon from: SE, PAHs, PCBs, pesticides, other (unidentified) semivolatiles, and volatiles (in untreated material). In addition, some portion of the naturally occurring humic and fulvic acids will oxidize during the time of the analytical test run, and this portion of the organic acids will contribute to total measured carbon. (While humic and fulvic acids are theoretically all oxidizable, the typical Dohrmann instrument will "time out" before the oxidation is complete). Effect of thermal desorption on TOC is given in Tables 30A and 30B. A graph of TOC concentration versus final solids temperature is given in Figure 16. (Error bars shown are for standard error of the mean.)

Removals of ToC ranged from 5 percent to 35 percent, indicating that most of the compounds contributing to ToC (Table 31) were not removed at the process temperatures employed. ToC was examined as a potentially predictive surrogate parameter for several classes of organic compounds. A reasonably large correlation coefficient relates removal of HMW PAHs and ToC removal, as evidenced by the following correlation coefficients (r). Caution must be exercised in using ToC removal to predict HMW PAH removal, however, because 85 percent of the PAHs were removed with only 25 percent of the ToC.

## TABLE 29 SUMMARY OF CALCULATIONS SOLVENT EXTRACTABLES

#### <--- GRAMS OUT --->

	and the second second			PERCENT
BIN	GRAMS IN	RESIDUE	CONDENSATE	REMOVED
A2	1152	163	113	85.9
A3	1208	349	NO DATA	71.2
B1	1184	229	8	80.7
B2	1137	218	12.5	80.8
C1	818	224	0	72.6
C2	883	254	0	71.2
C3	1808	1500	0	17.1
D1	734	253	0	<u>65.5</u>
			AVG	68.1

TABLE 30A
TOTAL ORGANIC CARBON IN SEDIMENT
(mg/g Dry Weight)

Run Number	_A2	A3	B1	В2	C1	C2	С3	D1
PROCESS CONDITIONS			[		[    -	[ ]	[	1
Feed Rate lbs/hr	346	716	l   860	   644	1   484	   635	   862	I ! 388
Residence Time min.	60	30	   45	60	   90	   60	45	i   90
Max. Sediment Temp. °F	480	380	300	364	1   392	415	474	1   367
SAMPLE POINTS					]   		· 	   !
After Dredging (ls)	18.6	18.6	18.4	18.4	17.7	17.7	17.7	17.6
After Screening (2s)	18.4	19.0	18.2	18.7	18.0	17.7	18.4	18.2
Before Thermal Proc. (3s)	18.6	19.0	18.9	19.1	18.3	18.0	17.5	18.5
After Thermal Proc. (4s)	12.1	14.7	14.2	10.3	15.2	15.4	16.6	13.2
Solids from 1st Cyclone (7s)	14.8	17.2	17.1	15.9	20.6	16.6	20.5	18.4
Solids from 2nd Cyclone (8s)	10.4	14.7	16.9	15.3	14.6	N/A	15.9	15.3

TABLE 30B
TOTAL ORGANIC CARBON IN CONDENSATE
(mg/g liquid)

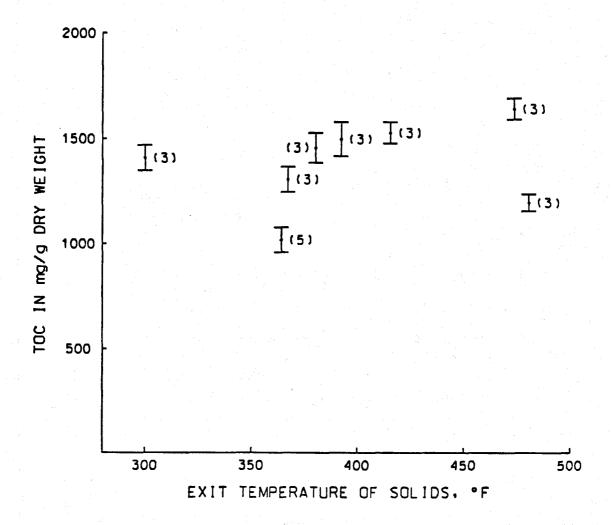
Run Number	A2	A3	<u>B1</u>	B2	C1	C2	C3	D1
SAMPLE POINTS *						    -	<u> </u>	
After 1st Condenser (9L)	1 1.58	1.58	.85	.90	.83	.72	.43	1 .70
After 2nd Condenser (10L)	1 .85	.51	. 53	.75	.28	.25	1.17	1 .37

<sup>\*</sup> Process conditions same as for sediment

N/A Not Analyzed

Highlighted values are averages of multiple measurements. Averages were calculated using 3-5 individual measurements.

FIGURE 16
TOC (mg/g SOLIDS) VERSUS EXIT TEMPERATURE OF SOLIDS
(NUMBERS IN PARENTHESES ARE NUMBERS OF DATA POINTS
FROM WHICH THE STANDARD ERRORS WERE CALCULATED)



#### TABLE 31 SUMMARY OF CALCULATIONS TOC

<	LBS	OUT	>
\	பபல	OUL	

BIN	LBS IN	RESIDUE	CONDENSATE	PERCENT REMOVED
A2	18.7	12.1	1.4	35.3
A3	23.3	12.5	0.4	33.5
В1	18.9	14.2	NO DATA	24.9
B2	19.1	19.1 10.2		46.6
Cl	18.3	15.2	0.5	16.9
C2	18.0	15.4	0.4	14.4
С3	17.5	16.6	0.3	5.1
D1	18.5	13.2	0.5	28.7
			AVG	25.7

Organic Material	r
LMW PAHs	0.58
HMW PAHs	0.81
Total PAHs	0.77
Solvent Extractables	0.71

Fate of TOC is not discussed here, as the "fate" of a surrogate parameter is not a meaningful concept. What should be emphasized is that it was possible to account for an average of 77 percent of the initial TOC and that most of it remained with the sediment.

#### 3.1.7 Polychlorinated Biphenyls (PCB)

Analyses were performed before and after processing for four commercial mixtures of PCB (Aroclors): 1242, 1248, 1254, 1260. These are the Aroclors that could be present in the Buffalo River based on site history, thus a total of the individual concentrations of these Aroclors is considered to be total PCB. Total PCB data are presented in Tables 32A and 32B. Data in Tables 32A and 32B are limited primarily to information associated with performance of the thermal processor itself; data associated with more remote parts of the process were not analyzed (N/A) due to cost constraints.

Percent PCB removals were calculated using data in Table 32, and these results are presented in Table 33. Removals ranged from 0 to 100 percent. No correlation was observed between maximum sediment temperature and PCB removal (r = -0.05).

TABLE 32A
TOTAL PCB IN SEDIMENT
(ng/g dry weight)

Run Number	A2	A3	B1	B2	<u>C1</u>	C2	C3	D1
PROCESS CONDITIONS	1	 		<u> </u>	\ !	. <b> </b> 		 
Feed Rate 1bs/hr	346	   716	860	644	484	635	862	388
Residence Time min.	60	1   30	45	60	90	60	45	90
Max. Sediment Temp. °F	480	1   380	300	364	392	415	1 474	367
SAMPLE POINTS	! 	   						
After Dredging (ls)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
After Screening (2s)	   N/A	   N/A	ND	N/A	1113	N/A	N/A	N/A
Before Thermal Proc. (3s)	ND	ND	184	351	232	209	163	286
After Thermal Proc. (4s)	ND	I   ND	94	319	17	122	109	ND
Solids from 1st Cyclone (7s)	I   ND	402	   589	1 158	   N/A	284	738	674
Solids from 2nd Cyclone (8s)	I ND	67	1 156	I ND	N/A	N/A	ND	N/A

TABLE 32B
TOTAL PCB IN CONDENSATE
(ng/L)

Run Number	A2	A3	B1	B2	<u>C1</u>	C2	C3	D1
SAMPLE POINTS *			!					
Liq. from 1st Condenser (9L)	24698	27343	N/A	ND	25956	39269	5814	l ND
Liq. from 2nd Condenser (10L)	66186	69074	27605	ND	1 12692	17890	19471	ND

N/A - Not Analyzed '

ND - None Detected

Highlighted values are averages of multiple (3-5) measurements.

<sup>\*</sup> Process conditions same as for sediment

### TABLE 33 SUMMARY OF CALCULATIONS PCB IN SOLIDS

<---> MG OUT --->

BIN	MG IN	RESIDUE	CONDENSATE	PERCENT REMOVED
A2	ND	ND	ND	:
<b>A</b> 3	ND	ND	ND	
B1	63.5	35.3	1.4	44.4
B2	189.2	267.3	0.2	0.0
Cl	90.0	6.7	N/A	92.6
C2	91.8	52.8	0.6	42.5
C3	69.3	44.8	2.6	35.4
D1	87.8	<b>0</b>	1.1	100.0

#### 3.1.8 Solidification/Stabilization of Treated Residue

Following application of the RETEC thermal desorption technology, the U.S. Army Corps of Engineers solidified selected batches of treated sediment residue with cement. The intent of this action was to curtail mobility of the pollutants remaining in the residue. Four distinct ratios of cement-to-residue ratios were employed: 0.1, 0.2, 0.4, and 0.6. Solidified residues were cured for approximately one month and then tested to determine unconfined compressive strength and degree of pollutant attenuation for Cr, Cu, Hg, Pb, and ToC as measured by either the toxicity characteristic leach procedure (TCLP) or the sequential batch leach test (SBLT). (TCLP is performed in a single leach step while SBLT is performed using 4 sequential extractions.) Results of this work appear in Tables 34 through 36.

From these tests it is concluded that unconfined compressive strength varied directly as cement: residue ratio, indeed the correlation coefficient relating the two variables was 0.994. Additionally, assessments of results for TCLP and SBLT follow:

#### TCLP:

- . Because treated, unsolidified sediment contained no mercury, it was not possible to determine whether solidification could attenuate the mobility of mercury.
- . Solidification of the treated residue resulted in an 89 percent reduction in extract Pb concentration. Reduction was not correlated with cement: residue ratio.

TABLE 34
SOLIDIFICATION/STABILIZATION UNCONFINED
COMPRESSIVE STRENGTH (UCS) RESULTS

Run No.	Cement to - Residue Ratio	USC (1bs/sq in.)	Average (1bs/sq in.)	Std. Dev. (1bs/sq in.)	Coefficient of Variation (Percent)
B1 - B3	0.1	208			
B1 - B3	0.1	203	250	77	30.7
B1 - B3	0.1	338			•
		400			
A2	0.2	433			
A2	0.2	410	388	48	12.3
A2	0.2	323			
<b>A</b> 2	0.2	384			
. A3	0.4	925			
A3	0.4	836	898	59	6.6
A3	0.4	968			
A3	0.4	865			
B2	0.6	1277			
В2	0.6	1115	1212	86	7.1
В2	0.6	1245			· • • • • • • • • • • • • • • • • • • •

DATA SOURCE: Corps of Engineers Waterways Experiment Station

TABLE 35
RESULTS OF RESIDUE STABILIZATION

### CONCENTRATIONS OF EXTRACTS FROM TOXICITY CHARACTERISTIC LEACH PROCEDURE (TCLP)

		CEMENT TO	co	NCENTR	ATION :	IN ug/L	$1b/IN^2$	
	BIN R	ESIDUE RATIO	Cr	Cu	Hg	Pb	UCS	pН
BEFORE	A2		0.27	4.2	ND	2.57		6.21
STABILIZATION	A3		0.71	15.1	ND	6.55		6.10
	B2		0.13	2.4	ND	1.93		6.23
	B1/B3		0.69	13.6	ND	6.16		6.10
AFTER	A2	0.2	36.5	42.3	ND	ND	388	10.94
STABILIZATION	A3	0.4	44.4	12.0	ND	ND	898	11.67
	В2	0.6	17.9	13.1	ND	.72	1212	12.06
	B1/B3	0.1	2.0	30.8	.008	1.07	250	6.61

TABLE 36 SEQUENTIAL BATCH LEACH TEST (SBLT) FOR METALS

		CEMENT TO	CR	CR (ug/L)	3	Cu (ug/L)	Hg (ug/L)	17/b	(1/6n) qd	(1/6	
	BIN	RESIDUE RATIO	Avg. Value 1 <u>s</u> t FR.	Avg. Value ΣFR. 2-4	Avg. Value 1st FR	Avg. Value Avg. Value Avg. Value E FR. 2-4 1st FR E FR. 2-4	Avg. Value 1st FR	Avg. Value E FR 2-4	Avg. Value Avg. Value Avg. Value Avg. Value 1st FR Σ FR 2-4 1st FR Σ FR 2-4	Avg. Value E FR 2-4	
	,			o c	•		ş	00101	S	7 2	
	Ą		*. •	0.0	:	3.6	9	200.0	è	ŗ	
STABILIZATION	Ą		1.0	0.7	20.1	8.7	0.00149	0.00356	2	9.3	
	B2		æ	2	2.4	SX SX	0.0047	9	Q	9	
	81/83	•	9.0	1.9	4.7	10.4	0.00054	0.00320	9	7.2	
	A2	0.2	8.4	22.4	60.2	83.7	0.00101	0.00204	8.1	11.0	
STABILIZATION	A3	7.0	12.2	34.9	15.1	17.3	0.00030	0.00126	7.1	15.1	
	B2	9.0	11.8	44.7	16.9	24.5	0.00026	0.00094	8.9	16.7	
	81/83		6.1	12.1	125.4	234.2	0.00104	Ð	13.4	8.2	
	<b>A</b> 2	0.2	+8.0	+21.6	+59.1	+78.5	+0.00101	+0.00103	8.1	+7.6	
	Α3	7.0	+11.2	+34.2	-5.0	+8.6	-0.00419	-0.00230	7.1	+5.8	
	82	9.0	+11.8	444.7	+14.5	+24.5	-0.00021	+0.000.0+	6.8	+16.7	
	B1/8C	0.1	+5.5	+10.2	+120.7	+223.8	+0.00050	-0.00320	13.4	+1.0	

DATA SOURCE: Referenced Battelle Report

. Leachability of Cu and Cr were increased by solidification. Leachability is not correlated with cement: residue ratio, thus the cause of increased Cu and Cr leaching in solidified material is unknown.

#### SBLT:

- . Attenuation of TOC mobility in solidified residue is variable, as measured by Steps 1-4 of the SBLT leach test. These results are shown graphically in Figure 17. In two cases mobility was attenuated and in two cases it was enhanced. These results do not correlate with cement: residue ratio, thus the reason for this pattern is unknown.
- . Mobility of all metals but mercury was generally enhanced by the stabilization procedure. Mercury results were variable.

#### 3.2 FULL SCALE IMPLEMENTATION

The following discussion provides a description and cost estimate for a full scale remediation of contaminated sediments using the thermal desorption process. Two separate cost estimates were made for sediment remediation involving 10,000 and 100,000 cubic yards of material. These quantities were believed to represent feasible cleanup scenarios for areas with heavily polluted sediments. Due to the anticipated high cost per cubic yard of such a cleanup it did not seem reasonable that millions of cubic yards or several 100's of thousands of cubic yards would be remediated using the thermal desorption process.

#### 3.2.1 Thermal Desorption Remediation

The following discussion provides a description of the thermal desorption system and a cost estimate for the remediation of 10,000 and 100,000 cubic yards of contaminated sediments. In preparing the estimates for sediment treatment, it was assumed that all processing would be conducted at a centralized facility on-site and that the moisture content of the sediments would be adjusted to approximately 60 percent by weight to facilitate handling and treatment operations.

The application of the thermal desorption technology provides for the volalitized components to be condensed and separated into concentrated streams. The aqueous condensate would be treated on-site and combined with the treated solids for dust control, while the concentrated organic condensate would be transported off-site for disposal in a permitted facility.

#### 3.2.1.1 Full-Scale Treatment System--

A nominal processing rate of approximately 41 tons per day (34 cubic yards at 1.2 tons per yard) was assumed. The processing system would have a rated capacity of 2.0 tons per hour for a three shift-per-day operation. A system utilization rate of 85 percent was assumed to provide time for routine maintenance and repair. The proposed throughput assumes a solids residence time of 120 minutes for the full-scale remediation based on the results of the pilot scale demonstration which

FIGURE 17
RESULTS OF RESIDUE STABILIZATION: TOC ANALYSIS
OF EXTRACTS FROM SEQUENTIAL BATCH LEACH TEST (SBLT)

FIGURE 17A: BIN A2 CEMENT: RESIDUE RATIO = 0.2

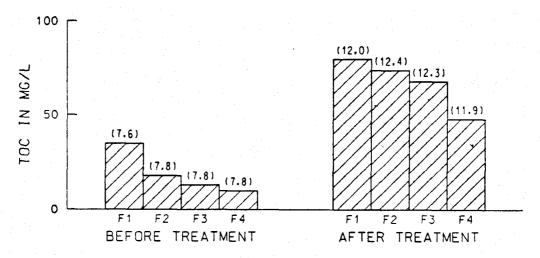
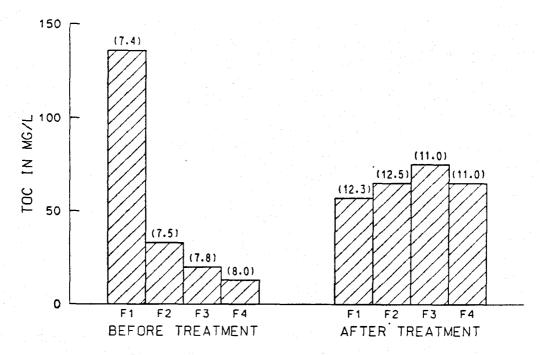


FIGURE 17B: BIN A3 CEMENT: RESIDUE RATIO = 0.4



F# = FRACTION NUMBER
NUMBER IN PARENTHESIS IS PH OF ASSOCIATED LEACHATE

FIGURE 17C: BIN B2 CEMENT: RESIDUE RATIO = 0.6

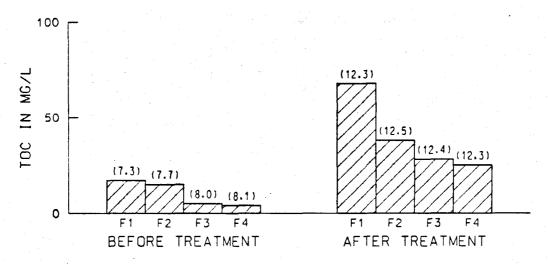
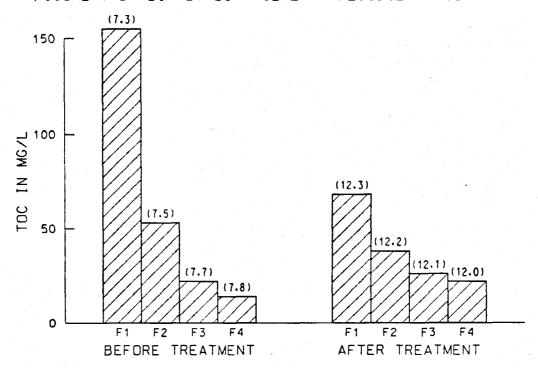


FIGURE 17D: BIN B1/B3 CEMENT: RESIDUE RATIO = 0.1



F# = FRACTION NUMBER NUMBER IN PARENTHESIS IS PH OF ASSOCIATED LEACHATE

indicated that the extended residence would be required to ensure the removal of organic contaminants.

material Feed - The moisture content of the dredged material would be adjusted to approximately 60 percent prior to screening and treatment. The addition of water and associated mixing would be conducted on a semi-continuous basis. Agitation of the material would be conducted using propeller agitator mixers. Aqueous condensate from the process would be used for make-up water. The sediments would then be pumped from the tanks to the processor at a flow consistent with the proposed processing rate, approximately 6 gallons per minute. The inlet pump line and the pump effluent would be screened to exclude over-sized material or debris. Accumulated oversized material would be removed from the bottom of the tanks during routine maintenance. A positive displacement-style pump would be utilized in transferring the sediments from the tank to the treatment unit.

Thermal Processor - The initial processor in the system is designed to remove moisture and organics from the feed material and reduce the volume of the material for subsequent disposal. A model D-24-24 screw dryer manufactured by the Denver Equipment Company, with a capacity of 2.0 tons per hour, would be used in the processor. The Denver processor uses a contained, non-contact circulating heat transfer fluid to raise the temperature of the solids being treated. Based on results of the pilot scale demonstration, it was assumed that final solids temperatures of 600 to 700° F would be required to ensure the complete removal of organics. The heat transfer fluid for the full scale remediation would be COASTAL HI-TEC salt, which has a maximum operating temperature of 1,100° F. The heat transfer media would be heated with an oil fired system having a capacity to circulate fluid at a rate of 200 gallons per minute (gpm) and provide approximately 3.0 million BTU/per hour to the processor (Remediation Technologies, Inc., 1992).

The final component of the system would be designed to cool the solids to a temperature of 140° F for subsequent handling. The cooling screw would require approximately 20 gpm of cooling water.

It is believed that the build up of feed material around the thermal processor augers could be prevented during a full scale operation by maintaining a feed moisture content of approximately 60 percent. If it were found that the caking of material persisted, the Holo-Flite Screw Processor System could be replaced with a system that continuously self cleans the internal surfaces of the processor.

The off-gas handling system would consist of a cylone, quench chamber, indirectly-cooled condenser and activated carbon beds. The off gas control system would be designed to accommodate an off-gas flow rate of approximately 2500 cubic feet per minute at 600° F, and "worst case" moisture and organic loading of 2400 pounds per hour and 4 pounds per hour respectively. A cyclone particulate removal system would remove any fine solid particles (>10 um) which may be entrained with the off-gases.

These solids would be removed and combined with the feed material for reprocessing. The volatilized organics and moisture would be condensed into a combined liquid stream. The condenser would be designed to achieve 90 percent removal of organics and moisture in the gas. Separation of the organics and aqueous condensate streams would be enhanced by the use of a coalescing plate separator. The condensed organics would be disposed of off site.

Approximately 5 gpm of aqueous condensate would be generated as a result of treatment operations. One half of the condensate would be used to dilute the dredged sediments in the mixing tanks, while the remaining volume of condensed water would be treated on site using biological treatment or activated carbon. After the liquid and particulate are removed from the purge gas stream the gas would be treated to remove residual volatile organics. Treatment would consist of filtration through granulated activated carbon beds.

#### 3.2.1.2 Cost Estimate for Sediment Remediation--

Cost estimates for the remediation of 10,000 and 100,000 cubic yards of contaminated sediment using the thermal desorption technology were prepared. The estimated operating costs (+/- 20 percent) for treating the contaminated sediments on site are shown in Tables 36 and 37. Unit prices were determined using a processing rate of 890 tons (612 cubic yards of "as-dredged" material (40 percent moisture) per month, assuming a 24 hour per day operation with an 85 percent system utilization rate. estimate includes costs for all mobilization/demobilization, thermal treatment, associated analytical activities, on-site treatment of the aqueous condensate, and the off-site disposal of the organic condensate stream. Costs associated with sediment excavation and transport to the treatment site were not included. These costs can be expected to be less than 10 percent of the associated remediation cost discussed below. Engineering and design work would add approximately 10 percent to the project cost, as would construction management. Therefore, total project cost would be roughly 1-1/3 times the remediation cost shown below.

Remediation of 10,000 Cubic Yards - Treatment costs for processing this volume of waste were estimated at \$535 per cubic yard, with the work being completed in approximately 16 months. Mobilization and demobilization costs were estimated to be \$500,000 while the monthly equipment charge was estimated at \$132,000. The equipment charge was calculated to provide a 25 percent return on capital investment over the duration of the contract.

Field labor and utilities were estimated to make up approximately 30 percent of the total treatment cost. The labor costs includes 4 workers per shift and three shifts per day at an average hourly rate of \$35, including overhead. Utility costs are based upon the fuel requirements to maintain the temperature of the heat transfer media during treatment, and the electrical requirements of the system (200 kw, 480 v, 225 amp).

Maintenance and activated carbon disposal comprise less than 5 percent of the cost. Activated carbon disposal/replacement was estimated at \$1000 per month. Carbon would be recharged and

reused until its useful life was exhausted. Spent carbon would be disposed of by landfilling or incineration if required. The off-site disposal of the condensated liquid organics was conservatively estimated at \$1000 per ton while the on-site treatment of the aqueous condensate was estimated to cost \$0.02 per gallon. This cost equates to approximately \$8 per ton of

dredged sediment. The total cost for processing 10,000 cubic yards of sediments was estimated at \$5,350,000 and is shown in Table 37.

Remediation of 100,000 Cubic Yards - The cost estimate for treating 100,000 yards of contaminated sediments includes the use of four parallel treatment systems to allow the completion of the remediation in a reasonable time period. As discussed previously, each system would process 612 cubic yards of "asdredged" sediments per month, assuming a 24 hour per day operation with an 85 percent system utilization rate. With this treatment train, the sediment remediation work could be completed within 41 months at an estimated unit cost of \$352 per cubic yard. Mobilization and demobilization costs were estimated to be \$1,200,000, or \$12 per cubic yard of sediment. Other operating expenses such as fuel, maintenance and waste disposal will have unit costs similar to those discussed under the smaller treatment scenario.

Monthly equipment charges for the four treatment units were estimated to be \$363,000, resulting in a monthly charge per individual unit that is significantly less than the monthly charge for the single unit anticipated for the remediation of 10,000 cubic yards of sediment. This is due to the increased period of time, 41 verses 16 months, available to recover the capital investment. The total cost for processing 100,000 cubic yards of contaminated sediments was estimated to be \$35,200,000 and is shown in Table 38.

Variations in the moisture content can impact the thermal requirements, while variations in the organic content of the feed sediment would primarily affect the pricing of services by changing the rate of activated carbon usage. RETEC does not believe that any of these factors or material processing requirements would significantly affect the throughput of the system or the estimated cost of treatment (Remediation Technologies, Inc., 1992).

#### 3.3 CONCLUSIONS AND RECOMMENDATIONS

#### 3.3.1 <u>Conclusions</u>

A review of the results from the program provides the following conclusions related to material composition, material handling, effectiveness of treatment, and process operation.

1. Material Handling - The dredged materials were relatively free of debris or over-sized material which would adversely affect the processing of the sediments during full-scale implementation. Some problems were caused by the physical

TABLE 37

COST ESTIMATE FOR REMEDIATING 10,000 CUBIC YARDS OF SEDIMENT

DESCRIPTION	ESTIMATED COST
Mobilization and Demobilization (Treatment) Equipment Rental Utilities: Fuel Electricity: Cooling Misc. Operating Field Labor Maintenance Activated Carbon Other Operating Costs Disposal of Organic Condensate	\$ 500,000 2,150,000 250,000 320,000 160,000 1,630,000 80,000 20,000 160,000
and Treatment of Aqueous Condensate	80,000
TOTAL	\$5,350,000
TOTAL COST PER CUBIC YARD	\$ 535

DATA SOURCE: Referenced RETEC, Inc. Report

TABLE 38

COST ESTIMATE FOR REMEDIATING 100,000 CUBIC YARDS OF SEDIMENT

DESCRIPTION	ESTIMATED COST
Mobilization and Demobilization Equipment Rental Utilities: Fuel Electricity: Cooling Misc.	\$ 1,200,000 14,900,000 2,500,000 3,200,000
Operating Field Labor Maintenance Activated Carbon Other Operating Costs Disposal of Organic Condensate and Treatment of Aqueous Condensate	1,000,000 9,600,000 800,000 200,000 1,000,000
TOTAL	\$35,200,000
TOTAL COST PER CUBIC YARD	\$352

DATA SOURCE: Referenced RETEC, Inc. Report and Corps of Engineers, Buffalo District

characteristics of the material: (1) Sediments can cause conveyance problems for solids handling systems such as conveyors, bucket elevators, and screw conveyors due to their cohesive properties. However, the feed material was determined to be readily pumpable at moisture contents above 45 percent by (2) Dried sediments can collect in the processor, weight. eventually preventing the rotation of the screw auger. Results from the pilot scale demonstration indicate that this problem was more pronounced when feed material with lower moisture contents were being processed. Minimal problems were encountered when processing material with a moisture content in excess of 50 percent by weight. From the limited data available it was not clear if this was due to a physical change in the properties of the solids or is the result of a lower mass feed rate of solids due to dilution with water.

- Process Operations After initial optimization of the material handling system, the technology operated without significant problems and provided the following information. general, the heat transfer characteristics for the sediment were low, resulting in exit solids temperatures that were significantly lower than anticipated, 300 to 535°F versus 700°F. Residence times of 60 minutes were appropriate to achieve moisture removal/mass reduction, while consistent organic removal required treatment for periods in excess of 90 minutes. Particulate buildup in the off-gas control system was not a significant problem due to the high moisture content of the feed One of the operating results was the poor separation material. of the organic and aqueous condensates due to the dilute nature of the oil stream. RETEC attempted to separate the streams by "controlled condensation," separation on the basis of condensation temperature. This proved to be largely unsuccessful, probably due to the low concentration of organics versus moisture in the waste. Results from several test runs indicated that the aqueous and organic streams generally contained low concentrations of volatile organics which were concentrated to some degree in the organic stream. Effective separation of such a dilute stream would require the use of a physical separator.
- 3. Feed material containing 44-56 percent solids was successfully pumped and dryed to a solids content  $\geq$  95 percent.
- 4. Removal levels for constituents of concern were contaminant specific. Ranges of removal for each constituent of concern were as follows:
  - a. Mercury: 9-100%
  - b. Low molecular weight polycyclic aromatic hydrocarbons: 45-90%
  - c. High molecular weight polycyclic aromatic hydrocarbons: 42-96%
  - d. Oil and grease: 17-86%
  - e. Total organic carbon (TOC): 5-35%

f. Polychlorinated biphenyls (PCBs): 0-100%

g. Chromium: 0-9%h. Copper: 0-11%i. Lead: 0-13%

- 5. Removal of organic materials was not strongly correlated with measured process conditions such as maximum sediment temperature, residence time, and percent moisture in the feed. Some other parameter is controlling removal.
- 6. Since copper, chromium, and lead remain with the treated sediment, the dryed sediment is a potential candidate for remediation by a stabilization/solidification technology. While stabilization/solidification with a cementitious process was not successful for chromium and copper when the material was ground up, it is possible that chromium and copper leachability would be negligible if the unground material was tested by exposure to normal weathering processes.
- 7. Solvent extractables and "TOC" are both potentially usable as surrogate parameters for predicting removal of high molecular weight PAHs.
- 8. Air emissions were measured for PAHs, dioxins, furans, and PCBs, and were extremely low:

Low molecular weight PAHs: 1.6 - 18.0 mg/hour High molecular weight PAHs: 0.4 - 8.6 mg/hour Dioxins: 0.005 - 0.017 mg/hour Furans: 0.000 - 0.032 mg/hour PCBs: 1.3 - 2.4 mg/hour

- 9. It is of interest to determine the percent of each hazardous material entering the processor that was released to the atmosphere via air emissions. This value was quantifiable for PAHs only;  $\leq$  0.004 percent of the PAHs in the feed material were discharged via air emissions.
- 10. Stabilization/solidification of the treated residue resulted in an 89 percent attenuation of the mobility of lead. Leachability of copper and chromium were increased.
- 11. Fate of the removed materials was not determined in many cases. Factors contributing to this problem were (1) the combining of stream rates rather than taking individual weights, (2) slight particulate losses at the processor seals, (3) processing of relatively clean sediment, (4) exclusion of metals analysis in the air sampling, and (5) failure to quantify materials captured by carbon.

#### 3.3.2 Recommendations/Lessons Learned

The following recommendations are made for performing future pilot studies in thermal desorption.

1. Operation at higher temperatures should be considered to

assess whether higher removal levels can be achieved for semi-volatiles and other organic materials.

- 2. Individual weights of each stream should be obtained rather than combined weights (e.g., Solids from each cyclone should be weighed and recorded, as should the treated residue. The solids should not all be combined and then reported as a single weight.). The taking of individual weights will make it possible to determine the fate of each contaminant.
- 3. Analysis of air emissions should include analysis for metals.
- 4. Sediments with greater contaminant levels should be selected for treatment. A large percent error is inherent in measurements and mass balances for low concentrations of contaminants.
- 5. Use of solvent extractables and/or "Total Organic Carbon" as surrogate parameters for estimating removal of high molecular weight PAHs should be further investigated.
- 6. Analysis of activated carbon for organics and metals should be considered and carried out. PAHs and PCBs are likely partitioning to the carbon in the emissions system, because of the fundamental nature of activated carbon to adsorb organics.
- 3.3.3 The following recommendations concern the use of the thermal desorption and solidification for sediment remediation:
- 1. Thermal desorption should be tried again at higher temperatures/longer residence times to achieve a more complete assessment of organic contaminant removal ability is made.
- 2. Thermal desorption should be applied to a more contaminated feed material than the Buffalo River sediments before an assessment of organic contaminant removal ability is made.
- 3. Solidification/stabilization is not practical for Buffalo River residues, as two of the three metal contaminants (Cu, Cr) leach more quickly when solidified than when the material has not been treated in this way.

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## APPENDIX A SAMPLE CALCULATIONS



# SAMPLE MASS BALANCE CALCULATION MASS BALANCE FOR CHROMIUM

PART A: ADJUSTMENT OF STREAM WEIGHTS TO DRY WEIGHT BASIS:

A1: NO DATA

A2:

INPUT

(2010 1bs) X (.554 <u>1bs dry solids</u>) x (<u>.454 kg</u>) = 505 kg dry solids 1b 1b

**OUTPUT SOLIDS** 

Average % solids in treated solids + cyclone residue =  $(1055 \text{ lb}) \times (.998) \times (0.454) = 478 \text{ kg}$ 

OUTPUT LIQUIDS

(890 1b) x (.011 1b solids/1b liquid) x (0.454) = 4.4 kg

A3:

INPUT (2150)(.550)(.454) = 537 kg

OUTPUT SOLIDS (1235)(.995)(.454) = 557 kg

OUTPUT LIQUIDS (688)(.008)(.454) = 2.5 kg

**B**1

INPUT (1355)(.561)(.454) = 345

OUTPUT SOLIDS (845)(.986)(.454) = 378

OUTPUT LIQUIDS (620)(.008)(.454) = 2.3

**B2** 

INPUT (2175)(.546)(.454) = 539 kg

OUTPUT SOLIDS (1850)(.998)(.454) = 838 kg

OUTPUT LIQUIDS (445)(.007)(.454) = 1.4 kg

INPUT (1640)(.521)(.454) = 388

OUTPUT SOLIDS (880)(.998)(.454) = 398

OUTPUT LIQUIDS (840)(.009)(.454) = 3.4

C2

INPUT (1905)(.508)(.454) = 439

OUTPUT SOLIDS (955)(.999)(.454) = 433

OUTPUT LIQUIDS (880)(.005)(.454) = 2 kg

C3

INPUT (1940)(.483)(.454) = 425

OUTPUT SOLIDS (950)(.952)(.454) = 411

OUTPUT LIQUIDS (850)(.009)(.454) = 3.5

D1

INPUT (1515)(.446)(.454) = 307

OUTPUT SOLIDS (700)(.999)(.454) = 317

OUTPUT LIQUIDS (950)(.004)(.454) = 1.7

### SOLIDS BALANCE

RUN	SOLIDS INPUT (kg)	SOLIDS OUTPUT (kg)	SOLIDS OUTPUT IN LIQUID (kg)
A2	505	478	4.4
A3	537	(557)	2.5
B1	345	(378)	2.3
В2	539	(838)	1.4
C1	388	(398)	3.4
C2	439	433	2.0
С3	425	411	3.5
D1	307	(317)	1.7

For numbers in parentheses, output exceeds input according to calculations. Possible reasons include material holdup in the equipment and errors inherent in the analytical test methods.

### MASS BALANCES/METALS

Chromium (A2)

505,000 g solids 
$$(47\times10^{-6} \text{ g Cr}) = 23.7 \text{ Cr in}$$
  
g solids

Since it is not known what % of total solids came from the cyclones, the following is assumed for these calculations:

cyclone 1: 4%

cyclone 2: negligible

. . Overall concentration of processed solids is:

$$.96(70) + .04(137) = 73 \text{ ug/g}$$

IN SOLIDS:

$$(477,000 \text{ g}) \times (\underline{73 \times 10^{-6} \text{ g Cr}}) = 34.8 \text{ g}$$

IN CONDENSATE SOLIDS: Consider this negligible

$$(4,400 \text{ g}) (\frac{137 \times 10^{-6} \text{ g}}{\text{g}}) = .60 \text{ g}$$

In Condensate:

890 lbs  $(\underline{.454 \text{ kg}})$  = 404 kg - 4 kg solids output from liquid 1b

404 kg 
$$\frac{L}{kg}$$
 (13.130 x 10<sup>-6</sup> g Cr = 5.2 grams

A3: In:  $(537,000)(68)(10^{-6}) = 36.5$  Cr in

$$.96(61) + .04(148) \approx 65 \text{ ug/g}$$

Out:  $(557,000)(65\times10^{-6}) = 36.2$  Cr in treated solids

Out/Liquids: Correction to liquid amount by removing amount solids is negligible and is ignored for this and future calculations.

$$\frac{(688)(454)(14,200 \times 10^{-6})}{(1000)} = 4.4 \text{ g}$$

<u>Bl:</u>

In: 
$$(345,000)(47)(10^{-6}) = 16.2 \text{ g}$$
  
 $(0.96)(56) + (0.04)(129) \approx 59 \text{ ug/g}$ 

Out (solids): 
$$(378,000)(59 \times 10^{-6}) = 22.3 \text{ g}$$

Out (liquid): 
$$\frac{(620)(454)(1847 \times 10^{-6})}{(1000)} = 0.5 g$$

B2: In: 
$$(539,000)(58)(10^{-6}) = 31.3 g$$
  
 $0.96(44) + 0.04(106) \approx 47 \text{ ug/g}$ 

Out (solid): 
$$(838,000)(47)(10^{-6}) = 39.4 g$$

Out (liquid): 
$$\frac{(445)(454)(200)(10^{-6})}{(1,000)} = 0.04 \approx 0 \text{ g}$$

B3: Closure too poor to consider mass balance on Cr.

C1: In: 
$$(388,000)(73)(10^{-6}) = 28.3 \text{ g Cr in}$$

$$0.96(67) + 0.04(136) = 70$$
 ug/g Cr in treated solids  
 $(398,000)(70 \times 10^{-6}) = 27.9$  g

Out (liquid): 
$$(840)(454)(830)(10^{-6}) = 0.3 \text{ g}$$
  
1000

C2: In: 
$$(439,000(59)(10^{-6}) = 25.9 \text{ Cr in}$$
  
 $.96(58) + .04(129) \approx 61 \text{ ug/g Cr}$ 

Out: 
$$(433,000(61)(10^{-6}) = 26.4$$
 Cr in treated solids

Out (liquid): 
$$(880)(454)(410)(10^{-6}) = 0.2 \text{ g Cr}$$
  
 $1000$ 

<u>C3:</u> In:  $(425,000)(69)(10^{-6}) = 29.3$  Cr in

0.96(62) + 0.04(140) = 65 ug/g

Out:  $(411,000)(65)(10^{-6}) = 12.1$  g Cr out with solids

Out (Liquid):  $\frac{(454)(850)(1140)(10^{-6})}{(1000)} = 0.4 \text{ g Cr}$ 

<u>D1</u>: In:  $(307,000)(55)(10^{-6}) = 16.9 \text{ g Cr}$ 

0.96(62) + 0.04(112) = 64 ug/g

Out:  $(317,000)(64)(10^{-6}) = 20.3 \text{ g Cr in solids}$ 

Out (liquid):  $\frac{(950)(454)(723)(10^{-6})}{1000} = 0.3$ 

### CORRELATION COEFFICIENT:

 $r = \delta (x_i - \overline{x}) (y_i - \overline{y}) / [(x_i - \overline{x})^2 (y_i - \overline{y})^2]^{1/2}$ 

WHERE:  $x_i$  = given value of process variable (e.g., temperature)  $y_i$  = given value of measured parameter (e.g., % solids)

 $\bar{x}$  = average value of process variable

 $\overline{y}$  = average value of measured parameter

### AIR EMISSIONS OF POLYCHLORINATED BIPHENYLS

	Min	imum	Max	imum
PCB	LBS/Hour	Grams/Hour	LBS/Hour	Grams/Hour_
Monochlorobiphenyl	1.25E-07	5.67E-05	2.23E-07	1.01E-04
Dichlorobiphenyl	1.25E-07	5.67E-05	2.23E-07	1.01E-04
Trichlorobiphenyl	1.25E-07	5.67E-05	2.23E-07	1.01E-04
Tetrachlorobiphenyl	2.49E-07	1.13E-04	4.46E-07	2.02E-04
Pentachlorobipheny1	2.49E-07	1.13E-04	4.46E-07	2.02E-04
Hexachlorobipheny1	2.49E-07	1.13E-04	4.46E-07	2.02E-04
Heptachlorobipheny1	3.82E-07	1.73E-04	6.84E-07	3.11E-04
Octachlorobipheny1	3.82E-07	1.73E-04	6.84E-07	3.11E-04
Nonachlorobipheny1	3.82E-07	1.73E-04	6.84E-07	3.11E-04
Decachlorobipheny1	6.31E-07	2.86E-04	1.13E-06	5.13E-04
TOTAL	2.90E-06	1.32E-03	5.19E-06	2.23E-03

### AIR EMISSIONS OF PARTICULATES

	Min	imum	Max	imum
*	LBS/Hour	Grams/Hour	LBS/Hour	Grams/Hour_
Particulates	0.0019	0.086	0.0026	1.18

### AIR EMISSIONS OF POLYCYCLIC AROMATIC HYDROCARBONS

	341.1			
	Minimu		Maximum	· .
PAH	LBS/Hour	Grams/Hour	LBS/Hour	Grams/Hour
Naphtahalene	2.35E-06	1.07E-03	2.58E-05	1.17E-02
Acenapthylene	3.01E-08	1.37E-05	1.26E-06	5.72E-04
Acenaphthene	9.65E-08	4.38E-05	2.49E-06	1.13E-03
Fluorene	1.16E-08	5.27E-06	1.14E-06	5.18E-04
Phenanthrene	9.58E-07	4.35E-05	7.92E-06	3.60E-03
Anthracene	1.04E-07	4.72E-05	9.51E-06	4.32E-03
		1.22E-03		2.18E-02
Fluoranthene	3.89E-07	1.77E-04	2.33E-06	1.06E-03
Pyrene	2.22E-07	1.00E-04	4.56E-06	2.07E-03
Benz(a)anthracene	4.38E-08	1.99E-05	9.16E-06	4.16E-03
Chrysene	5.30E-08	2.40E-05	1.04E-06	4.72E-04
Benzo(bjk)fluoranthrene	9.52F-08	4.32E-05	4.72E-07	2.14E-04
Benzo(a)pyrene	2.63E-08	1.19E-05	5.16E-07	2.34E-04
<pre>Indo(1,2,3-cd)pyrene</pre>	1.99E-08	9.03E-06	1.28E-07	5.81E-05
Dibenz(a,h)anthracene	1.90E-08	8.63E-06	1.22E-07	5.54E-05
Benzo(g,h,i)perylene	2.70E-08	1.22E-05	5.46E-07	2.48E-04
(8, , ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		405.86E-06		857.15E-05
				0552
TOTAL	4.44E-06	2.02E-03	5.86E-05	2.66E-02

### AIR EMISSIONS OF DIOXINS\*

	Min	imum	Max	imum
DIOXIN	nanograms/sec	nanograms/hour	nanograms/sec	nanograms/hour
2378-TCDD	7.00E-04	2.52	1.66E-03	5.98
12378-PeCDD 123478-HxCDD	3.46E-04 8.67E-05	1.25 0.31	2.01E-03 2.68E-04	7.24 0.96
123678-HxCDD 123789-HxCDD	5.33E-05 6.67E-05	0.19 0.24	2.41E-04 2.72E-04	0.87 0.98
1234678-HpCDD OCDD	1.67E-05 1.30E-05	0.06 <u>0.04</u>	2.91E-04 8.99E-05	1.05 0.32
TOTAL		4.61		17.40

<sup>\*</sup> Emissions reported as 2378-TCDD Toxicity Equivalents (EPA 1989)

### AIR EMISSIONS OF FURANS\*

	Mini	mum	Maxi	imum
FURAN	nanograms/sec	nanograms/hou	r nanograms/sec	nanograms/hour
2378-TCDF	0.00E+00	0.00	6.08E-05	0.22
12378-PeCDF	0.00E+00	0.00	0.00E+00	0.00
23478-PeCDF	0.00E+00	0.00	5.48E-03	19.73
123478-HxCDF	0.00E+00	0.00	1.30E-03	4.68
123678-HxCDF	1.47E-05	0.05	1.07E-03	3.85
234678-HxCDF	0.00E+00	0.00	7.12E-05	0.26
123789-HxCDF	0.00E+00	0.00	3.38E-04	1.22
1234678-HpCDF	0.00E+00	0.00	3.68E-04	1.32
1234789-HpCDF	0.00E+00	0.00	0.00E+00	0.00
OCDF	0.00E+00	0.00	0.00E+00	0.00
		•		
TOTAL		0.05		32.28

<sup>\*</sup> Emissions reported as 2378-TCDD Toxicity Equivalents (EPA 1989)



## APPENDIX B

UNREDUCED ANALYTICAL DATA



### REPORT OF CHEMICAL ANALYSES

Volume I: Metals and Conventionals

PROJECT: Buffalo River Pilot Project

### Prepared for:

USEPA Great Lakes National Program Office Attn: Dr. Steve Garbaciak 230 S. Dearborn Chicago, IL 60604

### SAMPLE LABEL KEY

Sample label key is explained by using the following examples:

- (1) Date of sample
- (2) Time of sample
- (3) Sampling point number from Figure 10

Where S = solid stream

L = liquid stream

G = gas stream

- (4) Bin (A,B,C, or D: There were 4 bins filled)
- (5) Type of sample, where:

0 = organic

M = metal

L = leach test

G = grain size

S = solids

C = Total Organic Carbon (TOC)

When sample has additional number preceding the last letter of the series, i.e.

23OCT 4:28 4S A2 O

The number is a run number, i.e. Run 2 from Bin A

REPORT OF:

CHEMICAL ANALYSES

PROJECT:

BUFFALO RIVER PILOT PROJECT

DATE:

ISSUED TO: Dr. Steve Garbaciak

CF#: 379GLBR

Technical Project Manager

USEPA Great Lakes National Program Office

230 S. Dearborn Chicago, IL 60604

### INTRODUCTION

This report summarizes the results from analyses performed on pilot study samples which were submitted by the U.S. Army Corps of Engineers Great Lakes Division, Buffalo District.

### SAMPLE CUSTODY

Samples were received in good condition from October 7, 1991 through November 25. 1991. Samples were logged in and stored as specified in the narrative accompanying each method description. Samples were analyzed within the holding times specified in the QA plan. Any exceptions are noted in the narrative associated with each analysis.

### GRAIN SIZE

Seventeen samples were analyzed for grain size according to Battelle SOP# MSL-M-37 (a modified version of Plumb; 1981). The samples were separated into four classes: gravel, sand, silt and clay. Those classes (excluding gravel) were further subdivided into 5 sand fractions, 6 silt fractions and 4 clay fractions. Samples were stored at  $4^{\circ}\pm2^{\circ}$ C prior to and following analysis. Five samples (two in duplicate) were archived and maintained at  $40\pm20$  C for possible analysis in the future.

Sponsor ID 070CT1:221SCG	Sample Type Sediment	<u>Analyses</u> Grain Size	Battelle ID 379GLBR*25
070CT12:511SBG 070CT12:161SAG	Sediment Sediment	Grain Size Grain Size	379GLBR*31 379GLBR*32
070CT12:1613AG	Sediment	Grain Size	379GLBR*33
080CT5:222SD2G	Sediment	Grain Size	379GLBR*47
090CT12:002SAG	Sediment	Grain Size	379GLBR*61
090CT10:502SBG 090CT5:082SCG	Sediment Sediment	Grain Size Grain Size	379GLBR*69 379GLBR*77
230CT4:304SA2G	Sediment	Grain Size	379GLBR*120
250CT9:264SA3G	Sediment	Grain Size	379GLBR*156
250CT2:324SB1G	Sediment	Grain Size	379GLBR*184 379GLBR*219
310CT9:274SB2G 310CT2:364SB3G	Sediment Sediment	Grain Size Grain Size	379GLBR 219 379GLBR*241
19NOV8:584SC1G	Sediment	Grain Size	379GLBR*299
19NOV4:464SC2G	Sediment	Grain Size	379GLBR*321
20N0V3:114SC3G 21N0V5:204SD1G	Sediment Sediment	Grain Size Grain Size	379GLBR*346 379GLBR*391

### ARCHIVED SAMPLES

19NOV4:464SC2G Sediment Grain Size 379GLBR*321-T 19NOV4:464SC2G Sediment Grain Size 379GLBR*321-T 22NOV3:124SD2G Sediment Grain Size 379GLBR*420	
22NOV3:124SD2G Sediment Grain Size 379GLBR*420	

Some values for % dry weight are greater than 100% due to absorption of moisture during the cooling step of the method for determining % dry weight. If a desiccator had been used, the samples would have exhibited % dry weight values = 99.5%. The analyst did not use a desiccator for the oven-drying step for the determination of grain size. Therefore, when the analyst calculates the data, any effect of moisture absorption is canceled out through the equations resulting in valid data.

### **METALS**

Forty-six sediment samples and thirty-three water samples were analyzed for metals. The sediment samples were dried (Battelle SDP# MSL-M-3) and an aliquot was analyzed by X-ray fluorescence for Cr. Cu and Pb. A separate dried aliquot was digested with nitric, hydrofluoric and perchloric acids (Battelle SOP# MSL-M-7), then analyzed for Hg by cold vapor atomic absorption (Battelle SOP# MSL-M-31). An aliquot of each water sample was digested with hot nitric acid (Battelle SOP# MSL-M-22) and analyzed by flame atomic absorption and graphite furnace atomic absorption for Cr. Cu and Pb according to Battelle SOP# MSL-M-32 (based on EPA method 200.9). A separate aliquot was digested with a solution of nitric and sulfuric acid, then analyzed for Hg by cold vapor atomic fluorescence following Battelle SOP# MSL-M-11. According to the Buffalo River QA plan we were to analyze the Hg samples following Battelle SOP# MSL-M-27 for Hg in water, however, due to the high content of combustion by-products from organic contaminants it was necessary to treat these samples as sediments. Thirteen sediment samples (3 in quadruplicate) and 12 water samples (2 in quadruplicate, 2 in duplicate) were archived for possible analysis in the future. Sediment samples were stored at -70°±10°C prior to drying. Once dried, the samples were stored at room temperature prior to and following analysis. Water samples were acidified at the time of collection and stored at room temperature prior to and following analysis.

	_	•	
Sponsor ID	Sample Type	Analyses	Da++-11- TD
070CT1:261SCM	Sediment		Battelle ID
070CT12:191SAM	Sediment	Metals	379GLBR*26
070CT2:001SDM		Metals	379GLBR*27
	Sediment	Metals	379GLBR*28
070CT12:541SBM	Sediment	Metals	379GLBR*29
080CT4:572SDM	Sediment	Metals	379GLBR*49
090CT12:002SAM	Sediment	Metals	379GLBR*60
090CT10:502SBM	Sediment	Metals	379GLBR*68
090CT5:052SCM	Sediment	Metals	379GLBR*76
220CT11:287SA1M	Sediment	Metals	379GLBR*103
220CT11:358SA1M	Sediment	Metals	379GLBR*106
230CT1:303SA2M	Sediment	Metals	 379GLBR*115
230CT4:314SA2M	Sediment	Metals	379GLBR*119
240CT10:457SA2M	Sediment	Metals	379GLBR*135
240CT10:508SA2M	Sediment	Metals	
240CT6:203SA3M	Sediment	Metals	379GLBR*138
250CT9:194SA3M	Sediment		379GLBR*146
250CT9:287SA3M	Sediment	Metals	379GLBR*150
250CT9:338SA3M		Metals	379GLBR*155
	Sediment	Metals	379GLBR*168
250CT2:153SB1M	Sediment	Metals	 379GLBR*177
250CT2:334SB1M	Sediment	Metals	379GLBR*186
250CT3:517SB1M	Sediment	Metals	379GLBR*192
250CT3:558SB1M	Sediment	Metals	379GLBR*195
300CT4:463SB2M	Sediment	Metals	379GLBR*207
310CT9:007SB2M	Sediment	Metals	379GLBR*208
310CT9:088SB2M	Sediment	Metals	379GLBR*211
310CT9:274SB2M	Sediment	Metals	 379GLBR*215
310CT2:384SB3M	Sediment	Metals	379GLBR*245
		ui3	3/30LBK 243

310CT10:453SB3M	Sediment	Metals		379GLBR*246
1NOV10:208SB3M	Sediment	Metals		379GLBR*265
1NOV10:157SB3M	Sediment	Metals		379GLBR*267
18NOV4:403SC1M	Sediment	Metals		379GLBR*285
19N0V8:484SC1M	Sediment	Metals		379GLBR*300
19NOV9:218SC1M	Sediment	Metals		379GLBR*305
19NOV9:327SC1M	Sediment	Metals		379GLBR*308
19NOV3:553SC2M	Sediment	Metals		379GLBR*316
19NOV4:414SC2M	Sediment	Metals		379GLBR*320
20N0V8:157SC2M	Sediment -	Metals		379GLBR*336
20NOV1:553SC3M	Sediment	Metals		379GLBR*345
20NOV3:184SC3M	Sediment	Metals		379GLBR*353
20N0V3:327SC3M	Sediment	Metals		379GLBR*356
20N0V3:268SC3M	Sediment	Metals		379GLBR*359
21NOV2:433SD1M	Sediment	Metals		379GLBR*381
21NOV4:578SD1M	Sediment	Metals		379GLBR*383
21NOV5:087SD1M	Sediment	Metals		379GLBR*386
21NOV5:174SD1M	Sediment	Metals		379GLBR*389
21NOV5:1743D1M		Metals		379GLBR*390
	Sediment			
230CT4:459LA2M	011	Metals		379GLBR*127†
230CT5:2510LA2M	Water	Metals		379GLBR*131†
230CT5:2010LA2M	Water	Metals		379GLBR*133*†
250CT10:2010LA3M	Water	Metals		379GLBR*163†
250CT11:0010LA3M	Water	Metals		379GLBR*170*
250CT10:009LA3M	011	Metals		379GLBR*171†
250CT3:1210LB1M				373GLDR 1711
	Water	Metals		379GLBR*188†
250CT3:3010LB1M	Water	Metals		379GLBR*189*
300CT4:216LA3M	Water	Metals		379GLBR*203
310CT10:089LB2M -	011	Metals		379GLBR*223
310CT10:2010LB2M	Water	Metals		379GLBR*228†
310CT10:3010LB2M	Water	Metals	1.	379GLBR*229*†
310CT3:5010LB3M	Water	Metals		379GLBR*251*
310CT2:5710LB3M	Water	Metals		379GLBR*254†
310CT3:069LB3M				
	011	Metals		379GLBR*255
1NOV11:006LB2M	Water	Metals		379GLBR*270
1NOV2:506LB1B3M	Water	Metals		379GLBR*274
6NOV12:003LM	Water	Metals		379GLBR*277
18NOV5:309LC1M	011	Metals		379GLBR*290†
18NOV6:1810LC1M	Water	Metals		379GLBR*292*
18NOV6:1810LC1M	Water	Metals		379GLBR*293
19NOV5:559LC2M	Oil			
	= ' '	Metals		379GLBR*328†
19NOV5:2010LC2M	Water	Metals		379GLBR*333*
19N0V5:3510LC2M	Water	Metals		379GLBR*334
20N0V2:173LC3M	Water	Metals		379GLBR*362*
20NOV2:173LC3M	Water	Metals		379GLBR*363
20NOV2:439LC3M	011	Metals		379GLBR*368†
20N0V3:0310LC3M	Water	Metals		379GLBR*371
20NOV3:0710LC3M	Water	Metals		379GLBR*372*
21NOV3:3810LD1M	Water	Metals		379GLBR*3991
21NOV3:4510LD1M	Water	Metals		379GLBR*400*
21NOV4:359LD1M	011	Metals		379GLBR*405†
*Samples were filtered	d at the time of d	collection	therefo	re, results are for
dissolved metals.				
tSamples had a pH sign	nificantly dreater	than 2.		
F	, , , , , , , , , , , , , , , , , , ,			

ARCHIVED SAMPLES

Sponsor ID	<u>Sample Type</u>	<u>Analyses</u>	<u>Battelle ID</u>
070CT1:121SBM	Sediment	Metals	379GLBR*30
080CT4:502SDM	Sediment	Metals	379GLBR*49- <b>T2</b>
080CT4:472SDM	Sediment	Metals	379GLBR*49-T3
080CT4:552SDM	Sediment	Metals	379GLBR*49-M1

080CT4:522SDM		Sediment		Metals		379GLBR*49-M2	
210CT12:503SA1M		Sediment		Metals		379GLBR*81	
210CT5:484SA1M		Sediment		Metals		379GLBR*86	
300CT4:493SB2M		Sediment :		Metals			
300CT4:503SB2M		Sediment	•	Metals		379GLBR*207-T	
300CT4:3033B2M		Sediment				379GLBR*207-T2	
300CT4:4733B2M				Metals		379GLBR*207-M	
		Sediment		Metals		379GLBR*207-M2	<u> </u>
19NOV4:414SC2M		Sediment		Metals		379GLBR*320-T	l .
19NOV4:414SC2M		Sediment		Metals		379GLBR*320-T2	2
19NOV4:414SC2M		Sediment	•	Metals		379GLBR*320-M1	
19NOV4:414SC2M		Sediment		Metals		379GLBR*320-M2	) -
22NOV1:453SD2M		Sediment		Metals		379GLBR*413	
<b>22NOV3:18</b> 4SD2M		Sediment		Metals		379GLBR*421	
22NOV3:164SD2M		Sediment		Metals		379GLBR*422	
22NOV3:348SD2M		Sediment		Metals		379GLBR*425	
25NOV2:203SD3M		Sediment		Metals		379GLBR*441	
25NOV4:004SD3M		Sediment		Metals		379GLBR*442	
25NOV4:004SD3M		Sediment		Metals		379GLBR*448	
210CT6:2510LA1M		Water		Metals		379GLBR*96	
210CT6:459LA1M		011		Metals		379GLBR*102†	
18NOV5:309LC1M		011		Metals		379GLBR*290-T1	<b>+</b> '
18NOV5:309LC1M		011		Metals		379GLBR*290-T2	
18NOV5:309LC1M		011		Metals			
18NOV5:309LC1M		011		Metals		379GLBR*290-M1	, I
19NOV5:2010LC2M		Water				379GLBR*290-M2	. Т
19NOV5:2010LC2M				Metals		379GLBR*333-T2	
		Water		Metals		379GLBR*333-M2	
19NOV5:3510LC2M		Water		Metals		379GLBR*334-T1	
19NOV5:3510LC2M		Water		Metals		379GLBR*334-T2	
21NOV4:359LD1M		011		Metals		379GLBR*405-T1	
21NOV4:359LD1M		011		Metals		379GLBR*405-T2	
21NOV4:359LD1M		011		Metals		379GLBR*405-M1	
21NOV4:359LD1M		011		Metals		379GLBR*405-M2	†
22NOV2:3210LD2M		Water		Metals		379GLBR*429†	
22NOV2:4010LD2M		Water		Metals		379GLBR*430*	
22NOV2:559LD2M		011		Metals		379GLBR*434†	
25NOV4:0010LD3M		Water		Metals		379GLBR*455	
25NOV4:009LD3M		011		Metals		379GLBR*457†	
25NOV4:0010LD3M		Water		Metals		379GLBR*459	
*Samples were fi	ltered	at the time	of	collection	theref	organite ar	a for
discolved metals		. 25 5116 51116	٠,	55116661011,	CHELC!	ore results at	e 101

\*Samples were filtered at the time of collection, therefore results are for dissolved metals.

tSamples had a pH significantly greater than 2.

Some samples were not acidified at the time of collection to a  $pH \leq 2$ . Metals in water samples stored for any period of time at a  $pH \geq 2$  tend to adsorb onto the walls of the container which usually provide lower results. It became apparent in March, after all samples had been analyzed, that some samples were not acidified properly when mold was detected in those samples. We provided the acid normally required to acidify freshwater samples to a  $pH \leq 2$ . Therefore, either the acid was not added to the sample or the alkalinity was so high in the sample that the amount of acid provide was not sufficient to bring the pH down to qH. Those samples have been acidified since then and are available for re-analysis.

The water samples collected for metals analysis contained a high content of oil. As indicated by GLNPO, we digested the water including oil with hot nitric acid to obtain a total metals value. Values for samples flagged with an F represent total dissolved metals in the entire sample (water + oil).

The high standard for lead in water has a concentration of 1 mg/L and a milliabsorbance reading of 47. Some water samples analyzed for lead had a milliabsorbance reading slightly higher than 47 (48-55). The curve should still be linear at these milliabsorbance values, therefore would not affect the quality of

the data. One sample had a milliabsorbance reading of 66 which was diluted and rerun by graphite furnace.

Deviations of the precision acceptance criteria for chromium were found on samples that had concentrations near the detection limit of 25  $\mu g/g$ . Samples that had higher chromium concentrations were well within the precision acceptance criteria established in the OA plan.

Water samples for mercury were analyzed by the water method initially. As the analyst became aware of matrix problems, she digested and analyzed all the samples as sediments. The results on the first raw data sheet are for mercury by the water method. Those results were not reported. When applicable, duplicate analyses were averaged and the average was reported. Recoveries for one set of matrix spikes for mercury in water were outside the criteria. Recoveries were high (128 and 155%) due to very large dilution factors necessary to obtain results within the calibration curve, however this should not compromise the data.

### SOLIDS and TOC

Ninety-six sediment samples and twenty-two water samples were analyzed for solids content and total organic carbon. An aliquot of each sample was oven-dried at 105∘±5∘C according to Battelle SOP# MSL-M-3, then taken to 550∘±10∘C to allow volatilization according to Battelle SOP# MSL-M-2. A separate aliquot of each sample was freeze-dried according to Battelle SOP# MSL-M-3 and sent to Global Geochemistry Laboratory for total organic carbon analysis according to the LECO method for TOC in weight percent. Water samples were analyzed for total solids according to Battelle SOP# MSL-M-40 (based on Standard Methods, 2540B) and total suspended solids according to Battelle SOP# MSL-M-39 (based on Standard Methods. 2540D). With such a high amount of heavy particulates, it was difficult for the analyst to obtain a representative sample for total suspended solids and total solids. All solids samples were analyzed within the holding time of 7 days from collection. However, if the reproducibility was outside the acceptance criteria of  $\pm 20\%$  the samples were re-analyzed, usually after the holding time had been exceeded. Separate samples collected at the sampling site were sent to Analytical Resources. Inc. for total organic carbon. There was a problem with high particulate concentrations in the samples. After some discussion with Eric Crecelius (program manager), they were instructed to allow the particulates to settle, then withdraw a portion of the liquid phase for analysis.

090CT4:362SC2S 090CT4:552SC1S 090CT4:552SC1S 090CT4:152SC3S 220CT11:307SA1S 220CT11:368SA1S 220CT4:203SA2S 220CT5:553SA2S 230CT1:303SA20 230CT4:254SA2S 230CT4:264SA2S 230CT4:274SA2S 240CT10:457SA2S 240CT10:508SA2S 240CT5:503SA3S 240CT5:503SA3S 240CT5:503SA3S 240CT6:203SA3S 250CT9:234SA3S 250CT9:234SA3S 250CT9:254SA3S 250CT9:337SA3S 250CT9:358SA3S 250CT9:358SA3S 250CT2:353SB1S 250CT2:314SB1S 250CT2:314SB1S 250CT2:314SB1S 250CT2:314SB1S 250CT2:324SB1S 250CT2:334SB1S 250CT3:517SB1S 250CT2:334SB3S 310CT2:364SB3S 310CT2:374SB3S 310CT2:364SB3S 310CT2:374SB3S	Sediment Sediment	TS. TVS. TO TS. TV	379GLBR*71 379GLBR*72 379GLBR*105 379GLBR*105 379GLBR*1100 379GLBR*1110 379GLBR*114 379GLBR*114 379GLBR*116 379GLBR*117 379GLBR*118 379GLBR*137 379GLBR*137 379GLBR*140 379GLBR*140 379GLBR*140 379GLBR*140 379GLBR*140 379GLBR*140 379GLBR*175 379GLBR*200 379GLBR*200 379GLBR*200 379GLBR*200 379GLBR*200 379GLBR*200 379GLBR*216 379GLBR*216 379GLBR*235 379GLBR*235 379GLBR*236 379GLBR*236 379GLBR*237 379GLBR*237 379GLBR*238 379GLBR*237 379GLBR*238 379GLBR*237 379GLBR*238 379GLBR*239
19N0V8:564SC1S 19N0V8:574SC1S 19N0V9:228SC1S 19N0V9:337SC1S 19N0V11:303SC2S 19N0V2:203SC2S 19N0V3:553SC2S	Sediment Sediment Sediment Sediment	TS. TVS. TOO TS. TVS. TOO TS. TVS. TOO TS. TVS. TOO	379GLBR*297 379GLBR*298 379GLBR*306 379GLBR*309 379GLBR*310 379GLBR*312
19N0V4:3145C2S 19N0V4:314SC2S 19N0V4:314SC2S 20N0V8:157SC2S 20N0V11:443SC3S 20N0V1:003SC3S	Sediment Sediment Sediment Sediment Sediment Sediment	TS. TVS. TOO	379GLBR*317 379GLBR*318 379GLBR*319 379GLBR*338 379GLBR*339

20N0V1:553SC3S 20N0V3:124SC3S 20N0V3:124SC3S 20N0V3:124SC3S 20N0V3:317SC3S 20N0V3:258SC3S 21N0V12:003SD1S 21N0V1:353SD1S 21N0V2:433SD1S 21N0V4:558SD1S 21N0V5:087SD1S 21N0V5:214SD1S 21N0V5:214SD1S 21N0V5:214SD1S	Sediment Sediment Sediment Sediment Sediment Sediment Sediment Sediment Sediment Sediment Sediment Sediment Sediment	TS. TVS. TOC	379GLBR*343 379GLBR*347 379GLBR*348 379GLBR*355 379GLBR*355 379GLBR*375 379GLBR*377 379GLBR*379 379GLBR*382 379GLBR*387 379GLBR*382 379GLBR*393 379GLBR*393
230CT4:459LA2S 230CT5:2010LA2S 250CT10:2210LA3S 250CT10:2110LA3S 250CT3:1110LB1S 300CT4:166LA3S 310CT10:059LB2S 310CT10:1910LB2S 310CT2:5410LB3S 310CT2:5610LB3S 310CT3:049LB3S 310CT3:059LB3S 6NOV12:003LS 18NOV5:409LC1S 18NOV5:539LC2S 19NOV5:539LC2S 19NOV5:2410LC2S 20NOV2:163LC3S 20NOV2:409LC3S 20NOV3:0010LC3S 21NOV3:3510LD1S 21NOV4:039LD1S	Oil Water Water Water Water Oil Water Water Oil	TS. TSS	379GLBR*126 379GLBR*130 379GLBR*159 379GLBR*159 379GLBR*202 379GLBR*224 379GLBR*224 379GLBR*259 379GLBR*259 379GLBR*260 379GLBR*261 379GLBR*261 379GLBR*261 379GLBR*276 379GLBR*361 379GLBR*362 379GLBR*364 379GLBR*367 379GLBR*364 379GLBR*373 379GLBR*401 379GLBR*401 379GLBR*403
30CT4:459LA20 230CT5:2010LA2C 250CT10:2110LA3C 250CT10:009LA3C 250CT3:1110LB1C 300CT4:206LA3C 310CT10:109LB2C 310CT10:2410LB2C 310CT2:5810LB3C 310CT3:099LB3C 1N0V11:006LB2C 1N0V2:506LB1B3C 6N0V12:003LC 18N0V6:0610LC1C 18N0V5:459LC1C 19N0V5:579LC2C 19N0V5:4310LC2C 20N0V2:183LC3C 20N0V2:449LC3C 20N0V3:0210LC3C 21N0V4:459LD1C	Oil Water Water Oil Water Water Oil Water Water Water Water Water Water Water Water Oil Water Water Oil Water Water Oil Water Oil Water Oil Water Oil	TOC	379GLBR*125 379GLBR*129 379GLBR*162 379GLBR*165 379GLBR*190 379GLBR*201 379GLBR*225 379GLBR*225 379GLBR*231 379GLBR*263 379GLBR*273 379GLBR*273 379GLBR*273 379GLBR*273 379GLBR*330 379GLBR*335 379GLBR*335 379GLBR*335 379GLBR*335 379GLBR*335 379GLBR*365 379GLBR*374 379GLBR*406

# BUFFALO PILOT PROJECT (CF# 379) GRAIN SIZE - TOTAL SOLIDS ANALYSIS

			Predicted	Actual	
		% Total	Dry	Dry	Estimated
MSL Code	Sponsor ID	Solids	Mass (g)	Mass (g)	Recovery
		•			
		*			
	; <b>L</b>	BIN A			
379GLBR-32	07OCT12:161SAG	60.05%	14.2368	15.2327	107.00%
379GLBR-61	09OCT12:002SAG	64.44%	13.5706	13.7666	101.44%
379GLBR-120	230CT4:304SA2G	99.87%	10.4067	10.0779	96.84%
379GLBR-156	25OCT9:264SA3G	99.55%	9.2782	10.2376	110.34%
		BIN B			
379GLBR-31	07OCT12:511SBG	54.78%	14.4168	15.7037	108.93%
379GLBR-69	09OCT10:502SBG	59.75%	12.2001	13.2007	108.20%
379GLBR-184	250CT2:324SB1G	98.94%	9.3495	10.1831	108.92%
379GLBR-219	310CT9:274SB2G	100.09%	9.5281	10.1853	106.90%
379GLBR-241	310CT2:364SB3G	100.01%	9.8506	10.5914	107.52%
		BIN C			
379GLBR-25	07OCT1:221SCG	65.29%	14.5604	15.0865	103.61%
379GLBR-77	09OCT5:082SCG	60.00%	11,9039	13.0577	109.69%
379GLBR-299	19NOV8:584SC1G	100.05%	10.3054	10.4093	101.01%
379GLBR-321 Rep 1	19NOV4:464SC2G	100.11%	9.8212	10.4951	106.86%
379GLBR-321 Rep 2	19NOV4:464SC2G	100.14%	9.8535	10.3475	105.01%
379GLBR-321 Rep 3	3 19NOV4:464SC2G	100.14%	9.9439	10.5172	105.77%
379GLBR-346	20NOV3:114SC3G	96.79%	9.4950	10.1702	107.11%
		BIN D			
379GLBR-33	07OCT1:561SDG	59.83%	13.2771	14.1625	106.67%
	08OCT5:222SD2G	75.50%	14.6170	12.6762	86.72%
	08OCT5:222SD2G	58.80%	11.3138	12.5171	110.64%
	08OCT5:222SD2G	58.80%	11.4663	12.4534	108.61%
379GLBR-391	21NOV5:204SD1G	99.97%	9.2072	10.0154	108.78%
379GLBR-346 *	20NOV3:114SC3G	96.79%	9.4950	10.1720	107.11%
379GLBR-391 •	21NOV5:204SD1G	99.93%	10.2629	10.8617	105.83%

<sup>\*</sup> These dry samples were not disaggregated before analysis was done. They should be used only as a comparison for the rest of the dry samples which were disaggregated before analysis.

# BUFFALO RIVER PILOT PROJECT (CF#379) GRAIN SIZE - TOTAL SOLIDS ANALYSIS

			PERC	PERCENT OF TOTAL MASS	FAL MASS				
			1.00-	0.500-	0.25-	0.125-	0.0625-	48.0-	31.2-
MSL Code	Sponsor ID	>2.00 mm	2.00 mm	1.00 mm	0.500 mm	0.250 mm	0.125 mm	62.5 um	48.0 um
BIN A									
379GLBR-32	07OCT12:161SAG	90.0	0.11	0.15	0.53	2.67	10.29	3.73	6.38
379GLBR-61	09OCT12:002SAG	0.40	0.05	0.20	1.12	3.83	12.19	3.60	5.99
379GLBR-120	23OCT4:304SA2G	00.0	0.21	0.38	1.91	4.75	14.32	2.58	11.23
379GLBR-156	250CT9:264SA3G	0.00	0.38	0.91	1.28	3.85	13.25	6.90	8.38
BIN B									
379GLBR-31	07OCT12:511SBG	0.08	90.0	0.22	0.66	1.78	7.46	4.79	3.23
379GLBR-69	09OCT10:502SBG	0.13	0.14	0.27	1.48	4.90	13.75	3.30	7.55
379GLBR-184	250CT2:324SB1G	0.04	0.16	0.36	1.86	9.10	16.40	2.51	11.51
379GLBR-219	31OCT9:274SB2G	0.00	0.24	0.33	2.06	7.65	17.86	9.90	6.99
379GLBR-241	310CT2:364SB3G	0.04	0.19	0.59	3.18	6.03	16.82	1.40	8.84
BINC									
379GLBR-25	070CT1:221SCG	0.10	0.13	0.23	1.45	15.60	15.58	1.22	7.87
379GLBR-77	09OCT5:082SCG	0.08	0.14	0.20	1.09	4.86	13.74	4.56	5.76
379GLBH-299	19NOV8:584SC1G	0.00	0.31	0.45	2.17	8.53	18.63	7.99	7.38
379GLBR-321	Rep 1 19NOV4:464SC2G	0.00	0.39	0.34	3.24	13.37	14.17	5.49	8.65
3/9GLBH-321	Hep 2 19NOV4:464SC2G	0.11	0.07	0.48	3.56	10.75	17.68	8.39	7.19
3/9GLBH-321	Hep 3 19NOV4:464SC2G	0.00	0.11	0.45	3.90	10.24	17.52	6.28	9.28
3/9GLBH-346	20NOV3:114SC3G	0.27	0.66	0.98	2.52	8.44	17.27	6.88	7.98
BIN D									
379GLBR-33	07OCT1:561SDG	0.10	0.05	0.14	0.73	4.33	13.79	3.39	808
379GLBR-47	Rep 1 08OCT5:222SD2G	0.05	0.09	0.32	1.13	3.61	12.76	4.23	7.57
379GLBR-47	Rep 2 08OCT5:222SD2G	0.09	0.14	0.26	1.17	3.88	12.50	2.05	7.22
379GLBR-47	Rep 3 08OCT5:222SD2G	0.82	0.16	0.25	1.10	3.54	12.58	2.18	8.87
379GLBR-391	21NOV5:204SD1G	0.00	0.14	99.0	4.40	8.32	16.38	2.16	8.43
379GLBR-346	• 20NOV3:114SC3G	30.59	15.06	9.86	4.84	5.79	7.78	1.24	3.14
379GLBR-391	• 21NOV5:204SD1G	33.61	17.82	11.90	5.37	3.97	6.34	2.03	1.84

NOTE: All results are in percent.

These dry samples were not disaggregated before analysis was done.
 They should be used only as a comparison for the rest of the dry samples which were disaggregated before analysis.

# BUFFALO RIVER PILOT PROJECT (CF#379) GRAIN SIZE - TOTAL SOLIDS ANALYSIS

			PERC	PERCENT OF TOTAL MASS	AL MASS					
		23.0-	15.6-	7.8-	3.9-	1.9-	0.976-	0.488-		Salt Blank
MSL Code	Sponsor ID	31.2 um	23.0 um	15.6 um	7.8 um	3.9 um	1.9 um	0.976 um	<0.488 um	(6)
BIN A			:							
379GLBR-32	07OCT12:161SAG	10.50	10.61	20.06	10.48	7.59	5.17	3.12	8.38	0.0158
379GLBR-61	09OCT12:002SAG	8.08	10.87	17.84	9.24	6.57	4.68	3.31	12.03	0.0072
379GLBR-120	230CT4:304SA2G	11.35	11.35	19.85	8.57	6.03	3.81	2.66	0.99	0.000
379GLBR-156	250CT9:264SA3G	10.79	11.65	21.89	2.96	4.75	6.66	0.43	5.92	0.0005
BIN B										
379GLBR-31	070CT12:511SBG	10.49	10.55	21.17	12.00	8.35	5.09	3.72	10.34	0.0111
379GLBR-69	09OCT10:502SBG	8.09	9.48	17.21	8.48	6.39	4.85	3.21	10.78	0.0109
379GLBR-184	250CT2:324SB1G	10.29	8.60	14.02	8.68	5.66	4.24	0.86	5.70	0.0004
379GLBR-219	310CT9:274SB2G	10.17	9.86	15.16	8.25	5.07	3.50	1.96	1.02	0.0003
379GLBR-241	310CT2:364SB3G	9.44	8.76	23.79	8.57	5.36	0.04	2.04	4.91	0.0005
BIN C										
379GLBR-25	070CT1:221SCG	6.95	8.46	12.20	9.68	5.30	3.37	2.81	9.07	0.0119
379GLBR-77	09OCT5:082SCG	10.14	9.59	16.76	8.73	2.67	4.07	3.37	11.24	0.0105
_	19NOV8:584SC1G	7.92	7.99	21.17	2.96	7.72	0.77	3.34	2.69	0.0004
	Rep 1 19NOV4:464SC2G	8.16	7.47	15.51	7.55	9.68	3.28	0.95	1.75	0.0006
_	Rep 2 19NOV4:464SC2G	7.38	7.50	14.61	6.84	5.03	8.12	0.89	1.39	0.0011
	Rep 3 19NOV4:464SC2G	8.10	7.53	13.92	6.47	5.25	8.48	0.65	1.83	0.0007
379GLBR-346	20NOV3:114SC3G	8.14	7.35	16.91	7.91	5.03	3.85	4.88	0.90	0.0003
BIN D										
	07OCT1:561SDG	8.08	10.20	18.08	9.46	6.44	4.80	3.50	8.84	0.0156
_	Rep 1 08OCT5:222SD2G	7.76	10.67	16.82	60.6	6.41	4.29	3.41	11.83	0.0098
_	Rep 2 08OCT5:222SD2G	9.62	9.81	17.70	8.66	6.20	4.44	3.32	12.91	0.0087
	Rep 3 08OCT5:222SD2G	8.45	11.15	17.18	90.6	6.33	4.53	3.31	10.54	0.0157
379GLBR-391	21NOV5:204SD1G	8.55	10.78	20.45	8.07	4.75	3.99	2.12	0.80	0.0006
379GLBR-346 •	20NOV3:114SC3G	1.98	3.29	6.78	2.90	1.34	0.99	0.14	4.28	0.0222
379GLBR-391 •	21NOV5:204SD1G	2.25	2.32	2.08	1.58	0.88	0.48	0.37	4.16	0.0191

NOTE: All results are in percent.
These dry samples were not disaggregated before analysis was done.
They should be used only as a comparison for the rest of the dry samples which were disaggregated before analysis.

BIN A	MSL Code	Sponsor ID	Cr			Pb (ug/g)
379GLBR- 8 07OCT12:301SAL 77 39.8 46.0 379GLBR- 27 07OCT12:191SAM 73 46.2 72.2 379GLBR- 60 09OCT12:002SAM 60 45.8 52.4 379GLBR- 103 22OCT11:287SA1M 110 55.3 65.6 379GLBR- 106 22OCT11:358SA1M 155 55.4 56.6 379GLBR- 115 23OCT13:303SA2M 47 41.1 53.7 379GLBR- 135 24OCT10:457SA2M 137 51.3 58.9 379GLBR- 135 24OCT10:457SA2M 137 51.3 58.9 379GLBR- 138 24OCT10:508SA2M 84 42.3 48.8 379GLBR- 146 24OCT6:203SA3M 68 40.6 52.4 379GLBR- 150 25OCT9:194SA3M 61 41.3 52.7 379GLBR- 155 25OCT9:104SA3M 66 42.7 54.9 379GLBR- 155 25OCT9:287SA3M 148 47.1 56.7 379GLBR- 168 25OCT9:287SA3M 88 43.1 48.0 379GLBR- 462 4DEC12:055SA2M 51 43.0 58.2 379GLBR- 462 4DEC12:055SA2M 51 43.0 58.2 379GLBR- 186 25OCT9:153SB1M 47 37.6 64.3 379GLBR- 186 25OCT2:334SB1M 56 45.7 65.7 379GLBR- 192 25OCT3:517SB1M 129 48.2 65.1 379GLBR- 195 25OCT3:558SB1M 121 46.2 58.4 379GLBR- 207 Rep 1 30OCT4:463SB2M 70 41.1 56.4 379GLBR- 207 Rep 2 30OCT4:463SB2M 70 41.1 56.7 379GLBR- 207 Rep 3 30OCT4:463SB2M 70 41.1 56.4 379GLBR- 207 Rep 3 30OCT4:463SB2M 77 47.1 64.5 379GLBR- 208 31OCT9:07SB2M 106 46.8 67.0 379GLBR- 215 31OCT9:274SB2M 44 45.6 67.0 379GLBR- 245 31OCT9:274SB2M 44 45.6 67.0 379GLBR- 245 31OCT9:274SB2M 44 45.6 67.0 379GLBR- 245 31OCT9:274SB2M 45 44.6 65.7 379GLBR- 245 31OCT9:274SB2M 45 44.6 66.8 67.0 379GLBR- 245 31OCT9:274SB2M 45.6 67.0 379GLBR- 245 31OCT9:274SB2M 55 43.2 60.6 379GLBR- 245 31OCT9:274SB2M 55 43.2 60.6 379GLBR- 245 31OCT10:453SB3M 55 43.2 60.6 379GLBR- 246 31OCT10:453SB3M 55 43.2 60.6 379GLBR- 265 1NOV10:208SB3M 117 49.5 61.3	INOL COUR	טוווסטו וט		XPF	XPF	XRF
379GLBR- 27       07OCT12:191SAM       73       46.2       72.2         379GLBR- 60       09OCT12:002SAM       60       45.8       52.4         379GLBR- 106       22OCT11:287SA1M       110       55.3       65.6         379GLBR- 106       22OCT11:303SA2M       47       41.1       53.7         379GLBR- 115       23OCT1:303SA2M       47       41.1       53.7         379GLBR- 135       24OCT10:457SA2M       70       38.2       52.1         379GLBR- 138       24OCT10:508SA2M       84       42.3       48.8         379GLBR- 150       25OCT9:194SA3M       63       40.6       52.4         379GLBR- 154       25OCT9:104SA3M       61       41.3       52.7         379GLBR- 155       25OCT9:104SA3M       64       42.7       54.9         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 195       25OCT3:53TSB1M       47       37.6       64.3         379GLBR- 195       25OCT3:55SSB1M		· BIN A				
379GLBR- 27       07OCT12:191SAM       73       46.2       72.2         379GLBR- 60       09OCT12:002SAM       60       45.8       52.4         379GLBR- 106       22OCT11:287SA1M       110       55.3       65.6         379GLBR- 106       22OCT11:303SA2M       47       41.1       53.7         379GLBR- 115       23OCT1:303SA2M       47       41.1       53.7         379GLBR- 135       24OCT10:457SA2M       70       38.2       52.1         379GLBR- 138       24OCT10:508SA2M       84       42.3       48.8         379GLBR- 150       25OCT9:194SA3M       63       40.6       52.4         379GLBR- 154       25OCT9:104SA3M       61       41.3       52.7         379GLBR- 155       25OCT9:104SA3M       64       42.7       54.9         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 195       25OCT3:53TSB1M       47       37.6       64.3         379GLBR- 195       25OCT3:55SSB1M	379GLBR- 8	07OCT12:301SAL		77	39.8	46.0
379GLBR- 103       22OCT11:287SA1M       110       55.3       65.6         379GLBR- 106       22OCT11:358SA1M       155       55.4       56.6         379GLBR- 115       23OCT1:303SA2M       47       41.1       53.7         379GLBR- 119       23OCT4:314SA2M       70       38.2       52.1         379GLBR- 135       24OCT10:508SA2M       84       42.3       48.8         379GLBR- 138       24OCT10:508SA2M       84       42.3       48.8         379GLBR- 146       24OCT6:203SA3M       68       40.6       52.4         379GLBR- 150       25OCT9:194SA3M       61       41.3       52.7         379GLBR- 154       25OCT9:104SA3M       66       42.7       54.9         379GLBR- 168       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 186       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 192       25OCT3:558SB1M       129       48.2       65.1	379GLBR- 27	07OCT12:191SAM		73	46.2	
379GLBR- 106	379GLBR- 60	09OCT12:002SAM		60	45.8	
379GLBR- 115       23OCT1:303SA2M       47       41.1       53.7         379GLBR- 119       23OCT4:314SA2M       70       38.2       52.1         379GLBR- 135       24OCT10:457SA2M       137       51.3       58.9         379GLBR- 138       24OCT10:508SA2M       84       42.3       48.8         379GLBR- 146       24OCT6:203SA3M       68       40.6       52.4         379GLBR- 150       25OCT9:194SA3M       61       41.3       52.7         379GLBR- 154       25OCT9:104SA3M       66       42.7       54.9         379GLBR- 155       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:334SB1M       47       37.6       64.3         379GLBR- 186       25OCT2:334SB1M       56       45.7       65.7         379GLBR- 192       25OCT3:558SB1M       129       48.2       65.1         379GLBR- 207 Rep 1       30OCT4:463	379GLBR- 103	22OCT11:287SA1M		110	55.3	
379GLBR- 119       23OCT4:314SA2M       70       38.2       52.1         379GLBR- 135       24OCT10:457SA2M       137       51.3       58.9         379GLBR- 138       24OCT10:508SA2M       84       42.3       48.8         379GLBR- 146       24OCT6:203SA3M       68       40.6       52.4         379GLBR- 150       25OCT9:194SA3M       61       41.3       52.7         379GLBR- 154       25OCT9:104SA3M       66       42.7       54.9         379GLBR- 155       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B         BIN B         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 186       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 195       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 207 Rep 1       30OCT4:463SB2M       70       41.1       56.4	379GLBR- 106	22OCT11:358SA1M		155	55.4	56.6
379GLBR- 135       24OCT10:457SA2M       137       51.3       58.9         379GLBR- 138       24OCT10:508SA2M       84       42.3       48.8         379GLBR- 146       24OCT6:203SA3M       68       40.6       52.4         379GLBR- 150       25OCT9:194SA3M       61       41.3       52.7         379GLBR- 154       25OCT9:104SA3M       66       42.7       54.9         379GLBR- 155       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 186       25OCT2:334SB1M       56       45.7       65.7         379GLBR- 192       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR- 207 Rep 2       30OCT4:363SB2M       70       41.1       56.4         379GLBR- 207 Rep 3       30OCT4:363	379GLBR- 115	23OCT1:303SA2M		47	41.1	53.7
379GLBR- 138       24OCT10:508SA2M       84       42.3       48.8         379GLBR- 146       24OCT6:203SA3M       68       40.6       52.4         379GLBR- 150       25OCT9:194SA3M       61       41.3       52.7         379GLBR- 154       25OCT9:104SA3M       66       42.7       54.9         379GLBR- 155       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B      379GLBR- 68  09OCT10:502SBM 51 43.0 58.2  379GLBR- 177 25OCT2:153SB1M 47 37.6 64.3  379GLBR- 186 25OCT2:334SB1M 56 45.7 65.7  379GLBR- 192 25OCT3:558SB1M 129 48.2 65.1  379GLBR- 195 25OCT3:558SB1M 129 48.2 65.1  379GLBR- 195 25OCT3:558SB1M 121 46.2 58.4  379GLBR- 207 Rep 1 30OCT4:463SB2M 46 44.9 65.7  379GLBR- 207 Rep 3 30OCT4:463SB2M 70 41.1 56.4  379GLBR- 207 Rep 3 30OCT4:463SB2M 57 43.0 62.9  379GLBR- 208 31OCT9:007SB2M 106 46.8 67.0  379GLBR- 211 31OCT9:08SB2M 77 47.1 64.5  379GLBR- 245 31OCT9:274SB2M 44 45.6 67.0  379GLBR- 245 31OCT2:384SB3M 58 44.1 61.1  379GLBR- 246 31OCT10:453SB3M 55 43.2 60.6  379GLBR- 265 1NOV10:208SB3M 117 49.5 61.3	379GLBR- 119	230CT4:314SA2M		70	38.2	52.1
379GLBR- 146       24OCT6:203SA3M       68       40.6       52.4         379GLBR- 150       25OCT9:194SA3M       61       41.3       52.7         379GLBR- 154       25OCT9:104SA3M       66       42.7       54.9         379GLBR- 155       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B         BIN B     379GLBR- 68  09OCT10:502SBM 51 43.0 58.2 379GLBR- 177 25OCT2:153SB1M 47 37.6 64.3 379GLBR- 186 25OCT2:334SB1M 56 45.7 65.7 379GLBR- 192 25OCT3:517SB1M 129 48.2 65.1 379GLBR- 195 25OCT3:558SB1M 121 46.2 58.4 379GLBR- 195 25OCT3:558SB1M 121 46.2 58.4 379GLBR- 207 Rep 1 30OCT4:463SB2M 46 44.9 65.7 379GLBR- 207 Rep 2 30OCT4:463SB2M 70 41.1 56.4 379GLBR- 207 Rep 3 30OCT4:463SB2M 57 43.0 62.9 379GLBR- 208 31OCT9:007SB2M 106 46.8 67.0 379GLBR- 211 31OCT9:088SB2M 77 47.1 64.5 379GLBR- 215 31OCT9:274SB2M 44 45.6 67.0 379GLBR- 245 31OCT2:384SB3M 58 44.1 61.1 379GLBR- 246 31OCT10:453SB3M 55 43.2 60.6 379GLBR- 265 1NOV10:208SB3M 117 49.5 61.3	379GLBR- 135	24OCT10:457SA2M		137	51.3	58.9
379GLBR- 150       25OCT9:194SA3M       61       41.3       52.7         379GLBR- 154       25OCT9:104SA3M       66       42.7       54.9         379GLBR- 155       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 186       25OCT2:334SB1M       56       45.7       65.7         379GLBR- 192       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 195       25OCT3:558SB1M       121       46.2       58.4         379GLBR- 207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR- 207 Rep 2       30OCT4:463SB2M       57       43.0       62.9         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 245       31OCT9:38SB3M <td>379GLBR- 138</td> <td>24OCT10:508SA2M</td> <td></td> <td>84</td> <td>42.3</td> <td>48.8</td>	379GLBR- 138	24OCT10:508SA2M		84	42.3	48.8
379GLBR- 154       25OCT9:104SA3M       66       42.7       54.9         379GLBR- 155       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         379GLBR- 462       4DEC12:055SA2M       100       41.6       50.5         BIN B         379GLBR- 29       07OCT12:541SBM       63       41.0       49.3         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 186       25OCT2:334SB1M       56       45.7       65.7         379GLBR- 192       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 195       25OCT3:558SB1M       121       46.2       58.4         379GLBR- 207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR- 207 Rep 2       30OCT4:463SB2M       70       41.1       56.4         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 245       31OCT9:0453SB3M <td>379GLBR- 146</td> <td>240CT6:203SA3M</td> <td></td> <td>68</td> <td>40.6</td> <td>52.4</td>	379GLBR- 146	240CT6:203SA3M		68	40.6	52.4
379GLBR- 155       25OCT9:287SA3M       148       47.1       56.7         379GLBR- 168       25OCT9:338SA3M       88       43.1       48.0         BIN B         A1.0       49.3         379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 192       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 195       25OCT3:558SB1M       121       46.2       58.4         379GLBR- 207 Rep 1       30OCT4:463SB2M       70       41.1       56.4         379GLBR- 208       31OCT9:07SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:08SB2M       77	379GLBR- 150	250CT9:194SA3M		61	41.3	52.7
BIN B           379GLBR- 462         4DEC12:055SA2M         100         41.6         50.5           BIN B           A1.0         49.3           379GLBR- 68         09OCT10:502SBM         51         43.0         49.3           379GLBR- 177         25OCT2:153SBIM         47         37.6         64.3           379GLBR- 186         25OCT2:334SB1M         56         45.7         65.7           379GLBR- 195         25OCT3:558SB1M         129         48.2         65.1           379GLBR- 207 Rep 1         30OCT4:463SB2M         46         44.9         65.7           379GLBR- 207 Rep 2         30OCT4:463SB2M         70         41.1         56.4           379GLBR- 208         31OCT9:007SB2M         106         46.8         67.0           379GLBR- 215         31OCT9:038SB2M         77	379GLBR- 154	250CT9:104SA3M		66	42.7	54.9
BIN B		25OCT9:287SA3M		148	47.1	56.7
BIN B  379GLBR- 29 07OCT12:541SBM 63 41.0 49.3 379GLBR- 68 09OCT10:502SBM 51 43.0 58.2 379GLBR- 177 25OCT2:153SB1M 47 37.6 64.3 379GLBR- 186 25OCT2:334SB1M 56 45.7 65.7 379GLBR- 192 25OCT3:517SB1M 129 48.2 65.1 379GLBR- 195 25OCT3:558SB1M 121 46.2 58.4 379GLBR- 207 Rep 1 30OCT4:463SB2M 46 44.9 65.7 379GLBR- 207 Rep 2 30OCT4:463SB2M 70 41.1 56.4 379GLBR- 207 Rep 3 30OCT4:463SB2M 57 43.0 62.9 379GLBR- 208 31OCT9:007SB2M 106 46.8 67.0 379GLBR- 211 31OCT9:088SB2M 77 47.1 64.5 379GLBR- 215 31OCT9:274SB2M 44 45.6 67.0 379GLBR- 245 31OCT2:384SB3M 58 44.1 61.1 379GLBR- 246 31OCT10:453SB3M 55 43.2 60.6 379GLBR- 265 1NOV10:208SB3M 117 49.5 61.3	379GLBR- 168	250CT9:338SA3M		88	43.1	48.0
379GLBR- 29 07OCT12:541SBM 63 41.0 49.3 379GLBR- 68 09OCT10:502SBM 51 43.0 58.2 379GLBR- 177 25OCT2:153SB1M 47 37.6 64.3 379GLBR- 186 25OCT2:334SB1M 56 45.7 65.7 379GLBR- 192 25OCT3:517SB1M 129 48.2 65.1 379GLBR- 195 25OCT3:558SB1M 121 46.2 58.4 379GLBR- 207 Rep 1 30OCT4:463SB2M 46 44.9 65.7 379GLBR- 207 Rep 2 30OCT4:463SB2M 70 41.1 56.4 379GLBR- 207 Rep 3 30OCT4:463SB2M 57 43.0 62.9 379GLBR- 208 31OCT9:007SB2M 106 46.8 67.0 379GLBR- 211 31OCT9:088SB2M 77 47.1 64.5 379GLBR- 215 31OCT9:274SB2M 44 45.6 67.0 379GLBR- 245 31OCT2:384SB3M 58 44.1 61.1 379GLBR- 246 31OCT10:453SB3M 55 43.2 60.6 379GLBR- 265 1NOV10:208SB3M 117 49.5 61.3	379GLBR- 462	4DEC12:055SA2M		100	41.6	50.5
379GLBR- 29 07OCT12:541SBM 63 41.0 49.3 379GLBR- 68 09OCT10:502SBM 51 43.0 58.2 379GLBR- 177 25OCT2:153SB1M 47 37.6 64.3 379GLBR- 186 25OCT2:334SB1M 56 45.7 65.7 379GLBR- 192 25OCT3:517SB1M 129 48.2 65.1 379GLBR- 195 25OCT3:558SB1M 121 46.2 58.4 379GLBR- 207 Rep 1 30OCT4:463SB2M 46 44.9 65.7 379GLBR- 207 Rep 2 30OCT4:463SB2M 70 41.1 56.4 379GLBR- 207 Rep 3 30OCT4:463SB2M 57 43.0 62.9 379GLBR- 208 31OCT9:007SB2M 106 46.8 67.0 379GLBR- 211 31OCT9:088SB2M 77 47.1 64.5 379GLBR- 215 31OCT9:274SB2M 44 45.6 67.0 379GLBR- 245 31OCT2:384SB3M 58 44.1 61.1 379GLBR- 246 31OCT10:453SB3M 55 43.2 60.6 379GLBR- 265 1NOV10:208SB3M 117 49.5 61.3			1			
379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 186       25OCT2:334SB1M       56       45.7       65.7         379GLBR- 192       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 195       25OCT3:558SB1M       121       46.2       58.4         379GLBR- 207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR- 207 Rep 2       30OCT4:463SB2M       70       41.1       56.4         379GLBR- 207 Rep 3       30OCT4:463SB2M       57       43.0       62.9         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3		BINB	1			
379GLBR- 68       09OCT10:502SBM       51       43.0       58.2         379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 186       25OCT2:334SB1M       56       45.7       65.7         379GLBR- 192       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 195       25OCT3:558SB1M       121       46.2       58.4         379GLBR- 207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR- 207 Rep 2       30OCT4:463SB2M       70       41.1       56.4         379GLBR- 207 Rep 3       30OCT4:463SB2M       57       43.0       62.9         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 29	07OCT12:541SBM		63	41.0	49.3
379GLBR- 177       25OCT2:153SB1M       47       37.6       64.3         379GLBR- 186       25OCT2:334SB1M       56       45.7       65.7         379GLBR- 192       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 195       25OCT3:558SB1M       121       46.2       58.4         379GLBR- 207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR- 207 Rep 2       30OCT4:463SB2M       70       41.1       56.4         379GLBR- 207 Rep 3       30OCT4:463SB2M       57       43.0       62.9         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 68					
379GLBR- 186       25OCT2:334SB1M       56       45.7       65.7         379GLBR- 192       25OCT3:517SB1M       129       48.2       65.1         379GLBR- 195       25OCT3:558SB1M       121       46.2       58.4         379GLBR- 207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR- 207 Rep 2       30OCT4:463SB2M       70       41.1       56.4         379GLBR- 207 Rep 3       30OCT4:463SB2M       57       43.0       62.9         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 177	25OCT2:153SB1M		47		
379GLBR-       195       25OCT3:558SB1M       121       46.2       58.4         379GLBR-       207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR-       207 Rep 2       30OCT4:463SB2M       70       41.1       56.4         379GLBR-       207 Rep 3       30OCT4:463SB2M       57       43.0       62.9         379GLBR-       208       31OCT9:007SB2M       106       46.8       67.0         379GLBR-       211       31OCT9:088SB2M       77       47.1       64.5         379GLBR-       215       31OCT9:274SB2M       44       45.6       67.0         379GLBR-       245       31OCT2:384SB3M       58       44.1       61.1         379GLBR-       246       31OCT10:453SB3M       55       43.2       60.6         379GLBR-       265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 186	25OCT2:334SB1M		56	45.7	
379GLBR- 207 Rep 1       30OCT4:463SB2M       46       44.9       65.7         379GLBR- 207 Rep 2       30OCT4:463SB2M       70       41.1       56.4         379GLBR- 207 Rep 3       30OCT4:463SB2M       57       43.0       62.9         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 192	25OCT3:517SB1M		129	48.2	65.1
379GLBR- 207 Rep 2       30OCT4:463SB2M       70       41.1       56.4         379GLBR- 207 Rep 3       30OCT4:463SB2M       57       43.0       62.9         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 195	25OCT3:558SB1M		121	46.2	58.4
379GLBR- 207 Rep 3       30OCT4:463SB2M       57       43.0       62.9         379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 207 Rep 1	30OCT4:463SB2M		46	44.9	65.7
379GLBR- 208       31OCT9:007SB2M       106       46.8       67.0         379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 207 Rep 2	30OCT4:463SB2M		70	41.1	56.4
379GLBR- 211       31OCT9:088SB2M       77       47.1       64.5         379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 207 Rep 3	30OCT4:463SB2M		57	43.0	62.9
379GLBR- 215       31OCT9:274SB2M       44       45.6       67.0         379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 208	31OCT9:007SB2M		106	46.8	67.0
379GLBR- 245       31OCT2:384SB3M       58       44.1       61.1         379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 211	31OCT9:088SB2M	÷, - /	77	47.1	64.5
379GLBR- 246       31OCT10:453SB3M       55       43.2       60.6         379GLBR- 265       1NOV10:208SB3M       117       49.5       61.3	379GLBR- 215			44	45.6	67.0
379GLBR- 265 1NOV10:208SB3M 117 49.5 61.3	379GLBR- 245	310CT2:384SB3M		58	44.1	61.1
	379GLBR- 246	31OCT10:453SB3M		55	43.2	60.6
379GLBR- 267 1NOV10:157SB3M 130 47.8 62.3	379GLBR- 265	1NOV10:208SB3M		117	49.5	61.3
	379GLBR- 267	1NOV10:157SB3M		130	47.8	62.3

MSL Code	Sponsor ID	Cr (ug.	/g) Cu (ug/g) xəғ	Pb (ug/g) xaf
	. BIN C	]		
379GLBR- 26	07OCT1:261SCM		30 56.8	88.8
379GLBR- 76	09OCT5:052SCM		71 47.8	62.3
379GLBR- 285	18NOV4:403SC1M		73 45.3	68.4
379GLBR- 300	19NOV8:484SC1M	•	57 58.0	70.6
379GLBR- 305	19NOV9:218SC1M	12	29 62.1	59.7
379GLBR- 308	19NOV9:327SC1M	13	<b>54.8</b>	83.8
379GLBR- 316	19NOV3:553SC2M		59 48.2	71.9
379GLBR- 320 Rep 1	19NOV4:414SC2M	7	75 47.6	68.6
379GLBR- 320 Rep 2	19NOV4:414SC2M	•	51.4	67.4
379GLBR- 320 Rep 3	19NOV4:414SC2M	3	37 47.4	65.5
379GLBR- 336	20NOV8:157SC2M	12	29 56.1	70.7
379GLBR- 345	20NOV1:553SC3M	•	9 47.2	56.3
379GLBR- 353	20NOV3:184SC3M	• 6	45.4	58.3
379GLBR- 356	20NOV3:327SC3M	14	62.4	70.4
379GLBR- 359	20NOV3:268SC3M	14	52.5	61.7
	BIN D	]		
379GLBR- 28	07OCT2:001SDM	7	4 37.7	49.7
379GLBR- 49 Rep 1	08OCT4:572SDM	4	9 44.5	65.0
379GLBR- 49 Rep 2	08OCT4:572SDM	•5	6 42.8	60.3
379GLBR- 49 Rep 3	08OCT4:572SDM	. 7	6 47.1	61.7
379GLBR- 381	21NOV2:43ESD1M	5	5 44.8	73.5
379GLBR- 383	212NOV4:578SD1M	11	8 53.7	71.8
379GLBR- 386	21NOV5:087SD1M	11	2 51.3	63.6
379GLBR- 390	21NOV5:194SD1M	6	2 47.6	64.7

			Cr	(ug/g)	Cu (ug/g)	Pb (ug/g)
MSL Code		Sponsor ID		XRF	XPF	XRF
STANDARD RE	FERENC	E MATERIAL				
SRM 1646	Rep 1			61	22.1	26.9
SRM 1646	Rep 2			78	19.7	28.3
SRM 1646	Rep 3			78	23.2	29.1
SRM1646	Rep 4			72	20.9	29.3
		certified		76	18	28.2
		value		±3	±3	±1.8
SRM 2704	Rep 1			140	91.6	156.5
SRM 2704	Rep 2			134	97.5	156.2
SRM 2704	Rep 3			139	92.9	155.1
	·	certified		135	98.6	161.0
		value		±5	±5.0	±17.0
REPLICATE AN	IALYSIS					
379GLBR- 207	Rep 1	300CT4:463SB2M		46	44.9	65.7
379GLBR- 207	Rep 2	300CT4:463SB2M		70	41.1	56.4
379GLBR- 207		30OCT4:463SB2M		57	43	62.9
	•	RSD %		21%	4%	8%
379GLBR- 320	Rep 1	19NOV4:424SC2M		75	47.6	68.6
379GLBR- 320	Rep 2	19NOV4:424SC2M		63	51.4	67.4
379GLBR- 320	•	19NOV4:424SC2M		37	47.4	65.5
	•	RSD %		33%	5%	2%
379GLBR- 49	Rep 1	08OCT4:572SDM		49	44.5	65
379GLBR- 49	Rep 2	08OCT4:572SDM		56	42.8	60.3
379GLBR- 49	Rep 3	08OCT4:572SDM		76	47.1	61.7
		RSD %		23%	5%	4%

RSD % = Relative Standard Deviation.

MSL Code	Sponsor ID	Hg (ug/g)
	BIN A	
379GLBR- 8	070CT12:301SAL	0.112
379GLBR- 27	07OCT12:191SAM	0.183
379GLBR- 60	09OCT12:002SAM	0.192
379GLBR- 103	22OCT11:287SA1M	0.183
379GLBR- 106	22OCT11:358SA1M	0.089
379GLBR- 115	23OCT1:303SA2M	0.171
379GLBR- 119	230CT4:314SA2M	0.002
379GLBR- 135	24OCT10:457SA2M	0.146
379GLBR- 138	24OCT10:508SA2M	0.023
379GLBR- 146	24OCT6:203SA3M	0.175
379GLBR- 150	25OCT9:194SA3M	0.045
379GLBR- 154	25OCT9:L104SA3M	0.027
379GLBR- 155	25OCT9:287SA3M	0.120
379GLBR- 168	25OCT9:338SA3M	0.036
379GLBR- 462	4DEC12:055SA2M	0.017
	BIN B	
379GLBR- <b>29</b>	07OCT12:541SBM	0.170
379GLBR- 68	09OCT10:502SBM	0.208
379GLBR- 177	25OCT2:153SB1M	0.203
379GLBR- 186	25OCT2:334SB1M	0.111
379GLBR- 192	25OCT3:517SB1M	0.132
379GLBR- 195	25OCT3:558SB1M	0.121
379GLBR- 207 Rep 1	30OCT4:463SB2M	0.190
379GLBR- 207 Rep 2	30OCT4:463SB2M	0.205
379GLBR- 207 Rep 3	30OCT4:463SB2M	0.203
379GLBR- 208	31OCT9:007SB2M	0.102
379GLBR- 211	31OCT9:088SB2M	0.023
379GLBR- 215	31OCT9:274SB2M	<0.0003
379GLBR- 245	31OCT2:384SB3M	0.032
379GLBR- 246	31OCT10:453SB3M	0.173
379GLBR- 265	1NOV10:208SB3M	0.084
379GLBR- 267	1NOV10:157SB3M	0.175

	<u>-                                    </u>		Hg (ug/g)
MSL Code		Sponsor ID	CVAA
		•	
	· · · · · · · · · · · · · · · · · · ·	BIN C	
379GLBR- 23		07OCT1:261SCM	0.335
379GLBR- 76		09OCT5:052SCM	0.335
379GLBR- 285	5	18NOV4:403SC1M	0.198
379GLBR- 300		19NOV8:484SC1M	0.065
379GLBR- 305		19NOV9:218SC1M	0.300
379GLBR- 308		19NOV9:327SC1M	0.323
379GLBR- 316		19NOV3:553SC2M	0.213
379GLBR- 320		19NOV4:414SC2M	0.046
379GLBR- 320	•	19NOV4:414SC2M	0.054
379GLBR- 320	•	19NOV4:414SC2M	0.052
379GLBR- 336	•	20NOV8:157SC2M	0.228
379GLBR- 345		20NOV1:553SC3M	0.175
379GLBR- 353		20NOV3:184SC3M	0.151
379GLBR- 356		20NOV3:327SC3M	0.487
379GLBR- 359		20NOV3:268SC3M	0.060
		BIN D	
379GLBR- 28		07OCT2:001SDM	0.110
379GLBR- 49	Rep 1	08OCT4:572SDM	0.214
379GLBR- 49	Rep 2	08OCT4:572SDM	0.207
379GLBR- 49	Rep 3	08OCT4:572SDM	0.233
379GLBR- 381	•	21NOV2:433SD1M	0.187
379GLBR- 383		21NOV4:578SD1M	0.034
379GLBR- 386		21NOV5:087SD1M	0.209
379GLBR- 390		21NOV5:194SD1M	0.014
Blank	Rep 1		0.0003
Blank	Rep 2		0.0003
Blank	Rep 3		0.0003
Blank	Rep 4		0.0003
Blank	Rep 5		0.0003

MSL Code		Sponsor ID	Hg (ug/g)
STANDARD R	EFERENCE M	IATERIAL	
SRM 1646	Rep 1		0.072
SRM 1646	Rep 2		0.076
SRM 1646	Rep 3		0.070
SRM 1646	Rep 4		0.066
		certified	0.063
		value	±0.012
SRM 2704	Rep 1		1.434
SRM 2704	Rep 2		1.439
SRM 2704	Rep 3		1.450
		certified	1.44
		value	±0.07
MATRIX SPIK	E RESULTS		
Amount Spike	ed		0.500
379GLBR-8		07OCT12:301SAL	0.112
379GLBR-8 +	Spike		0.647
Amount Reco	vered		0.535
Percent Reco	very		107%
Amount Chile		Mark the state of	0.500
Amount Spike 379GLBR-8		. 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.500 0.112
379GLBR-8 +			0.112
Amount Recov	•	•	0.555
Percent Reco	· · · · · · · · · · · · · · · ·		111%
Amount Spike	d :		0.500
379GLBR-49	<b>.</b>	08OCT4:572SDM	0.214
379GLBR-49	•		0.649
Amount Recov			0.435
Percent Reco	very		87%
Amount Spike	d		0.500
379GLBR-49	DUPLICATE		0.207
379GLBR-49 +	•		0.639
Amount Recov			0.432
Percent Reco	very		86%

MSL Code	Sponsor ID	Hg (ug/g)
	•	
MATRIX SPIKE RESULTS		
Amount Spiked		0.500
379GLBR-207	30OCT4:463SB2M	0.190
379GLBR-207+ Spike		0.703
Amount Recovered		0.513
Percent Recovery		103%
Amount Spiked		0.500
379GLBR-207 DUPLICATE		0.205
379GLBR-207+ Spike		0.659
Amount Recovered		0.454
Percent Recovery		91%
Amount Spiked		0.500
379GLBR-320	19NOV4:424SC2M	0.046
379GLBR-320+ Spike		0.501
Amount Recovered		0.455
Percent Recovery		91%
Amount Spiked		0.500
379GLBR-320 DUPLICATE		0.054
379GLBR-320+ Spike		0.516
Amount Re∞vered		0.462
Percent Recovery		92%

MSL Code	Sponsor ID	Hg (ug/g)
REPLICATE ANALYSIS	· Major in the	
379GLBR- 207 Rep 1	30OCT4:463SB2M	0.190
379GLBR- 207 Rep 2	30OCT4:463SB2M	0.205
379GLBR- 207 Rep 3	30OCT4:463SB2M	0.203
	RSD %	4%
379GLBR- 320 Rep 1	19NOV4:424SC2M	0.046
379GLBR- 320 Rep 2	19NOV4:424SC2M	0.054
379GLBR- 320 Rep 3	19NOV4:424SC2M	0.052
	RSD %	8%
379GLBR- 49 Rep 1	08OCT4:572SDM	0.214
379GLBR- 49 Rep 2	08OCT4:572SDM	0.207
379GLBR- 49 Rep 3	08OCT4:572SDM	0.233
<b>,</b> 	RSD %	6%

RSD % = Relative Standard Deviation.

# BUFFALO RIVER PILOT PROJECT (CF #379) METALS IN WATER SAMPLES

		Cr	Cu	Pb	
MSL Code	Sponsor ID	ug/L	ug/L	ug/L	
MDL - Flame AA	•	40	50	100	
MDL - Graphite Furnace AA		0.22	0.72	1.03	
	BIN A				
	· · · · · · · · · · · · · · · · · · ·				
379GLBR- 127	23OCT4:459LA2M	13130	25590	12600	
379GLBR- 131	23OCT5:2510LA2M	1080	1350	1040	
379GLBR- 133 REP1	23OCT5:2010LA2M	4.15	830	2.97 *	F
379GLBR- 133 REP 2	23OCT5:2010LA2M	4.40 *	830	2.97 *	F
379GLBR- 133 REP 3	23OCT5:2010LA2M	4.15 *	820	3.56 *	F
379GLBR- 163	25OCT10:2010LA3M	600	570	230	
379GLBR- 170	250CT11:0010LA3M	2.89 *	410	1.19 *	F
379GLBR- 171	250CT10:009LA3M	14200	7100	7100	
379GLBR- 203	30OCT4:216LA3M	1.13 *	4.17 *	1.19 *	
	BIN B				
070CLDD 400	050070:404010414	4070			
379GLBR- 188 379GLBR- 189	25OCT3:1210LB1M	1870	840	900	_
379GLBR- 189 379GLBR- 223	25OCT3:3010LB1M	2.52 *	340	3.56 *	F
379GLBR- 228	31OCT10:089LB2M	22.4 *	2800	32.6 *	
	31OCT10:2010LB2M	200	560	154 *	-
379GLBR- 229 REP 1	31OCT10:3010LB2M	1.76 *	450	1.78 *	F
379GLBR- 229 REP 2	31OCT10:3010LB2M	1.76 *	450	2.37 •	F
379GLBR- 229 REP 3 379GLBR- 251	31OCT10:3010LB2M	1.76 *	450	2.37 *	F
379GLBR- 254	31OCT3:5010LB3M	1.76 *	330	25.5 *	F
379GLBR- 255	31OCT2:5710LB3M 31OCT3:069LB3M	270	520	200	
379GLBR- 270		120	1830	140	
379GLBR- 274	1NOV11:006LB2M 1NOV2:506LB1B3M	2.39 *	5.83 <b>*</b> 14.2 <b>*</b>	1.19 *	
3/3GLDN- 2/4	1140 42.500LB 1 B5/M	1.51 *	14.2	1.19 *	
	BIN C				
379GLBR- 290	18NOV5:309LC1M	830	3660	810	
379GLBR- 292	18NOV6:1810LC1M	2.77 *	720	1.78 *	F
379GLBR- 293	18NOV6:1810LC1M	230	1410	330	•
379GLBR- 328	19NOV5:559LC2M	410	2220	410	
379GLBR- 333 REP1	19NOV5:2010LC2M	1.64 *	120	13.1 *	F
379GLBR- 333 REP 2	19NOV5:2010LC2M	1.64 *	110	14.2 *	F
379GLBR- 333 REP 3	19NOV5:2010LC2M	2.14 *	120	14.8 *	F
379GLBR- 334	19NOV5:3510LC2M	160	260	180	
379GLBR- 362	20NOV2:173LC3M	1.51 *	5.00 *	2.37 *	F
379GLBR- 363	20NOV2:173LC3M	1.51 *	7.91 *	4.15 *	

NOTE: Sample values are not blank-corrected.

# BUFFALO RIVER PILOT PROJECT (CF #379) METALS IN WATER SAMPLES

		C.r	Cu	Pb	
MSL Code	Sponsor ID	ug/L	ug/L	ug/L	
MDL - Flame AA		40	50	100	
MDL - Graphite Furnace AA		0.22	0.72	1.03	
	BIN C				
379GLBR- 368	20NOV2:435LC3M	1140	1010	19.6 *	
379GLBR- 371	20NOV3:0310LC3M	170	190	160	164
379GLBR- 372	20NOV3:0710LC3M	1.01 *	70	17.8 *	F
	BIN D				
379GLBR- 399	21NOV3:3810LD1M	340	860	250	
379GLBR- 400	21NOV3:4510LD1M	1.64 *	755 °	8.90 *	F
379GLBR- 405 REP 1	21NOV4:359LD1M	800	1950	580	•
379GLBR- 405 REP 2	21NOV4:359LD1M	620	1950	560	
379GLBR- 405 REP 3	21NOV4:359LD1M	750	1950	560	
379GLBR- 429	22NOV2:3210LD2M	530	950	440	
379GLBR- 430	22NOV2:4010LD2M	2.52 *	630	9.49 *	F
379GLBR- 434	22NOV2:559LD2M	840	1310	540	
379GLBR- 457	25NOV4:009LD3M	790	3000	1620 *	
	DILUTION WATER				
379GLBR- 277	6NOV12:003LM	2.26 *	17.9 *	2.37 *	
Blank Rep 1	(Flame AA)	40 U	50 U	100 U	
Blank Rep 2		40 U	50 U	100 U	
Blank Rep 3		40 U	50 U	100 U	
Blank Rep 4		40 U	50 U	100 U	
Blank Rep 1	(Graphite Furnace AA)	1.13 *	4.17 *	1.03 U*	
Blank Rep 2		6.67 *	4.17 *	1.03 U*	
Blank Rep 3		1.01	3.33 *	1.03 U*	
Blank Rep 4		1.13 *	4.58 *	1.03 U*	

NOTE: Sample values are not blank-corrected.

# BUFFALO RIVER PILOT PROJECT (CF #379) METALS IN WATER SAMPLES

	,		Cr	Cu	Pb
MSL Code	Sponso	r ID	ug/L	ug/L	ug/L
MDL - Flame AA		•	40	50	100
MDL - Graphite Fur			0.22	0.72	1.03
STANDARD RE	FERENCE MATER	RIAL			
SRM 1643c	Rep 1		21.5 *	29.2 •	<b>35</b> .6 *
SRM 1643c	Rep 2		21.5 *	26.7 *	36.8 *
SRM 1643c	Rep 3		19.1 *	28.7 *	36.8 °
SRM 1643c	Rep 4		20.4 *	27.1 *	33.8
		certified	19.0	22.3	35.3
		value	±0.6	±2.8	±0.9
NOTE: SRM v	alues are not biai	nk-corrected.			
MATRIX SPIKE	RESULTS - FLA	ME AA			
Amount Spiked			1000	1000	1000
379GLBR- 203		•	40 U	50 U	100 U
379GLBR- 203			940	1030	1080
Amount Recove	•		940	1030	1080
Percent Recove	ered		94%	103%	108%
Amount Spiked			1000	1000	1000
379GLBR- 203			40 U	50	100 U
	+ Spike DUPLIC	ATE	890	1050	1060
Amount Recove	•		890	1050	1060
Percent Recove			89%	105%	106%
Amount Spiked			1000	1000	1000
379GLBR- 274			40 U	50 U	100 U
379GLBR- 274			890	990	1010
Amount Recove	•		890	990	1010
Percent Recove			89%	99%	101%
Amount Spiked			1000	1000	1000
379GLBR- 274			40 U	50 U	100 U
	+ Spike DUPLICA	ATE	1020	1140	1110
Amount Recove	•		1020	1140	1110
	· - <del>-</del>		·	<del>.</del>	· · · <del>-</del>

NOTE: Spike data run by Flame AA is not blank-corrected.

## BUFFALO RIVER PILOT PROJECT (CF #379) METALS IN WATER SAMPLES

		Cr	Cu	Pb	
MSL Code	Sponsor ID	ug/L	ug/L	ug/L	
MDL - Flame AA	_	40	50	100	
MDL - Graphite Furnace AA		0.22	0.72	1.03	
Amount Spiked		1000	1000	1000	
379GLBR- 362		40 U	50 U	100 U	
379GLBR- 362 + Spike		1030	1020	1000	
Amount Recovered		1030	1020	1000	
Percent Recovered		103%	102%	100%	
Amount Spiked		1000	1000	1000	
379GLBR- 362		40 U	50 U	100 U	
379GLBR- 362 + Spike	DUPLICATE	1040	1040	980	
Amount Recovered		1040	1040	980	
Percent Recovered		104%	104%	98%	
Amount Spiked		1000	1000	1000	
379GLBR- 400		40 U	330	100 U	
379GLBR- 400 + Spike		1040	1360	1020	
Amount Recovered •		1040	1030	1020	
Percent Recovered		104%	103%	102%	
Amount Spiked		1000	1000	1000	
379GLBR- 400		40 U	330	100 U	
379GLBR- 400 + Spike	DUPLICATE	1040	1370	980	
Amount Recovered		1040	1040	980	
Percent Recovered		104%	104%	98%	

NOTE: Spike data run by Flame AA is not blank-corrected

#### MATRIX SPIKE RESULTS - GRAPHITE FURNACE AA

Amount Spiked	1000	1000	1000
379GLBR- 203	0.22 U	0.72 U	1.19
379GLBR- 203 + Spike	1091	1110	919
Amount Recovered	1091	1110	917
Percent Recovered	109%	111%	92%
Amount Spiked	1000	1000	1000
379GLBR- 203	0.22 U	0.72 U	1.19
379GLBR- 203 + Spike DUPLICATE	1062	977	912
Amount Re∞vered	1062	977	911
Percent Recovered	106%	98%	91%

NOTE: Spike data run by Graphite Furnace AA is blank-corrected.

## BUFFALO RIVER PILOT PROJECT (CF #379) METALS IN WATER SAMPLES

	Cr	Cu	Pb
MSL Code Sponsor ID	ug/L	ug/L	ug/L
MDL - Flame AA	40	50	100
MDL - Graphite Furnace AA	0.22	0.72	1.03
Amount Spiked	1000	1000	1000
379GLBR- 274	0.38	10.0	1.19
379GLBR- 274 + Spike	1120	933	1057
Amount Recovered	1120	923	1055
Percent Recovered	112%	92%	106%
Amount Spiked	1000	1000	1000
379GLBR- 274	0.38	10.0	1.19
379GLBR- 274 + Spike DUPLICATE	1152	1066	1057
Amount Recovered	1152	1056	1055
Percent Recovered	115%	106%	106%
Amount Spiked	1000	1000	1000
379GLBR- 362	0.38	0.83	2.37
379GLBR- 362 + Spike	1052	1155	977
Amount Recovered	1052	1154	974
Percent Recovered	105%	115%	97%
Amount Spiked	1000	1000	1000
379GLBR- 362	0.38	0.83	2.37
379GLBR- 362 + Spike DUPLICATE	1023	1066	957
Amount Recovered	1023	1065	955
Percent Recovered	102%	107%	95%
Amount Spiked	1000	1000	1000
379GLBR- 400	0.50	577	8.90
379GLBR- 400 + Spike	1101	1421	983
Amount Re∞vered	1100	844	974
Percent Recovered	110%	84%	97%
Amount Spiked	1000	1000	1000
379GLBR- 400	0.50	577	8.90
379GLBR- 400 + Spike DUPLICATE	1110	1643	964
Amount Recovered	1110	1066	955
Percent Recovered	111%	107%	95%

NOTE: Spike data run by Graphite Furnace AA is blank-corrected.

## BUFFALO RIVER PILOT PROJECT (CF #379) METALS IN WATER SAMPLES

		Cr	Cu	Pb	
MSL Code	Sponsor ID	ug/L	ug/L	ug/L	
MDL - Flame AA	•	40	50	100	
MDL - Graphite Furnace AA		0.22	0.72	1.03	
REPLICATE ANALYSIS	1				
379GLBR- 130 REP1	23OCT5:2010LA2M	4.15 *	0.83	2.97 *	F
379GLBR- 133 REP 2	23OCT5:2010LA2M	4.40 *	0.83	2.97 *	F
379GLBR- 133 REP3	23OCT5:2010LA2M	4.15 *	0.82	3.56 *	F
	RSD %	3%	1%	11%	
379GLBR- 229 REP 1	31OCT10:3010LB2M	1.76 *	0.45	1.78 *	F
379GLBR- 229 REP 2	31OCT10:3010LB2M	1.76 *	0.45	2.37 *	F
379GLBR- 229 REP3	31OCT10:3010LB2M	1.76 *	0.45	2.37 *	F
	RSD %	0%	0%	16%	
379GLBR- 333 REP 1	19NOV5:2010LC2M	1.64 *	0.12	13.1 *	F
379GLBR- 333 REP 2	19NOV5:2010LC2M	1.64 *	0.11	14.2 *	F
379GLBR- 333 REP3	19NOV5:2010LC2M	2.14 *	0.12	14.8 *	F
	RSD %	16%	5%	6%	
379GLBR- 405 REP 1	21NOV4:359LD1M	800	1950	580	
379GLBR- 405 REP 2	21NOV4:359LD1M	620	1950	560	
379GLBR- 405 REP 3	21NOV4:359LD1M	750	1950	560	
	RSD %	13%	0%	2%	

<sup>\* =</sup> Analyzed by Graphite Furnace AA

RSD % = Relative Standard Deviation.

F = Samples were filtered prior to analysis.

U = Below detection limits

# BUFFALO RIVER PILOT PROJECT (CF #379) MERCURY IN WATER SAMPLES

MSL Code	Sponsor ID	Hg (ug/L) cvaa
	BIN A	
379GLBR- 127	230CT4:459LA2M	64.07
379GLBR- 131	23OCT5:2510LA2M	3.98
379GLBR- 133	23OCT5:2010LA2M	0.96
379GLBR- 163	25OCT10:2010LA3M	7.38
379GLBR- 170	25OCT11:0010LA3M	0.43
379GLBR- 171	25OCT10:009LA3M	3.27
379GLBR- 203	30OCT4:216LA3M	0.001
	BIN B	
970CLDD 400	0500T2:1010LD1M	1.28
379GLBR- 188 379GLBR- 189	25OCT3:1210LB1M 25OCT3:3010LB1M	0.52
379GLBR- 109 379GLBR- 223	31OCT10:089LB2M	5.28
379GLBR- 228	31OCT10:009LB2M	1.83
379GLBR- 229	31OCT10:3010LB2M	1.11
379GLBR- 229	31OCT3:5010LB3M	5.39
379GLBR- 254	31OCT2:5710LB3M	2.37
379GLBR- 255	31OCT3:069LB3M	2.40
379GLBR- 270	1NOV11:006LB2M	< 0.005
379GLBR- 274	1NOV2:506LB1B3M	0.001
	BIN C	
379GLBR- 290 Rep 1	18NOV5:309LC1M	10.99
379GLBR- 290 Rep 2	18NOV5:309LC1M	8.30
379GLBR- 290 Rep 3	18NOV5:309LC1M	8.60
379GLBR- 292	18NOV6:1810LC1M	0.31
379GLBR- 293	18NOV6:1810LC1M	2.37
379GLBR- 328	19NOV5:559LC2M	2.16
379GLBR- 333 Rep 1	19NOV5:2010LC2M	4.40
379GLBR- 333 Rep 2	19NOV5:2010LC2M	4.20
379GLBR- 333 Rep 3	19NOV5:2010LC2M	4.19
379GLBR- 334	19NOV5:3510LC2M	1.83
379GLBR- 362	20NOV2:173LC3M	< 0.005
379GLBR- 363	20NOV2:173LC3M	< 0.005
379GLBR- 368	20NOV2:439LC3M	< 0.005
379GLBR- 371	20NOV3:0310LC3M	0.69
379GLBR- 372	20NOV3:0710LC3M	2.92

# BUFFALO RIVER PILOT PROJECT (CF #379) MERCURY IN WATER SAMPLES

MSL Code		Sponsor ID	Hg (ug/L)
		BIN D	
97001 DD - 07	20	041101/0 00401 0414	
379GLBR- 39		21NOV3:3810LD1M	5.25
379GLBR- 40		21NOV3:4510LD1M	1.48
379GLBR- 40	)5	21NOV4:359LD1M	3.20
		DILUTION WATER	
379GLBR- 27	77	6NOV12:003LM	0.003
Blank 1			0.017
Blank 2			0.021
Blank 3			0.021
			0.047
STANDARD R	EFERENCE	MATERIAL	ng/l
SRM 1641b	Rep 1		1.46
SRM 1641b	Rep 2		1.45
SRM 1641b	Rep 3		1.82
SRM 1641b	Rep 4		1.59
SRM 1641b	Rep 5		1,41
SRM 1641b	Rep 6		1.37
SRM 1641b	Rep 7		1.44
	•	certified	1.52
		value	±0.04
MATRIX SPIKE	E RESULTS		
Amount Spike	d		5
379GLBR-290		18NOV5:309LC1M	9.30
379GLBR-290	+ Spike		15.68
Amount Recov	-		6.38
Percent Recov	very		128%
Amount Spike	4		
379GLBR-290		DUPLICATE	5
379GLBR-290		DUFLICATE	9.30
Amount Recov	•		17.03
Percent Recov			7.73
Fercent Necov	ery		155%

## BUFFALO RIVER PILOT PROJECT (CF #379) MERCURY IN WATER SAMPLES

MSL Code	Sponsor ID	Hg (ug/L)
MATRIX SPIKE RESULTS		
;		
Amount Spiked		5
379GLBR-334	19NOV5:3510LC2M	1.83
379GLBR-334+ Spike		7.58
Amount Recovered		5.76
Percent Recovery		115%
Amount Spiked		5
379GLBF-334	DUPLICATE	1.83
379GLBR-334+ Spike		6.39
Amount Recovered		4.56
Percent Recovery		91%
REPLICATE ANALYSIS		
379GLBR- 290 Rep 1	18NOV5:309LC1M	10.99
379GLBR- 290 Rep 2	18NOV5:309LC1M	8.30
379GLBR- 290 Rep 3	18NOV5:309LC1M	8.60
•	RSD %	16%
379GLBR- 333 Rep 1	19NOV5:2010LC2M	4.40
379GLBR- 333 Rep 2	19NOV5:2010LC2M	4.20
379GLBR- 333 Rep 3	19NOV5:2010LC2M	4.19
•	RSD %	3%

NOTE: All results are blank-corrrected.

RSD % = Relative Standard Deviation.

<sup>\* =</sup> Mean of replicated sample.

MSL Code	Sponsor ID	Total Solids (% Dry Wt.)	Total Volatile Solids (%Dry Wt.)
		(// 5.1) ************************************	Solids (76Diy WL)
	BIN A		
379GLBR- 39	07OCT12:411SAS	55.19	6.39
379GLBR- 44	07OCT12:321SAS	58.13	6.12
379GLBR- 45	07OCT12:121SAS	60.66	6.63
379GLBR- 54	09OCT11:282SA1S	60.54	5.62
379GLBR- 55	09OCT11:382SA2S	62.97	5.96
379GLBR- 56	09OCT11:502SA3S	60.15	6.03
379GLBR- 98	220CT11:307SA1S	64.59	6.46
379GLBR- 105	220CT11:368SA1S	98.45	4.65
379GLBR- 109	22OCT4:203SA2S	52.16	5.84
79GLBR- 110	220CT5:553SA2S	55.62	5.08
379GLBR- 114	23OCT1:303SA2S	55.69	5.72
379GLBR- 116	230CT4:254SA2S	99.81	3.44
379GLBR- 117	230CT4:264SA2S	99.77	3.52
379GLBR- 118	230CT4:274SA2S	99.78	3.22
179GLBR- 134	240CT10:457SA2S	95.34	4.69
79GLBR- 137	240CT10:508SA2S	77.07	2.29
79GLBR- 140 Re	p 1 24OCT2:203SA3S	53.65	5.83
	p 2 24OCT2:203SA3S	53.94	5.96
79GLBR- 140 Re	p 3 24OCT2:203SA3S	55.22	6.08
79GLBR- 142	24OCT5:503SA3S	55.79	5.16
79GLBR- 144	24OCT6:203SA3S	56.42	5.02
79GLBR- 147	25OCT9:234SA3S	99.44	4.54
79GLBR- 148	25OCT9:244SA3S	99.45	3.73
79GLBR- 149	25OCT9:254SA3S	99.48	4.46
79GLBR- 157	25OCT9:307SA3S	97.54	5.42
79GLBR- 169	250CT9:358SA3S	99.57	4.73

			Total Solids	Total Volatile
MSL Code	Sponsor ID		(% Dry Wt.)	Solids (%Dry Wt.)
	BIN B	7		
379GLBR- 36	07OCT1;111SBS		55.89	5.94
379GLBR- 41	07OCT1:021SBS		55.22	5.90
379GLBR- 42	07OCT12:501SBS		54.55	6.62
379GLBR- 62	09OCT9:552SB1S		63.18	5.72
379GLBR- 63	09OCT10:152SB2S		62.04	5.58
379GLBR- 64	09OCT10:352SB3S		63.01	5.61
379GLBR- 172	30OCT2:573SB2S		53.39	4.99
379GLBR- 173	250CT12:153SB1S		55.20	5.28
379GLBR- 175	25OCT2:153SB1S		56.91	5.80
379GLBR- 178	25OCT2:304SB1S		98.81	3.42
379GLBR- 179	250CT2:314SB1S		98.67	3.41
379GLBR- 180	250CT2:324SB1S		98.75	4.22
379GLBR- 191	250CT3:517SB1S		99.07	5.08
379GLBR- 194	25OCT3:568SB1S		99.51	5.00
379GLBR- 200	30OCT4:053SB2S		55.27	5.73
379GLBR- 205	30OCT4:393SB2S		55.16	5.67
379GLBR- 209	31OCT9:017SB2S		87.07	3.83
379GLBR- 212	31OCT9:068SB2S		99.52	3.79
379GLBR- 216 Rep 1	31OCT9:204SB2S		99.84	2.17
379GLBR- 216 Rep 2			99.84	2.81
379GLBR- 216 Rep 3			99.84	2.91
379GLBR- 217	310CT9:234SB2S		99.76	2.04
379GLBR- 218	310CT9:224SB2S		99.71	2.96
379GLBR- 235	310CT2:364SB3S		99.74	3.90
379GLBR- 236	31OCT11:503SB3S		52.57	5.73
379GLBR- 237	31OCT10:453SB3S		55.34	5.80
379GLBR- 238	310CT2:303SB3S		52.45	4.68
379GLBR- 239	310CT2:374SB3S		99.77	4.03
379GLBR- 240	310CT2:374SB3S		99.75	4.41
379GLBR- 264	1NOV10:208SB3S		99.35	4.39
379GLBR- 266	1NOV10:157SB3S		91.30	4.95

MSL Code	Sponsor ID	Total Solids (% Dry Wt.)	Total Volatile Solids (%Dry Wt.)
oz	05011307-113	(70 Diy 441.)	301105 (76DTY VVI.)
	BIN C.		
379GLBR- 37	07OCT1:2012SCS	54.73	6.30
379GLBR- 38	07OCT1:431SCS	64.58	4.29
379GLBR- 40	07OCT1:331SCS	60.22	4.78
379GLBR- 70	09OCT4:362SC2S	63.85	5.25
379GLBR- 71	09OCT4:552SC1S	63.79	4.91
379GLBR- 72	09OCT4:152SC3S	64.78	5.53
379GLBR- 279	18NOV2:553SC1S	46.95	5.53
379GLBR- 281	18NOV3:503SC1S	54.90	5.29
379GLBR- 283	18NOV4:403SC1S	54.53	5.35
379GLBR- 296	19NOV8:554SC1S	99.84	4.35
379GLBR- 297	19NOV8:564SC1S	99.82	4.38
379GLBR- 298	19NOV8:574SC1S	99.88	4.11
379GLBR- 306	19NOV9:228SC1S	98.37	4.22
379GLBR- 309	19NOV9:337SC1S	82.98	4.88
379GLBR- 310	19NOV11:303SC2S	49.86	4.87
379GLBR- 312	19NOV2:203SC2S	50.34	5.27
379GLBR- 314	19NOV3:553SC2S	52.26	5.56
379GLBR- 317	19NOV4:314SC2S	99.96	4.23
379GLBR- 318	19NOV4:314SC2S	99.96	3.62
379GLBR- 319 Rep	1 19NOV4:314SC2S	100.00	2.90
379GLBR- 319 Rep 2	2 19NOV4:314SC2S	99.98	4.04
379GLBR- 319 Rep (	3 19NOV4:314SC2S	99.99	3.95
379GLBR- 338	20NOV8:157SC2S	95.31	4.87
379GLBR- 339	20NOV11:443SC3S	50.16	5.01
379GLBR- 341	20NOV1:003SC3S	47.26	5.04
379GLBR- 343	20NOV1:553SC3S	47.50	4.83
379GLBR- 347	20NOV3:124SC3S	94.60	3.78
379GLBR- 348	20NOV3:124SC3S	95.77	3.76
379GLBR- 349	20NOV3:124SC3S	95.35	4.77
379GLBR- 355	20NOV3:317SC3S	85.08	5.24
379GLBR- 358	20NOV3:258SC3S	99.57	4.75

		Total Solids	Total Volatile
MSL Code	Sponsor ID	(% Dry Wt.)	Solids (%Dry Wt.)
	DIN D		
	BIN D.		
379GLBR- 34	07OCT2:091SDS	54.45	5.64
379GLBR- 35	07OCT1:521SDS	57.43	5.53
379GLBR- 43	07OCT2:051SDS	58.76	5.21
379GLBR- 48	08OCT5:312SD2S	58.01	5.68
379GLBR- 50	08OCT5:412SD1S	59.33	5.36
379GLBR- 52 Rep 1	080CT5:172SD3S	57.44	5.98
379GLBR- 52 Rep 2	2 08OCT5:172SD3S	58.06	6.38
379GLBR- 52 Rep 3	08OCT5:172SD3S	58.14	5.92
379GLBR- 375	21NOV12:003SD1S	40.67	4.09
379GLBR- 377	21NOV1:353SD1S	47.67	5.29
379GLBR- 379	21NOV2:433SD1S	45.34	5.37
379GLBR- 382 Rep 1		99.56	4.48
379GLBR- 382 Rep 2	21NOV4:558SD1S	99.55	4.29
379GLBR- 382 Rep 3		99.57	4.63
379GLBR- 387	21NOV5:087SD1S	94.22	5.11
379GLBR- 392	21NOV5:214SD1S	99.87	3.81
379GLBR- 393	21NOV5:214SD1S	99.89	3.48
379GLBR- 394	21NOV5:214SD1S	99.87	2.79
BLANK RESULTS		Total Solids To	otal Volatile Solids
			ions in grams)
<b>.</b>			
Blank 1		0.0005	0.0009
Blank 2		0.0013	0.0017
Blank 3		0.0001	0.0012
Blank 4		0.0005	0.0008
Blank 5		0.0006	0.0012
Blank 6		0.0005	0.0001
Blank 7		0.0001	0.0005
Blank 8		0.0010	0.0023
Blank 9		0.0014	0.0008
Blank 10		0.0011	0.0025

NOTE: Results are not blank-corrected.

NA = Not applicable/analyzed.

MSL Code	Sponsor ID	Total Solids	Total Volatile
oc occo	Sportson 1B	(% Dry Wt.)	Solids (%Dry Wt.)
	•		
REPLICATE ANA	LYSIS		
	<b>;</b>		
379GLBR- 140 R	ep 1 240CT2:203SA3S	53.65	5.83
	ep 2 24OCT2:203SA3S	53.94	5.96
	ep 3 24OCT2:203SA3S	55.22	<b>6.</b> 08
	RSD 9		2%
379GLBR- 216 R	ep 1 310CT9:204SB2S	99.84	2.17
379GLBR- 216 R	ep 2 31OCT9:204SB2S	99.84	2.81
379GLBR- 216 R	ep 3 310CT9:204SB2S	99.84	2.91
	RSD 9		15%
	ep 1 19NOV4:314SC2S	100.00	2.9
	ep 2 19NOV4:314SC2S	99.98	4.04
379GLBR- 319 R	ep 3 19NOV4:314SC2S	99.99	3.95
	RSD 9	<b>6</b> 0%	17%
	ep 1 08OCT5:172SD3S	57.44	5.98
	ep 2 08OCT5:172SD3S	58.06	6.38
379GLBR- 52 R	ep 3 08OCT5:172SD3S	58.14	5.92
	RSD %	6 1%	4%
379GLBR- 382 R	ep 1 21NOV4:558SD1S	99.56	4.48
	ep 2 21NOV4:558SD1S	99.55	4.29
379GLBR- 382 R	ep 3 21NOV4:558SD1S	99.57	4.63
	RSD %	6 0%	4%

RSD % = Relative Standard Deviation.

		Total Solids	Total Suspended
MSL Code	Sponsor ID	(mg/L)	Solids (mg/L)
	BIN A		
379GLBR- 95	210CT:6.2410LA1S	4214 *	318
379GLBR- 100	210CT6:459LA1S	7690 *	244
379GLBR- 126	230CT4:459LA2S	10486 *	344
79GLBR- 130 Rep	1 23OCT5:2010LA2S	7824 *	4947
79GLBR- 130 Rep	2 23OCT5:2010LA2S	8196 *	4810
•	3 23OCT5:2010LA2S	8054 *	5113
379GLBR- 158	250CT10:2210LA3S	12386 *	11080 *
379GLBR- 159	250CT10:2110LA3S	3564 *	2512 *
379GLBR- 202	300CT4:166LA3S	184 *	23 *
	BIN B		
79GLBR- 197 Rep	1 25OCT3:1110LB1S	7626 *	7368 *
179GLBR- 197 Rep	2 25OCT3:1110LB1S	7910 *	7040 *
79GLBR- 197 Rep	3 25OCT3:1110LB1S	7674 *	7384 *
79GLBR- 224	310CT10:059LB2S	6768	216
79GLBR- 230	310CT10:1910LB2S	2016	616
79GLBR- 258	310CT2:5410LB3S	990	950
79GLBR- 259	310CT2:5610LB3S	1156	972
79GLBR- 260	31OCT3:049LB3S	6482	528
79GLBR- 261	31OCT3:059LB3S	6810	776
	BIN C		
79GLBR- 289 Rep	1 18NOV5:409LC1S	11410 *	4748 *
79GLBR- 289 Rep	2 18NOV5:409LC1S	8324 *	5376 *
79GLBR- 289 Rep		8164 *	3878 *
79GLBR- 291	18NOV6:1010LC1S	2172 *	1273 *
79GLBR- 329	19NOV5:539LC2S	4918 *	3184 *
79GLBR- 332	19NOV5:2410LC2S	1248 *	863 *
79GLBR- 364	20NOV2:163LC3S	386 *	<1 *
79GLBR- 367	20NOV2:409LC3S	9420 *	8760 *
79GLBR- 373	20NOV3:0010LC3S	996 *	638 *

MSL Code	Sponsor ID	Total Solids (mg/L)	Total Suspended Solids (mg/L)
MOL 0000	-	(mg/L)	Oolios (Hig/E)
	BIN D		
379GLBR- 401	21NOV3:3510LD1S	1848	1156
379GLBR- 403 Rep 1		3908	2736
379GLBR- 403 Rep 2		3954	2614
379GLBR- 403 Rep 3		3970	2634
3/3GEBN- 403 Nep 3	2111014.0392013	3970	2034
	DILUTION WATER		
27001 00 076	6NOV49-0001-5	400	•
379GLBR- 276	6NOV12:003LS	166	8
REPLICATE ANALYSE	<b>:</b> S		
379GLBR- 130 Rep 1	23OCT5:2010LA2S	7824 <b>*</b>	5143
379GLBR- 130 Rep 2		8196 *	5007
379GLBR- 130 Rep 3		8054 *	5310
•	RSD %	2%	3%
379GLBR- 197 Rep 1	25OCT3:1110LB1S	7626 *	7256 °
379GLBR- 197 Rep 2		7910 *	6928 *
379GLBR- 197 Rep 3		7674 °	7272 *
	RSD %	2%	3%
379GLBR- 289 Rep 1		11410 *	2580 *
379GLBR- 289 Rep 2		8324 *	2818 *
379GLBR- 289 Rep 3		8164 *	2282 *
	RSD %	20%	10%
379GLBR- 403 Rep 1	21NOV4:039LD1S	3908	2700
379GLBR- 403 Rep 2		3954	2578
379GLBR- 403 Rep 3		3970	2598
· · • • •	RSD %	1%	2%
MOTE. All secules on	a blank assessed		

NOTE: All results are blank-corrected. RSD% = Relative Standard Deviation.

<sup>\* =</sup> Reruns outside holding times.

MSL CODE MDL		SPONSOR ID	TOC % Dry Weight 300 ug/g
		BIN A	
379GLBR- 39		07OCT12:411SAS	1.91
379GLBR- 44		07OCT12:321SAS	1.77
379GLBR- 45		07OCT12:121SAS	1.91
379GLBR- 54		09OCT11:282SA1S	1.86
379GLBR- 55		09OCT11:382SA2S	1.84
379GLBR- 56		09OCT11:502SA3S	1.90
379GLBR- 98		220CT11:307SA1S	2.73
379GLBR- 105		220CT11:368SA1S	1.86
379GLBR- 109		220CT4:203SA2S	1.87
379GLBR- 110		220CT5:553SA2S	1.86
379GLBR- 114		230CT1:303SA2S	1.89
379GLBR- 116		230CT4:254SA2S	1.25
379GLBR- 117		230CT4:264SA2S	1.18
379GLBR- 118		230CT4:274SA2S	1.21
379GLBR- 134		240CT10:457SA2S	1.48
379GLBR- 137		240CT10:508SA2S	1.04
379GLBR- 140	Rep 1	240CT2:203SA3S	1.86
379GLBR- 140	Rep 2	240CT2:203SA3S	1.99
379GLBR- 140	Rep 3	240CT2:203SA3S	1.85
379GLBR- 142		24AOCT5:503SA3S	1.90
379GLBR- 144		240CT6:203SA3S	1.82
379GLBR- 147		250CT9:234SA3S	1.40
379GLBR- 148		25OCT9:244SA3S	1.47
379GLBR- 149		250CT9:254SA3S	1.54
379GLBR- 157		25OCT9:307SA3S	1.72
379GLBR- 169		25OCT9:358SA3S	1.47

		TCC
MSL CODE	SPONSOR ID	% Dry Weight
MDL		300 ug/g

	;	BIN B		
	,			
379GLBR- 36		07OCT1:111SBS		1.93
379GLBR- 41		07OCT1:021SBS		1.67
379GLBR- 42		07OCT12:501SBS		1.91
379GLBR- 62		09OCT9:552SB1S		1.82
379GLBR- 63		09OCT10:152SB2S		1.87
379GLBR- 64		09OCT10:352SB3S		1.94
379GLBR- 172		300CT2:573SB2S		2.14
379GLBR- 173		25OCT12:153SB1S		1.94
379GLBR- 175		250CT2:153SB1S		1.84
379GLBR- 178		25OCT2:304SB1S		1.49
379GLBR- 179		250CT2:314SB1S		1.40
379GLBR- 180		25OCT2:324SB1S		1.37
379GLBR- 191		250CT3:517SB1S		1.71
379GLBR- 194		25OCT3:568SB1S		1.69
379GLBR- 200		30OCT4:053SB2S		1.81
379GLBR- 205		30OCT4:393SB2S		1.79
379GLBR- 209		310CT9:017SB2S		1.59
379GLBR- 212	_	31OCT9:068SB2S		1.53
379GLBR- 216	Rep 1	31OCT9:204SB2S		0.99
379GLBR- 216	Rep 2	31OCT9:204SB2S	•	1.02
379GLBR- 216	Rep 3	31OCT9:204SB2S		1.13
379GLBR- 217		31OCT9:234SB2S		1.02
379GLBR- 218		31OCT9:224SB2S		1.01
379GLBR- 235		310CT2:364SB3S		1.52
379GLBR- 236		31OCT11:503SB3S		1.80
379GLBR- 237		31OCT10:453SB3S		2.01
379GLBR- 238		31OCT2:303SB3S		1.78
379GLBR- 239		310CT2:374SB3S		1.39
379GLBR- 240		310CT2:374SB3S		1.39
379GLBR- 264		1NOV10:208SB3S		1.46
379GLBR- 266		1NOV10:157SB3S		1.42

		TCC
MSLCODE	SPONSOR ID	% Dry Weight
MDL		300 ug/g

	:	BIN C	]	
	_			
379GLBR- 37		07OCT1:201SCS		1.80
379GLBR- 38		07OCT1:431SCS		1.62
379GLBR- 40	_	07OCT1:331SCS		1.89
379GLBR- 70		09OCT4:362SC2S		1.77
379GLBR- 71		09OCT4:552SC1S		1.80
379GLBR- 72		09OCT4:152SC3S		1.84
379GLBR- 279		18NOV2:553SC1S		1.84
379GLBR- 281		18NOV3:503SC1S		1.82
379GLBR- 283	_	18NOV4:403SC1S		1.83
379GLBR- 296		19NOV8:554SC1S		1.49
379GLBR- 297		19NOV8:564SC1S		1.47
379GLBR- 298		19NOV8:574SC1S		1.61
379GLBR- 306		19NOV9:228SC1S	and the second	1.46
379GLBR- 309		19NOV9:337SC1S		2.06
379GLBR- 310		19NOV11:303SC2S		1.78
379GLBR- 312		19NOV2:203SC2S		1.85
379GLBR- 314		19NOV3:553SC2S		1.78
379GLBR- 317		19NOV4:314SC2S		1.49
379GLBR- 318		19NOV4:314SC2S		1.57
379GLBR- 319	•	19NOV4:314SC2S		1.49
379GLBR- 319	Rep 2	19NOV4:314SC2S		1.59
379GLBR- 319	•	19NOV4:314SC2S		1.56
379GLBR- 338		20NOV8:157SC2S		1.66
379GLBR- 339		20NOV11:443SC3S		1.76
379GLBR- 341		20NOV1:003SC3S		1.76
379GLBR- 343	}	20NOV1:553SC3S		1.73
379GLBR- 347		20NOV3:124SC3S		1.67
379GLBR- 348		20NOV3:124SC3S		1.61
379GLBR- 349		20NOV3:124SC3S		1.70
379GLBR- 355		20NOV3:317SC3S		2.05
379GLBR- 358		20NOV3:258SC3S		1.59

		TCC
MSL CODE	SPONSOR ID	% Dry Weight
MDL		300 ug/g

		; ;	BIN D	
379GLBR	. 34		07OCT2:091SDS	1.78
379GLBR-	. 35		07OCT1:521SDS	1.76
379GLBR	43		07OCT2:051SDS	1.74
379GLBR-	48		08OCT5:312SD2S	2.55
379GLBR	- 50		08OCT5:412SD1S	1.82
379GLBR-	52	Rep 1	08OCT5:172SD3S	1.91
379GLBR-	52	Rep 2	08OCT5:172SD3S	1.98
379GLBR-	52	Rep 3	08OCT5:172SD3S	1.91
379GLBR-	375	•	21NOV12:003SD1S	1.85
379GLBR-	377		21NOV1:353SD1S	1.84
379GLBR-	379		21NOV2:433SD1S	1.85
379GLBR-	382	Rep 1	21NOV4:558SD1S	1.53
379GLBR-	382	Rep 2	21NOV4:558SD1S	1.53
379GLBR-	382	Rep 3	21NOV4:558SD1S	1.53
379GLBR-	387		21NOV5:087SD1S	1.84
379GLBR-	392		21NOV5:214SD1S	\$ 1.35
379GLBR-	393		21NOV5:214SD1S	1.26
379GLBR-	394		21NOV5:214SD1S	1.36
BLANK	Rep 1			0.006
BLANK	Rep 2			0.005
BLANK	Rep 3			0.005
BLANK	Rep 4			0.005
BLANK	Rep 5	;		0.003
BLANK	Rep 6			0.005
BLANK	Rep 7	•		0.003
BLANK	Rep 8			0.004
BLANK	Rep 9	•		0.005
BLANK	Rep 1	0		0.003

MSL CODE			SPONSOR ID		TOC % Dry Weight
MOL	,			- · · · · · · · · · · · · · · · · · · ·	300 ug/g
			•		
STANDARD	REF	ERENC	E MATERIAL		
MESS-1	Rep	1			2.42
	Rep :				2.41
	Rep :				2.37
	Rep				2.39
MESS-1	Rep :	5			2.25
	CE	ertified			2.25
		value			±0.2
REPLICATI	E AN	IALYSE	<b>S</b>		
07001.00		D 4	0.40070.000400		
379GLBR-		Rep 1	24OCT2:203SA3S		1.86
379GLBR-		Rep 2	24OCT2:203SA3S		1.99
379GLBR-	140	Rep 3	24OCT2:203SA3S	DCD 0/	1.85
379GLBR- :	016	Don 1	31OCT9:204SB2S	RSD %	4%
379GLBR- 2		•			0.99 1.02
379GLBR- 2			310CT9:204SB2S		1.13
373GLBR- 7	210	ueh 3	310013.2043623	RSD %	7%
379GLBR- :	319	Ren 1	19NOV4:314SC2S	NOD /6	1.49
379GLBR- (		•	19NOV4:314SC2S		1.59
379GLBR- 3		•	19NOV4:314SC2S		1.56
O, OGEDIT (	3.3	TICP 0	1011014.0140020	RSD %	3%
379GLBR-	52	Rep 1	08OCT5:172SD3S	11.00 /0	1.91
379GLBR-	52	Rep 2	08OCT5:172SD3S		1.98
379GLBR-	52	•	08OCT5:172SD3S		1.91
				RSD %	2%
379GLBR- 3	382	Rep 1	21NOV4:558SD1S		1.53
379GLBR- 3		•	21NOV4:558SD1S		1.53
379GLBR- 3	382	Rep 3	21NOV4:558SD1S		1.53
•				RSD %	0%

NOTE: Results are blank-corrected. RSD % = Relative Standard Deviation.

MSL CODE	SPONSOR ID	TCC (ug/L) 1000 ug/L
	BIN A	
379GLBR- 125	230CT4:459LA2C	<b>23</b> 92600
379GLBR- 129	23OCT5:2010LA2C	853490
379GLBR- 162	25OCT10:2110LA3C	509150
379GLBR- 165	25OCT10:009LA3C	716190
379GLBR- 201	300CT4:206LA3C	530
	BIN B	
379GLBR- 190	250CT3:1110LB1C	531430
379GLBR- 225	31OCT10:109LB2C	854650
379GLBR- 231	310CT10:2410LB2C	747090
379GLBR- 262	31OCT2:5810LB3C	437250
379GLBR- 263	31OCT3:099LB3C	909520
379GLBR- 271	1NOV11:006LB2C	350
379GLBR- 273	1NOV2:506LB1B3C	400
	BIN C	
379GLBR- 294	18NOV6:0610LC1C	275150
379GLBR- 295	18NOV5:459LC1C	829720
379GLBR- 330	19NOV5:579LC2C	715150
379GLBR- 335	19NOV5:4310LC2C	251420
379GLBR- 365	20NOV2:183LC3C	7120
379GLBR- 369	20NOV2:449LC3C	428120
379GLBR- 374	20NOV3:0210LC3C	167150
	BIN D	
379GLBR- 402	21NOV3:3710LD1C	373020
379GLBR- 406	21NOV4:459LD1C	695120
	DILUTION WATER	
379GLBR- 278	6NOV12:003LC	1370
BLANK Rep 1		< 990
BLANK Rep 2		< 810
BLANK Rep 3		< 360

MSL CODE	SPONSOR ID		T <b>○</b> C (ug/L) 1000 ug/L
REPLICATE ANALYSE	:S		
379GLBR- 263 Rep 1	31OCT3:099LB3C		902000
379GLBR- 263 Rep 2	31OCT3:099LB3C		935000
379GLBR- 263 Rep 3	31OCT3:099LB3C		905000
•		RSD %	2%
379GLBR- 295 Rep 1	18NOV5:459LC1C		829720
379GLBR- 295 Rep 2	18NOV5:459LC1C		850280
379GLBR- 295 Rep 3	18NOV5:459LC1C		856480
•		RSD %	2%
379GLBR- 335 Rep 1	19NOV5:4310LC2C		251420
379GLBR- 335 Rep 2	19NOV5:4310LC2C		240650
379GLBR- 335 Rep 3	19NOV5:4310LC2C		238680
		RSD %	3%
379GLBR- 278 Rep 1	6NOV12:003LC		1370
379GLBR- 278 Rep 2	6NOV12:003LC		1390
379GLBR- 278 Rep 3	6NOV12:003LC		1390
•		RSD %	1%

NOTE: Results are blank-corrected. RSD % = Relative Standard Deviation.

#### REPORT OF CHEMICAL ANALYSES

Volume 2: Leach Test

PROJECT: Buffalo River Pilot Project

#### Prepared for:

USEPA Great Lakes National Program Office Attn: Dr. Steve Garbaciak 230 S. Dearborn Chicago, IL 60604 REPORT OF: CHEMICAL ANALYSES

PROJECT: BUFFALO RIVER PILOT PROJECT

DATE: April 23, 1992

CF#: 379GLBR

ISSUED TO: Dr. Steve Garbaciak

Technical Project Manager

USEPA Great Lakes National Program Office

230 S. Dearborn Chicago, IL 60604

#### INTRODUCTION

This report summarizes the results from analyses performed on pilot study samples which were submitted by the U.S. Army Corps of Engineers Great Lakes Division, Buffalo District.

#### SAMPLE CUSTODY

Samples were received in good condition from October 7, 1991 through December 5, 1991. Samples were logged in and stored as specified in the narrative. Samples were analyzed within the holding times specified in the QA plan. Any exceptions are noted in the narrative associated with each analysis.

#### LEACH TEST AND TCLP EXTRACTIONS

Twenty-one samples were leached following the sequential batch leach test (SBLT) and the toxicity characteristic leaching procedure (TCLP) provided by the Army Corps of Engineers-Buffalo District. All leach test samples were stored at 40±20C prior to leaching. The SBLT produced four extracts for each sample which were subsampled for each parameter, then analyzed separately for metals, specific conductivity, TOC and pH. Metal and TOC aliquots were acidified upon collection to a pH ≤2 with nitric acid and phosphoric acid, respectively. Specific conductivity aliquots were stored at 492°C until analysis. pH was determined immediately and the aliquots were archived at 40±20C. The TCLP produces one extract for each sample which was then analyzed for metals and pH. The metals aliquot was acidified to a pH ≤2 upon collection. pH was determined immediately and the aliquot archived at 49±2°C. Twelve samples were archived for possible analysis in the future. Samples for TOC were sent to Analytical Resources, Inc. for analysis by EPA method 415.1 and measured on a Dohrman DC-180 Organic Carbon Analyzer. Specific conductance and pH were determined potentiometrically, following Standard Methods 2510 B and EPA method 150.1, respectively. Cadmium, chromium and lead were analyzed by stabilized temperature graphite furnace, following Battelle SOP# MSL-M-32. Mercury was analyzed by cold vapor atomic fluorescence, following Battelle SOP# MSL-M-27.

Sponsor ID	Sample Type	<u>Analyses</u>	Battelle ID
07OCT12:381SAL	Sediment	Leach Test	379GLBR*5
07OCT12:571SBL	Sediment	Leach Test	379GLBR*7
07OCT12:301SAL	Sediment	Leach Test	379GLBR*8
07OCT1:071SBL	Sediment	Leach Test	379GLBR*10
230CT4:354SA2M	Sediment	Leach Test	379GLBR*121

250CT9:104SA3M	Sediment	Leach Test	379GLBR*154
250CT2:514SB1M	Sediment	Leach Test	379GLBR*185
31OCT9:304SB2M	Sediment	Leach Test	379GLBR*214
310CT2:404SB3M	Sediment	Leach Test	379GLBR*250
4DEC11:455SA2M	Sediment	Leach Test	379GLBR*460
4DEC11:555SA2M	Sediment	Leach Test	379GLBR*461
4DEC12:055SA2M	Sediment	Leach Test	379GLBR*462
4DEC11:155SA3M	Sediment	Leach Test	379GLBR*463
4DEC11:305SA3M	Sediment	Leach Test	379GLBR*464*
4DEC11:375SA3M	Sediment	Leach Test	379GLBR*465*
4DEC12:505SB2M	Sediment	Leach Test	379GLBR*466
4DEC1:005SB2M	Sediment	Leach Test	379GLBR*467*
4DEC1:155SB2M	Sediment	Leach Test	379GLBR*468*
4DEC1:255SB1/B3M	Sediment	Leach Test	379GLBR*469
4DEC1:305SB1/B3M	Sediment	Leach Test	379GLBR*470*
4DEC1:355SB1/B3M	Sediment	Leach Test	379GLBR*471*

\*The second, third and fourth extracts of these leach test were not analyzed, but archived for possible future analysis as directed by the Army Corps of Engineers-Buffalo District.

#### ARCHIVED SAMPLES

Sponsor ID	Sample Type	Analyses	Battelle ID
07OCT1:451SCL	Sediment	Leach Test	379GLBR*1
07OCT1:501SDL	Sediment	Leach Test	379GLBR*2
07OCT2:061SDL	Sediment	Leach Test	379GLBR*3
07OCT2:151SDL	Sediment	Leach Test	379GLBR*4
07OCT1:401SCL	Sediment	Leach Test	379GLBR*6
07OCT1:141SBL	Sediment	Leach Test	379GLBR*9
07OCT1:261SCL	Sediment	Leach Test	379GLBR*11
07OCT12:451SAL	Sediment	Leach Test	379GLBR*12
210CT5:504SA1L	Sediment	Leach Test	379GLBR*87
19NOV8:504SC1M	Sediment	Leach Test	379GLBR*301
19NOV4:374SC2M	Sediment	Leach Test	379GLBR*322
20NOV3:204SC3M	Sediment	Leach Test	379GLBR*354

#### Metals

The SBLT samples could not be spiked for metals prior to extraction as at a pH >2, metals tend to remain in the sediment. Therefore, any matrix spike added would adsorb onto the sediment and recoveries would be meaningless. Although two TCLP samples (379GLBR\*5 and 465) were spiked with 40  $\mu$ g of Pb, 20  $\mu$ g of Cu and 20  $\mu$ g of Cr prior to extraction, the pH in the extraction fluid was ~ 5, consequently, the metal spikes were not recovered. The analyst performed spike additions at the time of analysis for both the SBLT and TCLP samples. Since spike additions are not true matrix spikes, that data is not presented on the final summary tables but is available in the raw data. Replicate analyses were quite variable for the metals analysis of both TCLP and SBLT extracts, which may be due in part to nonhomogeneous samples and partly to values near the method detection limits. Variability increased for the treated sediment (ash) samples and may be a result of matrix interference. Certified reference material values were always within the ARCS criteria of  $\pm$  20%.

Replicates of the leaching procedure for TOC produced variable results, of which some were outside the ARCS criteria. Replicates performed at the time of analysis produced RSD values within the ARCS criteria, indicating the variability comes from the leach procedure itself, rather than the TOC methodology. Generally, the first fraction results were consistent with an RSD ~ 15%, suggesting the variability in extraction efficiency lies in the following days of the method. Variability increased for the treated sediment (ash) samples and may be a result of matrix interference.

MSL Code	•	Sponsor ID	рН
		BIN A	
379GLBR- 5 Rep 1 Fraction	on 1	07OCT12:381SAL	7.74
Fraction	on 2	070CT12:381SAL	7.83
Fraction	on 3	07OCT12:381SAL	7.93
Fraction	on 4	070CT12:381SAL	7.99
379GLBR- 5 Rep 2 Fraction	n 1	07OCT12:381SAL	7.75
Fraction	n 2	07OCT12:381SAL	7.93
Fraction	n 3	07OCT12:381SAL	<b>8</b> .06
Fraction	n 4	07OCT12:381SAL	7.97
379GLBR- 5 Rep 3 Fraction	n 1	07OCT12:381SAL	7.63
Fraction	n 2	07OCT12:381SAL	7.93
Fraction	n 3	070CT12:381SAL	8.05
Fraction	n 4	070CT12:381SAL	8.01
379GLBR- 8 Fraction	n 1	070CT12:301SAL	6.80
Fractio	n 2	07OCT12:301SAL	7.20
Fractio	n 3	07OCT12:301SAL	7.56
Fractio	n 4	07OCT12:301SAL	7.89
379GLBR-121 Rep 1 Fractio	n 1	230CT4:354SA2M	7.66
Fractio	n 2	230CT4:354SA2M	7.63
Fractio	n 3	230CT4:354SA2M	7.82
Fractio		230CT4:354SA2M	7.80
379GLBR-121 Rep 2 Fractio	n 1	23OCT4:354SA2M	7.57
Fractio	n 2	23OCT4:354SA2M	7.87
Fractio	n 3	230CT4:354SA2M	7.68
Fractio		230CT4:354SA2M	7.80
379GLBR-121 Rep 3 Fraction	n 1 🐇	230CT4:354SA2M	7.69
Fraction	n 2	230CT4:354SA2M	7.84
Fraction	า 3	230CT4:354SA2M	7.77
Fraction	1 4	230CT4:354SA2M	7.83
379GLBR- 154 Fraction	•	25OCT9:104SA3M	7.38
Fraction		25OCT9:104SA3M	7.51
Fraction	_	25OCT9:104SA3M	7.82
Fraction	1 4	25OCT9:104SA3M	8.04

MSL Code		Sponsor ID	рН
379GLBR- 460	Fraction 1	4DEC11:455SA2M	12.05
	Fraction 2	4DEC11:455SA2M	12.38
· · · · · · · · · · · · · · · · · · ·	Fraction 3	4DEC11:455SA2M	12.27
	Fraction 4	4DEC11:455SA2M	11.80
379GLBR- 461	Fraction 1	4DEC11:555SA2M	12.01
	Fraction 2	4DEC11:555SA2M	12.42
	Fraction 3	4DEC11:555SA2M	12.32
	Fraction 4	4DEC11:555SA2M	11.95
379GLBR- 462	Fraction 1	4DEC12:055SA2M	12.08
	Fraction 2	4DEC12:055SA2M	12.40
	Fraction 3	4DEC12:055SA2M	12.31
	Fraction 4	4DEC12:055SA2M	11.98
379GLBR- 463	Fraction 1	4DEC11:155SA3M	12.45
	Fraction 2	4DEC11:155SA3M	12.50
	Fraction 3	4DEC11:155SA3M	11.02
	Fraction 4	4DEC11:155SA3M	11.03
379GLBR- 464	Fraction 1	4DEC11:305SA3M	12.28
379GLBR- 465	Fraction 1	4DEC11:375SA3M	12.26
		BIN B	
379GLBR- 7	Fraction 1	07OCT12:571SBL	7.47
	Fraction 2	07OCT12:571SBL	7.79
	Fraction 3	07OCT12:571SBL	7.80
	Fraction 4	07OCT12:571SBL	7.68
379GLBR- 10	Fraction 1	07OCT1:071SBL	7.92
	Fraction 2	07OCT1:071SBL	7.84
	Fraction 3	07OCT1:071SBL	7.78
	Fraction 4	07OCT1:071SBL	7.79
379GLBR- 214	Fraction 1	31OCT9:304SB2M	7.34
	Fraction 2	31OCT9:304SB2M	7.73
	Fraction 3	31OCT9:304SB2M	7.96
	Fraction 4	31OCT9:304SB2M	8.06
379GLBR- 250	Fraction 1	31OCT2:404SB3M	7.32
	Fraction 2	310CT2:404SB3M	7.53
	Fraction 3	310CT2:404SB3M	7.72
	Fraction 4	31OCT2:404SB3M	7.82

MSL Code		Sponsor ID	рН
379GLBR-466	Fraction 1	4DEC12:505SB2M	12.19
	Fraction 2	4DEC12:505SB2M	12.48
•	Fraction 3	4DEC12:505SB2M	12.44
	Fraction 4	4DEC12:505SB2M	12.27
379GLBR- 467	Fraction 1	4DEC1:005SB2M	12.32
379GLBR- 468	Fraction 1	4DEC1:155SB2M	12.30
379GLBR- 469	Fraction 1	4DEC1:255SB1/B3M	11.93
	Fraction 2	4DEC1:255SB1/B3M	12.20
	Fraction 3	4DEC1:255SB1/B3M	12.08
	Fraction 4	4DEC1:255SB1/B3M	11.98
379GLBR- 470	Fraction 1	4DEC1:305SB1/B3M	12.42
379GLBR- 471	Fraction 1	4DEC1:355SB1/B3M	12.43
BLANK-1	Fraction 1		5.60
BLANK-1	Fraction 2		5.75
BLANK-1	Fraction 3		5.63
BLANK-1	Fraction 4		6.00
BLANK-2	Fraction 1		6.85
BLANK-2	Fraction 2		6.25
BLANK-2	Fraction 3		5.04
BLANK-2	Fraction 4		5.18
BLANK-3	Fraction 1		5.32
BLANK-3	Fraction 2		4.89
BLANK-3	Fraction 3		5.07
BLANK-3	Fraction 4		5.57

MSL Code		Sponsor ID	рН
REPLICATE	ANALYSIS	en e	
379GLBR-	5 Rep 1 Fraction 1	07OCT12:381S/.L	7.74
379GLBR-	5 Rep 2 Fraction 1	07OCT12:381SAL	7.75
379GLBR-	5 Rep 3 Fraction 1	07OCT12:381SAL	7.63
		RSD %	1%
379GLBR-	5 Rep 1 Fraction 2	07OCT12:381SAL	7.83
379GLBR-	5 Rep 2 Fraction 2	07OCT12:381SAL	7.93
379GLBR-	5 Rep 3 Fraction 2	07OCT12:381SAL	7.93
		RSD %	1%
379GLBR-	5 Rep 1 Fraction 3	07OCT12:381SAL	7.93
379GLBR-	5 Rep 2 Fraction 3	07OCT12:381SAL	8.06
379GLBR-	5 Rep 3 Fraction 3	07OCT12:381SAL	8.05
		RSD %	1%
379GLBR-	5 Rep 1 Fraction 4	07OCT12:381SAL	7.99
379GLBR-	5 Rep 2 Fraction 4	07OCT12:381SAL	7.97
379GLBR-	5 Rep 3 Fraction 4	07OCT12:381SAL	8.01
		RSD %	0%
379GLBR- 1	21 Rep 1 Fraction 1	23OCT4:354SA2M	7.66
379GLBR- 1	21 Rep 2 Fraction 1	23OCT4:354SA2M	7.57
379GLBR- 1	21 Rep 3 Fraction 1	23OCT4:354SA2M	7.69
		RSD %	1%
379GLBR- 1	21 Rep 1 Fraction 2	23OCT4:354SA2M	7.63
379GLBR- 1	21 Rep 2 Fraction 2	23OCT4:354SA2M	7.87
379GLBR- 1	21 Rep 3 Fraction 2	23OCT4:354SA2M	7.84
		RSD %	2%

RSD % = Relative Standard Deviation.

MSL Code	eta e a como e	Sponsor ID	рН
REPLICATE ANALYSIS	<b>}</b>		
379GLBR-121 Rep 1 I	Fraction 3	23OCT4:354SA2M	7.82
379GLBR-121 Rep 2 i		230CT4:354SA2M	7.68
379GLBR- 121 Rep 3 F	Fraction 3	23OCT4:354SA2M	7.77
		RSD %	1%
379GLBR-121 Rep 1 F	Fraction 4	230CT4:354SA2M	7.80
379GLBR-121 Rep 2 F	raction 4	23OCT4:354SA2M	7.80
379GLBR-121 Rep 3 F	Fraction 4	23OCT4:354SA2M	7.83
		RSD %	0%

RSD % = Relative Standard Deviation.

MSL Code -	Sponsor ID	На
	BIN A	
379G'_BR- 5 Rep 1	070CT12:381SAL	5.53
379GLBR- 5 Rep 2	07OCT12:381SAL	5.54
379GLBR- 5 Rep 3	07OCT12:381SAL	5.56
379GLBR- 8	070CT12:301SAL	5.55
379GLBR- 121 Rep 1	230CT4:354SA2M	6.24
379GLBR- 121 Rep 2	230CT4:354SA2M	6.22
379GLBR- 121 Rep 3	230CT4:354SA2M	6.17
379GLBR- 154	25OCT9:104SA3M	6.10
379GLBR- 460	4DEC11:455SA2M	11.71
379GLBR- 461	4DEC11:555SA2M	11.84
379GLBR- 462	4DEC12:055SA2M	9.28
379GLBR- 463	4DEC11:155SA3M	11.64
379GLBR- 464	4DEC11:305SA3M	11.71
379GLBR- 465	4DEC11:375SA3M	11.67
	BIN B	
379GLBR- 7	07OCT12:571SBL	5.53
379GLBR- 10	07OCT1:071SBL	5.58
379GLBR- 214	31OCT9:304SB2M	6.23
379GLBR- 250	310CT2:404SB3M	6.10
379GLBR- 466	4DEC12:505SB2M	12.07
379GLBR- 467	4DEC1:005SB2M	12.05
379GLBR- 468	4DEC1:155SB2M	12.05
379GLBR- 469	4DEC1:255SB1/B3M	6.64
379GLBR- 470	4DEC1:305SB1/B3M	6.55
379GLBR- 471	4DEC1:355SB1/B3M	6.64
BLANK-1		4.92
BLANK-2		2.86

MSL Code	. Sponsor ID	рН
REPLICATE ANALYSIS		
379GLBR- 5 Rep 1	07OCT12:381SAL	5.53
379GLBR- 5 Rep 2	07OCT12:381SAL	5.54
379GLBR- 5 Rep 3	07OCT12:381SAL	5.56
	RSD %	0%
379GLBR- 121 Rep 1	230CT4:354SA2M	6.24
379GLBR- 121 Rep 2	23OCT4:354SA2M	6.22
379GLBR- 121 Rep 3	23OCT4:354SA2M	6.17
	RSD %	1%

RSD % = Relative Standard Deviation.

			Specific
			Conductance
MSL Code	Fraction No.	Sponsor ID	(umhos/cm)
		BIN A	
	<i>i</i>		
379GLBR-5, Rep 1	Fraction 1	070CT12:381SAL	440
	Fraction 2	07OCT12:381SAL	230
	Fraction 3	07OCT12:381SAL	162
	Fraction 4	07OCT12:381SAL	136
379GLBR-5, Rep 2	Fraction 1	07OCT12:381SAL	450
	Fraction 2	07OCT12:381SAL	220
	Fraction 3	07OCT12:381SAL	164
	Fraction 4	07OCT12:381SAL	136
379GLBR-5, Rep 3	Fraction 1	07OCT12:381SAL	480
	Fraction 2	07OCT12:381SAL	230
	Fraction 3	07OCT12:381SAL	171
	Fraction 4	07OCT12:381SAL	134
379GLBR-8	Fraction 1	07OCT12:301SAL	740
	Fraction 2	07OCT12:301SAL	570
	Fraction 3	07OCT12:301SAL	340
	Fraction 4	07OCT12:301SAL	240
379GLBR-121, Rep 1	Fraction 1	230CT4:354SA2M	1030
•	Fraction 2	230CT4:354SA2M	230
	Fraction 3	230CT4:354SA2M	103
	Fraction 4	230CT4:354SA2M	89
379GLBR-121, Rep 2	Fraction 1	230CT4:354SA2M	1010
	Fraction 2	230CT4:354SA2M	230
,	Fraction 3	230CT4:354SA2M	109
	Fraction 4	230CT4:354SA2M	88
379GLBR-121, Rep 3	Fraction 1	230CT4:354SA2M	980
5. 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	Fraction 2	23OCT4:354SA2M	220
	Fraction 3	230CT4:354SA2M	104
	Fraction 4	23OCT4:354SA2M	87
379GLBR-154	Fraction 1	25OCT9:104SA3M	750
	Fraction 2	25OCT9:104SA3M	310
	Fraction 3	250CT9:104SA3M	210
	Fraction 4	250CT9:104SA3M	154
379GLBR-460	Fraction 1	4DEC11:455SA2M	6960
J. J. W. B. J. 100	Fraction 2	4DEC11:455SA2M	7080
	Fraction 3	4DEC11:455SA2M	5400
	Fraction 4	4DEC11:455SA2M	4160
	TACHOH T		4.00

			Specific
NO. 0-4-	For all and Alla	0	Conductance
MSL Code	Fraction No.	Sponsor ID	(umhos/cm)
	· · · · · · · · · · · · · · · · · · ·	BIN A	
379GLBR-461	Fraction 1	4DEC11:555SA2M	7560
	Fraction 2	4DEC11:555SA2M	6960
	Fraction 3	4DEC11:555SA2M	6240
	Fraction 4	4DEC11:555SA2M	4560
379GLBR-462	Fraction 1	4DEC12:055SA2M	7480
	Fraction 2	4DEC12:055SA2M	6840
	Fraction 3	4DEC12:055SA2M	5640
	Fraction 4	4DEC12:055SA2M	3960
379GLBR-463	Fraction 1	4DEC11:155SA3M	9040
	Fraction 2	4DEC11:155SA3M	8720
	Fraction 3	4DEC11:155SA3M	8880
	Fraction 4	4DEC11:155SA3M	8160
379GLBR-464	Fraction 1	4DEC11:305SA3M	9600
379GLBR-465	Fraction 1	4DEC11:375SA3M	9680
		BIN B	
379GLBR-7	Fraction 1	07OCT1:571SBL	480
	Fraction 2	07OCT1:571SBL	230
	Fraction 3	07OCT1:571SBL	174
	Fraction 4	07OCT1:571SBL	200
379GLBR-214	Fraction 1	31OCT9:304SB2M	1100
	Fraction 2	31OCT9:304SB2M	250
	Fraction 3	31OCT9:304SB2M	116
	Fraction 4	31OCT9:304SB2M	88
379GLBR-466	Fraction 1	4DEC12:505SB2M	10160
	Fraction 2	4DEC12:505SB2M	8720
	Fraction 3	4DEC12:505SB2M	8080
	Fraction 4	4DEC12:505SB2M	8000
379GLBR-467	Fraction 1	4DEC1:005SB2M	10240
379GLBR-468	Fraction 1	4DEC1:155SB2M	11280
379GLBR-469	Fraction 1	4DEC1:2555SB1/B3M	6600
	Fraction 2	4DEC1:2555SB1/B3M	5400
	Fraction 3	4DEC1:2555SB1/B3M	3320
	Fraction 4	4DEC1:2555SB1/B3M	2740
379GLBR-470	Fraction 1	4DEC1:305SB1/B3M	6720
379GLBR-471	Fraction 1	4DEC1:355SB1/B3M	7400

						Specific Conductance
MSL Code		Fraction No.	•	Sponsor ID		(umhos/cm)
BLANK 1		Fraction 1				3
BLANK 1		Fraction 2	•			4
BLANK 1		Fraction 3			* * *	2
BLANK 1	The state of the s	Fraction 4				2
BLANK 2		Fraction 1				3
BLANK 2		Fraction 2				3
BLANK 2		Fraction 3				8
BLANK 2		Fraction 4				5
BLANK 3		Fraction 1		:		13
BLANK 3		Fraction 2				7
BLANK 3		Fraction 3				5
BLANK 3		Fraction 4				7
CTANDAT	<b>.</b>					
STANDARI	) - KC2 (u	imnos/cm)				
	.01M		Rep 1			1410
	.01M		Rep 2			1410
	.01M		Rep 3			1410
	.01M		Rep 4			1410
i de la companya de l					TRUE	
					VALUE	1413
STANDAR	) - KC1 (u	ımhos/cm)				
	.005M		Rep 1			730
	.005M		Rep 2			730
	.005M		Rep 3			730
	.005M		Rep 4		-	730
a de la composición dela composición de la composición dela composición de la composición de la composición dela composición dela composición de la composición de la composición dela composición de la composición dela composición dela composición					TRUE	747 0
REPLICATE	E ANALVEI	e	•		VALUE	717.8
HEFLICATI	- VIIVE 191	•				
379GLBR-5	, Rep 1	Fraction 1	•	07OCT12:381SAL		440
379GLBR-5	•	Fraction 1		07OCT12:381SAL		450
379GLBR-5	•	Fraction 1		07OCT12:381SAL		480
	• •	· · · · ·	RSD %			5%

	· .				Specific
					Conductance
MSL Code	Fraction No.		Sponsor ID		(umhos/cm)
REPLICATE ANALYS	is				
HEI CIONIE ANALIO					
379GLBR-5, Rep 1	Fraction 2		07OCT12:381SAL	v.	230
379GLBR-5, Rep 2	Fraction 2		07OCT12:381SAL		220
379GLBR-5, Rep 3	Fraction 2		07OCT12:381SAL		230
	, F	RSD %			3%
0700LDD E D 4			•=••=•••••		
379GLBR-5, Rep 1	Fraction 3		07OCT12:381SAL		162
379GLBR-5, Rep 2 379GLBR-5, Rep 3	Fraction 3 Fraction 3		07OCT12:381SAL		164
3/3GLBN-3, nep 3		RSD %	07OCT12:301SAL		171
	•	NGD /6			3%
379GLBR-5, Rep 1	Fraction 4		07OCT12:381SAL		136
379GLBR-5, Rep 2	Fraction 4		07OCT12:381SAL		136
379GLBR-5, Rep 3	Fraction 4		07OCT12:301SAL		134
	F	RSD %			1%
379GLBR-121, Rep 1	Fraction 1		23OCT4:354SA2M		1030
379GLBR-121, Rep 2			23OCT4:354SA2M		1010
379GLBR-121, Rep 3		30D 0/	23OCT4:354SA2M		980
	<b>.</b>	RSD %			2%
379GLBR-121, Rep 1	Fraction 2		230CT4:354SA2M		230
379GLBR-121, Rep 2			230CT4:354SA2M		230
379GLBR-121, Rep 3			230CT4:354SA2M		220
•	F	RSD %			3%
379GLBR-121, Rep 1	Fraction 3		23OCT4:354SA2M		103
379GLBR-121, Rep 2			23OCT4:354SA2M		109
379GLBR-121, Rep 3			23OCT4:354SA2M		104
	R	RSD %			3%
379GLBR-121, Rep 1	Fraction 4		230CT4:354SA2M		89
379GLBR-121, Rep 2	Fraction 4		230CT4:354SA2M		8.8
379GLBR-121, Rep 3	Fraction 4		23OCT4:354SA2M		87
••		SD %			1%

RSD % = Relative Standard Deviation.

	TOC
Sponsor ID	ug/L
	660
	Sponsor ID

		<del>-</del>	
		BIN A	
379GLBR- 5 Rep 1	Fraction 1	07OCT12:381SAL	10,620
	Fraction 2	07OCT12:381SAL	10,230
	Fraction 3	07OCT12:381SAL	7,160
	Fraction 4	070CT12:381SAL '	5,710
379GLBR- 5 Rep 2	Fraction 1	07OCT12:381SAL	10,880
	Fraction 2	07OCT12:381SAL	7,760
	Fraction 3	07OCT12:381SAL	6,310
	Fraction 4	07OCT12:381SAL	4,170
379GLBR- 5 Rep 3	Fraction 1	07OCT12:381SAL	13,370
	Fraction 2	07OCT12:381SAL	8,940
	Fraction 3	07OCT12:381SAL	10,300
	Fraction 4	07OCT12:381SAL	5,010
379GLBR- 8	Fraction 1	07OCT12:301SAL	17,350
	Fraction 2	07OCT12:301SAL	11,720
	Fraction 3	07OCT12:301SAL	12,070
	Fraction 4	07OCT12:301SAL	4,680
379GLBR- 121 Rep 1	Fraction 1	23OCT4:354SA2M	34,150
	Fraction 2	23OCT4:354SA2M	15,660
	Fraction 3	23OCT4:354SA2M	3,560
	Fraction 4	23OCT4:354SA2M	12,510
379GLBR- 121 Rep 2	Fraction 1	23OCT4:354SA2M	35,460
	Fraction 2	23OCT4:354SA2M	7,160
	Fraction 3	23OCT4:354SA2M	4,410
	Fraction 4	23OCT4:354SA2M	3,690
379GLBR- 121 Rep 3	Fraction 1	23OCT4:354SA2M	36,550
	Fraction 2	23OCT4:354SA2M	14,150
	Fraction 3	23OCT4:354SA2M	7,040
	Fraction 4	23OCT4:354SA2M	4,440
379GLBR- 154	Fraction 1	25OCT9:104SA3M	136,290
	Fraction 2	25OCT9:104SA3M	32,760
	Fraction 3	25OCT9:104SA3M	20,400
	Fraction 4	25OCT9:104SA3M	12,860

MSL Code		Sponsor ID	TOC ug/L
Method Detection L	_imit		660
		BIN A	
379GLBR- 460	Fraction 1	4DEC11:455SA2M	65,200
	Fraction 2	4DEC11:455SA2M	34,300
	Fraction 3	4DEC11:455SA2M	24,600
	Fraction 4	4DEC11:455SA2M	26,600
379GLBR- 461	Fraction 1	4DEC11:555SA2M	70,170
	Fraction 2	4DEC11:555SA2M	33,730
	Fraction 3	4DEC11:555SA2M	23,660
	Fraction 4	4DEC11:555SA2M	18,260
379GLBR- 462	Fraction 1	4DEC12:055SA2M	105,720
	Fraction 2	4DEC12:055SA2M	156,100
	Fraction 3	4DEC12:055SA2M	157,190
	Fraction 4	4DEC12:055SA2M	100,540
379GLBR- 463	Fraction 1	4DEC11:155SA3M	71,100
	Fraction 2	4DEC11:155SA3M	64,900
	Fraction 3	4DEC11:155SA3M	75,090
	Fraction 4	4DEC11:155SA3M	62,430
379GLBR- 464	Fraction 1	4DEC11:305SA3M	56,320
379GLBR- 465	Fraction 1	4DEC11:375SA3M	51,960
		BIN B	
379GLBR- 7	Fraction 1	07OCT12:571SBL	15,830
	Fraction 2	07OCT12:571SBL	4,910
	Fraction 3	07OCT12:571SBL	1,720
	Fraction 4	07OCT12:571SBL	1,740
379GLBR- 10	Fraction 1	07OCT1:071SBL	11,680
	Fraction 2	07OCT1:071SBL	7,120
	Fraction 3	07OCT1:071SBL	5,900
	Fraction 4	07OCT1:071SBL	5,450
379GLBR- 214	Fraction 1	31OCT9:304SB2M	15,400
	Fraction 2	31OCT9:304SB2M	13,800
	Fraction 3	31OCT9:304SB2M	3,960

31OCT9:304SB2M

3,360

Fraction 4

MSL Code	•	Sponsor ID	TOC ug/L
Method Detection Limit			660

Method Detection F	.111114		
		BIN B	
379GLBR- 250	Fraction 1	310CT2:404SB3M	158,670
	Fraction 2	31OCT2:404SB3M	52,600
	Fraction 3	31OCT2:404SB3M	21,510
	Fraction 4	31OCT2:404SB3M	13,410
379GLBR- 466	Fraction 1	4DEC12:505SB2M	108,010
	Fraction 2	4DEC12:505SB2M	134,310
	Fraction 3	4DEC12:505SB2M	121,990
	Fraction 4	4DEC12:505SB2M	97,850
379GLBR- 467	Fraction 1	4DEC1:005SB2M	67,120
379GLBR- 468	Fraction 1	4DEC1:155SB2M	52,820
379GLBR- 469	Fraction 1	4DEC1:255SB1/B3M	88,910
	Fraction 2	4DEC1:255SB1/B3M	38,470
	Fraction 3	4DEC1:255SB1/B3M	26,910
	Fraction 4	4DEC1:255SB1/B3M	23,370
379GLBR- 470	Fraction 1	4DEC1:305SB1/B3M	118,120
379GLBR- 471	Fraction 1	4DEC1:355SB1/B3M	91,590
BLANK-1	Fraction 1		6,680
BLANK-1	Fraction 2		950
BLANK-1	Fraction 3		1,250
BLANK-1	Fraction 4		3,890
BLANK-2	Fraction 1		5,980
BLANK-2	Fraction 2		5,010
BLANK-2	Fraction 3		2,010
BLANK-2	Fraction 4		840
BLANK-3	Fraction 1		9,460
BLANK-3	Fraction 2		1,750
BLANK-3	Fraction 3		1,310
BLANK-3	Fraction 4		1,720

		TOC
MSL Code · ·	Sponsor ID	ug/L
Method Detection Limit		660
REPLICATE ANALYSIS		
379GLBR- 5 Rep 1 Fraction 1	07OCT12:381SAL	10,620
379GLBR- 5 Rep 2 Fraction 1	07OCT12:381SAL	10,880
379GLBR- 5 Rep 3 Fraction 1	07OCT12:381SAL	13,370
	RSD %	13%
379GLBR- 5 Rep 1 Fraction 2	07OCT12:381SAL	10,230
379GLBR- 5 Rep 2 Fraction 2	07OCT12:381SAL	7,760
379GLBR- 5 Rep 3 Fraction 2	07OCT12:381SAL	8,940
	RSD %	14%
379GLBR- 5 Rep 1 Fraction 3	07OCT12:381SAL	7,160
379GLBR- 5 Rep 2 Fraction 3	07OCT12:381SAL	6,310
379GLBR- 5 Rep 3 Fraction 3	07OCT12:381SAL	10,300
	RSD %	27%
379GLBR- 5 Rep 1 Fraction 4	07OCT12:381SAL	5,710
379GLBR- 5 Rep 2 Fraction 4	07OCT12:381SAL	4,170
379GLBR- 5 Rep 3 Fraction 4	07OCT12:381SAL	5,010
	RSD %	16%
379GLBR- 121 Rep 1 Fraction 1	230CT4:354SA2M	34,150
379GLBR- 121 Rep 2 Fraction 1	23OCT4:354SA2M	35,460
379GLBR- 121 Rep 3 Fraction 1	23OCT4:354SA2M	36,550
	RSD %	3%
379GLBR- 121 Rep 1 Fraction 2	23OCT4:354SA2M	15,660
379GLBR- 121 Rep 2 Fraction 2	23OCT4:354SA2M	7,160
379GLBR- 121 Rep 3 Fraction 2	23OCT4:354SA2M	14,150
		· · • · •

MSL Code -	Sponsor ID	TOC ug/L
Method Detection Limit :		660
REPLICATE ANALYSIS		
379GLBR- 121 Rep 1 Fraction 3	23OCT4:354SA2M	3,560
379GLBR- 121 Rep 2 Fraction 3	230CT4:354SA2M	4,410
379GLBR- 121 Rep 3 Fraction 3	23OCT4:354SA2M	7,040
	RSD %	36%
379GLBR- 121 Rep 1 Fraction 4	230CT4:354SA2M	12,510
379GLBR- 121 Rep 2 Fraction 4	23OCT4:354SA2M	3,690
379GLBR- 121 Rep 3 Fraction 4	230CT4:354SA2M	4,440
	<b>RSD %</b>	71%

RSD % = Relative Standard Deviation.

NOTE: All results are blank-corrected.

l		Cr (ug/L)	Cu (ug/L)	Hg (ug/L)	Pb (ug/L)
MSL Code	Sponsor ID	AA	AA	CVAF	AA
Method Detection Limits		0.05	0.85		
	BIN A				
379GLBR- 5 Rep 1	07OCT12:381SAL	0.40	13.6	0.00216	21.95
379GLBR- 5 Rep 2	070CT12:381SAL	0.36	11.2	0.00094 U	19.88
379GLBR- 5 Rep 3	07OCT12:381SAL	0.36	11.7	0.00094 U	17.39
379GLBR- 8	07OCT12:301SAL	0.62	11.2	0.00094 U	16.15
379GLBR- 121 Rep 1	230CT4:354SA2M	0.22	5.3	0.00047 U	3.08
379GLBR- 121 Rep 2	230CT4:354SA2M	0.22	4.4	0.00047 U	3.08
379GLBR- 121 Rep 3	230CT4:354SA2M	0.36	2.9	0.00094 U	1.54
379GLBR- 154	250CT9:104SA3M	0.71	15.1	0.00094 U	6.55
379GLBR- 460	4DEC11:455SA2M	42.37	47.6	0.00094 U	0.72 L
379GLBR- 461	4DEC11:555SA2M	36.40	40.8	0.00094 U	0.72 L
379GLBR- 462	4DEC12:055SA2M	30.77	38.4	0.00094 U	0.69 L
379GLBR- 463	4DEC11:155SA3M	50.39	12.6	0.00094 U	0.69 L
379GLBR- 464	4DEC11:305SA3M	45.62	11.2	0.00094 U	0.69 L
379GLBR- 465	4DEC11:375SA3M	37.13	12.1	0.00094 U	0.69 L
	BIN B				
379GLBR- 7	07OCT12:571SBL	0.76	11.2	0.00094 U	16.57
379GLBR- 10	07OCT1:071SBL	0.62	12.1	0.00047 U	19.47
379GLBR- 214	31OCT9:304SB2M	0.13	2.4	0.00094 U	1.93
379GLBR- 250	31OCT2:404SB3M	0.71	13.6	0.00094 U	6.16
379GLBR- 466	4DEC12:505SB2M	18.04	11.7	0.00094 U	0.69 U
379GLBR- 467	4DEC1:005SB2M	17.50	13.1	0.00094 U	0.80
379GLBR- 468	4DEC1:155SB2M	18.04	14.6	0.00094 U	0.69 U
379GLBR- 469	4DEC1:255SB1/B3M	1.91	31.6	0.00996	1.20
379GLBR- 470	4DEC1:305SB1/B3M	2.29	29.6	0.00589	1.20
379GLBR- 471	4DEC1:355SB1/B3M	1.82	31.1	0.00695	0.80
BLANK-1		0.09	1.9	0.00094 U	0.72 U

MSL Code	Sponsor ID	Cr (ug/L)	Cu (ug/L)	Hg (ug/L)	Pb (ug/L)
Method Detection Limi	ts	0.05	0.85		
STANDARD REFEREN	ICE MATERIAL				
1643c-1 Rep		18.90	27.9	NA	00.40
1643c-1 Rep 2		18.37	30.1	NA NA	36.43
1643C-1 nep	certified	19.00	22.3	NA NA	35.42
•	Value	±0.6	±2.8	NA NA	35.3
	Agida	<b>10.6</b>	12.6	NA	±0.9
1641b Rep		NA	NA	1372	NA NA
1641b Rep 2		NA	NA NA	1452	NA.
1641b Rep 3		NA	NA	1484	NA
1641b Rep 4		NA	NA	1596	NA
1641b Rep 5		NA	NA	1572	NA
1641b Rep 6		NA	NA	1454	NA
	certified	NA	NA	1520	NA
	value	NA	NA NA	±40	NA NA
REPLICATE ANALYS	IS				
379GLBR- 5 Rep 1	07OCT12:381SAL	0.40	13.6	0.00216	21.95
379GLBR- 5 Rep 2	07OCT12:381SAL	. 0.36	11.2	0.00094 U	19.88
379GLBR- 5 Rep 3	070CT12:381SAL	. 0.36	11.7	0.00094 U	17.39
	RSI	0 % 6%	10%	NA	12%
379GLBR- 121 Rep 1	23OCT4:354SA2M	0.22	5.3	0.00047 U	3.08
379GLBR- 121 Rep 2	2 230CT4:354SA2M	0.22	4.4	0.00047 U	3.08
379GLBR- 121 Rep 3	230CT4:354SA2M	0.36	2.9	0.00094 U	1.54
	RSI	30%	29%	NA	35%

U = Detected at or below detection limit.

NA = Not applicable/analyzed.

RSD % = Relative Standard Deviation

MSL Code		Sponsor ID	Cr (ug/L)	Cu (ug/L)	Hg (ug/L)	Pb (ug/L)
		Bit A	7			
		BIN A				
379GLBR- 5	Rep 1 Fraction	1 07OCT12:381SAL	0.50	1.9 U	0.00094 U	0.701
O/BULDING S	•	2 07OCT12:381SAL	0.50			0.72 \
		3 07OCT12:381SAL	0.50	1.9 U		
		4 07OCT12:381SAL		5.2	0.00060	6.63
379GLBR- 5		1 07OCT12:381SAL	0.75	2.8	0.00047 U	4.56
oracen- o	•	2 07OCT12:381SAL	0.50	1.9 U		1.66
		3 07OCT12:381SAL	0.38 0.38	1.9 U		0.83
		4 07OCT12:381SAL	1.26	3.6 3.2	0.00069	5.80
379GLBR- 5		1 07OCT12:381SAL	0.50	3.2 1.9 U	0.00047 U	3.31
S/SGEBH- S		2 07OCT12:381SAL	0.50		0.00047 U	1.24
		3 07OCT12:381SAL	0.76	1.9 U	0.00047 U	1.66
		4 07OCT12:381SAL	0.76	2.4	0.00047 U	4.56
379GLBR- 8		1 07OCT12:301SAL	0.30 0.23 U	2.0	0.00047 U	2.07
37302011-0		2 07OCT12:301SAL			0.00047 U	1.18 U
		3 07OCT12:301SAL	0.23 U		0.00047 U	1.18 U
		4 070CT12:301SAL	0.23 U		0.00047 U	1.18 U
270CLDD 404			0.23 U		0.00047 U	1.18 U
3/9GLBH- 121	*	1 23OCT4:354SA2M	0.87	1.7	0.00047 U	0.60 U
		2 23OCT4:354SA2M	0.22	0.8	0.00024 U	0.60 U
		3 23OCT4:354SA2M	0.36	2.5	0.00024 U	1.00
370GLBB_ 121		4 230CT4:354SA2M 1 230CT4:354SA2M	0.36	2.5	0.00024 U	1.33
0/9GLBN- 121		2 230CT4:354SA2M	0.23 U		0.00047 U	0.60 U
		2 230CT4:354SA2M 3 230CT4:354SA2M	0.23 U		0.00024 U	0.67
		230CT4:354SA2M	0.23	2.1	0.00024 U	1.00
370GI BD. 121		230CT4:354SA2M	0.23 U		0.00026	1.67
3/3GLBH- 121		230CT4:354SA2M 2 230CT4:354SA2M	0.23 U		0.00024 U	0.60 U
		3 230CT4:354SA2M	0.23 U		0.00024 U	0.60 U
•		230CT4:354SA2M	0.29	2.1	0.00024 U	2.00
379GLBR- 154			0.29	1.3	0.00035	1.33
3/9GLBH- 134		250CT9:104SA3M	1.01	20.1	0.00149	0.72 U
		2 25OCT9:104SA3M 3 25OCT9:104SA3M	0.64	14.2	0.00066	0.72 U
			0.65	5.9	0.00255	3.82
379GLBR- 460		25OCT9:104SA3M	0.65	5.9	0.00197	4.77
79GLDN- 460		4DEC11:455SA2M	8.40	70.7	0.00156	7.23
		4DEC11:455SA2M	6.70	35.8	0.00024 U	6.37
		4DEC11:455SA2M 4DEC11:455SA2M	5.90	25.7	0.00076	2.31
379GLBR- 461			9.80	22.3	0.00091	0.87
// 3GLDU- 40 i		4DEC11:555SA2M	8.70	53.5	0.00066	8.39
		4DEC11:555SA2M	6.80	34.5	0.00036	6.65
		4DEC11:555SA2M	5.70	25.7	0.00107	4.05
379GLBR- 464		4DEC11:555SA2M	7.90	20.2	0.00054	0.87
379GLBR- 464 379GLBR- 465		4DEC11:305SA3M	13.10	16.9	0.00024	6.91
,, adrou- 400	rraction 1	4DEC11:375SA3M	11.20	13.2	0.00036	6.50

MSL Code		Sponsor ID	Cr (ug/L)	Cu (ug/L)	Hg (ug/L)	Pb (ug/L)
		•	······	· · · · · · · · · · · · · · · · · · ·		
		BIN A	j			
379GLBR- 462	Fraction 1	4DEC12:055SA2M	8.00	56.4	0.00082	8.68
		4DEC12:055\$ 42M	7.00	35.8	0.00040	8.10
		4DEC12:055SA2M	8.20	27.4	0.00087	4.34
		4DEC12:055SA2M	9.20	23.6	0.00098	1.16
379GLBR- 463		4DEC11:155SA3M	9.50	10.5	0.00031	7.81
		4DEC11:155SA3M	8.80	6.7	0.00030	5.50
		4DEC11:155SA3M	12.50	5.5	0.00051	5.21
		4DEC11:155SA3M	13.60	5.1	0.00045	4.34
		BIN B	1			
379GLBR- 7	Fraction 1	07OCT12:571SBL	0.23 U		0.00047 U	
		07OCT12:571SBL	0.30	0.73 U	0.00047 U	0.60
	Fraction 3	07OCT12:571SBL	0.38	3.8	0.00024 U	3.81
		07OCT12:571SBL	0.23	1.3	0.00039	0.69
379GLBR- 10	Fraction 1	07OCT1:071SBL	1.40	8.0	0.00047	9.83
		07OCT1:071SBL	1.30	6.6	0.00024 U	9.17
	Fraction 3	07OCT1:071SBL	1.70	8.9	0.00024 U	10.81
	Fraction 4	07OCT1:071SBL	1.00	7.1	0.00025	9.17
379GLBR- 214	Fraction 1		0.23 U	2.4	0.00047 U	0.72
		31OCT9:304SB2M	0.23 U	1.9 U	0.00047 U	0.72
	Fraction 3	31OCT9:304SB2M	0.23 U	1.9 U	0.00047 U	0.72
	Fraction 4	31OCT9:304SB2M	0.23 U	1.9 U	0.00055	0.72
379GLBR- 250	Fraction 1	31OCT2:404SB3M	0.60	4.7	0.00054	0.57
	Fraction 2	31OCT2:404SB3M	0.50	1.9	0.00064	0.62
		31OCT2:404SB3M	0.70	5.2	0.00113	3.71
	Fraction 4	31OCT2:404SB3M	0.70	3.3	0.00143	3.09
379GLBR- 466	Fraction 1		15.40	15.5	0.00024 U	7.72
	–	4DEC12:505SB2M	15.30	9.4	0.00024 U	6.50
		4DEC12:505SB2M	14.60	8.5	0.00040	6.10
		4DEC12:505SB2M	14.80	6.6	0.00030	4.06
379GLBR- 467		4DEC1:005SB2M	10.00	17.9	0.00027	6.50
379GLBR- 468		4DEC1:155SB2M	9.90	17.4	0.00027	6.10
379GLBR- 469		4DEC1:255SB1/B3M	3.68	133.2	0.00047 U	10.98
		4DEC1:255SB1/B3M	3.22	88.3	0.00047 U	5.66
		4DEC1:255SB1/B3M	3.95 •	81.3	0.00047 U	1.77
		4DEC1:255SB1/B3M	4.96	64.6	0.00047 U	0.72 ل
379GLBR- 470		4DEC1:305SB1/B3M	6.90	121.7	0.00133	18.70
379GLBR- 471	Fraction 1	4DEC1:355SB1/B3M	7.70	121.3	0.00132	10.57

MCI Cada		,		Cr (ug/L)	Cu (ug/L)	Hg (ug/L)	Pb (ug/L)
MSL Code		Sponse	or ID		AA	CVAF	AA
BLANK-1	Fra	ction 1		0.23	U 1.9 ប	0.00047	0.72 (
BLANK-1	Fra	ction 2 :		0.23		0.00047	0.72 t
BLANK-1	Fra	ction 3		0.23		0.00047 U	0.72 t
BLANK-1	Fra	ction 4		0.23		0.00047 U	0.72 (
BLANK-2	Fra	ction 1		0.30	0.73 U	0.00024 U	0.72 t
BLANK-2	Frac	ction 2		0.23		0.00024 U	0.60 t
BLANK-2	Frac	ction 3		0.30	0.80	0.00024 U	0.60 t
BLANK-2	Frac	ction 4		0.23		0.00024 0	0.60 L
BLANK-3	Frac	ction 1		0.20		0.00070	0.57 L
BLANK-3	Frac	ction 2		0.50	0.82 U	0.00028	0.57 t
BLANK-3	Frac	ction 3		0.20		0.00058	0.57 L
BLANK-3	Frac	ction 4		0.20		0.00036	0.57 L
				0.20	0.02 0	0.00026	0.57
STANDARD F	REFERENCE N	IATERIAL					
1643c-1	Rep 1			19.59	27.5	NA	35 Ec
	Rep 1 Rep 2			19.59 20.81	27.5 25.8	NA NA	35.56 36.48
1643c-1				20.81	25.8	NA	36.48
643c-1 643c-2	Rep 2			20.81 19.50	25.8 26.5	NA NA	36.48 36.92
1643c-1 1643c-1 1643c-2 1643c-2	Rep 2 Rep 1			20.81 19.50 19.10	25.8 26.5 26.5	NA NA NA	36.48 36.92 37.85
643c-1 643c-2 643c-2 643c-3	Rep 2 Rep 1 Rep 2			20.81 19.50 19.10 19.80	25.8 26.5 26.5 26.3	NA NA NA NA	36.48 36.92 37.85 33.74
1643c-1 1643c-2 1643c-2	Rep 2 Rep 1 Rep 2 Rep 1			20.81 19.50 19.10 19.80 19.40	25.8 26.5 26.5 26.3 25.9	NA NA NA NA	36.48 36.92 37.85 33.74 36.95
643c-1   643c-2   643c-2   643c-3	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1	rtified		20.81 19.50 19.10 19.80 19.40 NA	25.8 26.5 26.5 26.3 25.9 NA	NA NA NA NA NA	36.48 36.92 37.85 33.74 36.95 37.56
643c-1   643c-2   643c-2   643c-3	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1	rtified value		20.81 19.50 19.10 19.80 19.40 NA 19.00	25.8 26.5 26.5 26.3 25.9 NA 22.3	NA NA NA NA NA NA	36.48 36.92 37.85 33.74 36.95 37.56 35.30
643c-1 643c-2 643c-2 643c-3 643c-3	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1			20.81 19.50 19.10 19.80 19.40 NA	25.8 26.5 26.5 26.3 25.9 NA	NA NA NA NA NA	36.48 36.92 37.85 33.74 36.95 37.56
1643c-1 1643c-2 1643c-2 1643c-3	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1			20.81 19.50 19.10 19.80 19.40 NA 19.00 ±0.6	25.8 26.5 26.5 26.3 25.9 NA 22.3 ±2.8	NA NA NA NA NA NA	36.48 36.92 37.85 33.74 36.95 37.56 35.30 ±0.90
643c-1 643c-2 643c-3 643c-3 643c-4	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1 Cer			20.81 19.50 19.10 19.80 19.40 NA 19.00 ±0.6	25.8 26.5 26.5 26.3 25.9 NA 22.3 ±2.8	NA NA NA NA NA NA NA	36.48 36.92 37.85 33.74 36.95 37.56 35.30 ±0.90
643c-1 643c-2 643c-3 643c-3 643c-4 641b	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1 Cer			20.81 19.50 19.10 19.80 19.40 NA 19.00 ±0.6	25.8 26.5 26.5 26.3 25.9 NA 22.3 ±2.8	NA NA NA NA NA NA 1465 1367	36.48 36.92 37.85 33.74 36.95 37.56 35.30 ±0.90
641b 641b 641c-1	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1 Cer			20.81 19.50 19.10 19.80 19.40 NA 19.00 ±0.6	25.8 26.5 26.5 26.3 25.9 NA 22.3 ±2.8 NA NA	NA NA NA NA NA NA 1465 1367	36.48 36.92 37.85 33.74 36.95 37.56 35.30 ±0.90 NA NA
1643c-1 1643c-2 1643c-2 1643c-3 1643c-3	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1 Cer Rep 1 Rep 2 Rep 3 Rep 4			20.81 19.50 19.10 19.80 19.40 NA 19.00 ±0.6	25.8 26.5 26.5 26.3 25.9 NA 22.3 ±2.8 NA NA	NA NA NA NA NA NA 1465 1367 1442 1504	36.48 36.92 37.85 33.74 36.95 37.56 35.30 ±0.90 NA NA NA
643c-1 643c-2 643c-3 643c-3 643c-4 641b 641b 641b 641b	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1 Cer Rep 1 Rep 2 Rep 2 Rep 3			20.81 19.50 19.10 19.80 19.40 NA 19.00 ±0.6 NA NA NA	25.8 26.5 26.5 25.9 NA 22.3 ±2.8 NA NA NA	NA NA NA NA NA NA 1465 1367 1442 1504 1440	36.48 36.92 37.85 33.74 36.95 37.56 35.30 ±0.90 NA NA NA
643c-1 643c-2 643c-3 643c-3 643c-4 641b 641b 641b 641b 641b	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1 Rep 1 Rep 2 Rep 3 Rep 3 Rep 4 Rep 5 Rep 6			20.81 19.50 19.10 19.80 19.40 NA 19.00 ±0.6 NA NA NA NA	25.8 26.5 26.3 25.9 NA 22.3 ±2.8 NA NA NA	NA NA NA NA NA NA 1465 1367 1442 1504 1440 1530	36.48 36.92 37.85 33.74 36.95 37.56 35.30 ±0.90 NA NA NA NA
643c-1 643c-2 643c-3 643c-3 643c-4 641b 641b 641b	Rep 2 Rep 1 Rep 2 Rep 1 Rep 2 Rep 1 Cer Rep 1 Rep 2 Rep 3 Rep 3 Rep 4 Rep 5 Rep 6 Rep 7			20.81 19.50 19.10 19.80 19.40 NA 19.00 ±0.6 NA NA NA	25.8 26.5 26.5 25.9 NA 22.3 ±2.8 NA NA NA	NA NA NA NA NA NA 1465 1367 1442 1504 1440	36.48 36.92 37.85 33.74 36.95 37.56 35.30 ±0.90 NA NA NA

MSL Code		Sponsor ID	Cr (ug/L)	Cu (ug/L)	Hg (ug/L)	Pb (ug/L)
REPLICATE AN	IALYSIS					
379GLBR- 5		07OCT12:381SAL	0.50	1.9 U		
379GLBR- 5		07OCT12:381SAL	0.50	1.9 U		
379GLBR- 5	Rep 3 Fraction	07OCT12:381SAL	0.50	1.9 U		
		RSD %	0%	NA	NA	29%
379GLBR- 5	Rep 1 Fraction	2 07OCT12:381SAL	0.50	1.9 U	0.00047 U	0.72 เ
379GLBR- 5	Rep 2 Fraction	07OCT12:381SAL	0.38	1.9 U	0.00047 U	0.83
379GLBR- 5	Rep 3 Fraction 2	07OCT12:381SAL	0.76	1.9 U	0.00047 U	1.66
		RSD %	35%	NA	NA	67%
379GLBR- 5	Rep 1 Fraction	070CT12:381SAL	0.50	5.2	0.00060	6.63
379GLBR- 5	•	07OCT12:381SAL	0.38	3.6	0.00069	5.80
379GLBR- 5	Rep 3 Fraction	07OCT12:381SAL	0.76	2.4	0.00047 U	4.56
•	·	RSD %	35%	38%	14%	18%
379GLBR- 5		07OCT12:381SAL	0.75	2.8	0.00047 U	4.56
379GLBR- 5		07OCT12:381SAL	1.26	3.2	0.00047 U	3.31
379GLBR- 5	Rep 3 Fraction	070CT12:381SAL	0.50	2.0	0.00047 U	2.07
		RSD %	46%	23%	NA	38%
	• • • • • • • • • • • • • • • • • • •	23OCT4:354SA2M	0.87	1.7	0.00047 U	0.60 ل
	•	23OCT4:354SA2M	0.22	0.8	0.00047 U	0.60 l
379GLBR- 121	Rep 3 Fraction 1	230CT4:354SA2M	0.36	0.73 U	0.00024 U	0.60 L
		RSD %	71%	72%	NA	NA
379GLBR- 121	Rep 1 Fraction 2	230CT4:354SA2M	0.36	0.8	0.00024 U	0.60 L
	•	230CT4:354SA2M	0.23 U		0.00024 U	0.67
379GLBR- 121	Rep 3 Fraction 2	2 23OCT4:354SA2M	0.23 U		0.00024 U	0.60 L
		RSD %	NA	30%	NA	NA
379GLBR- 121	Rep 1 Fraction 3	230CT4:354SA2M	0.23	2.5	0.00024 U	1.00
	•	23OCT4:354SA2M	0.23 U		0.00024 U	1.00
379GLBR- 121	Rep 3 Fraction 3	3 23OCT4:354SA2M RSD %	0.23 U NA	2.1 10%	0.00024 U NA	2.00 <b>43%</b>
			170	,0,0		
	•	23OCT4:354SA2M	0.36	2.5	0.00024 U	1.33
	•	23OCT4:354SA2M	0.23 U		0.00026	1.67
379GLBR- 121	Rep 3 Fraction 4	23OCT4:354SA2M	0.29	1.3	0.00035	1.33
	at ar bolow dotoe	RSD %	22%	33%	30%	16%

U = Detected at or below detection limit.

NA = Not applicable/analyzed.

NS = Not spiked.

RSD % = Relative Standard Deviation.

# REPORT OF CHEMICAL ANALYSES

Volume 3: Organics

PROJECT: Buffalo River Pilot Project

# Prepared for:

USEPA Great Lakes National Program Office Attn: Mr. Steve Garbaciak 230 S. Dearborn Chicago, IL 60604 REPORT OF: CHEMICAL ANALYSES

PROJECT: BUFFALO RIVER PILOT PROJECT DATE: May 26, 1992

ISSUED TO: Mr. Steve Garbaciak CF#: 379GLBR

Technical Project Manager
USEPA Great Lakes National Program Office

230 S. Dearborn

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### INTRODUCTION

This report summarizes the results from analyses performed on pilot study samples which were submitted by the U.S. Army Corps of Engineers Great Lakes Division, Buffalo District.

### SAMPLE CUSTODY

Samples were received in good condition from October 7, 1991 through December 5, 1991. Samples were logged in and stored as specified in the narrative. Samples were analyzed within the holding times specified in the QA plan. Any exceptions are noted in the narrative associated with each analysis.

### AIR SAMPLES

Five samples and one solvent blank were analyzed for dioxin/furans, PAH's and PCB's. Samples were stored at 4°±2°C prior to shipment to Twin City Testing for analysis of dioxin/furans, PAHs and PCBs. The samples were extracted in their entirety, therefore re-analysis was not possible. Included with this report are copies of the text which accompanied Twin City Testing's report for the air samples. Please refer to that data for information on extraction, analysis, quality control and any problems associated with analysis of the air samples. No samples were received to be archived.

### SAMPLE IDENTIFICATION

Sponsor ID	Sample Type	<u>Analyses</u>	Battelle ID
220CT5:0011GA10	Air	D/F, PAH, PCB	379GLBR*112
23OCT4:4511GA2O	Air	D/F, PAH, PCB	379GLBR*232
24OCT5:3011GA3O	Air	D/F, PAH, PCB	379GLBR*233
250CT1:4511GB10	Air	D/F, PAH, PCB	379GLBR*234
310CT1:0011GB30	Air	D/F, PAH, PCB	379GLBR*272

### SEDIMENT and WATER SAMPLES

Fifty-one sediment samples were analyzed for PAHs and oil and grease. Forty-six sediment samples were analyzed for PAHs, PCBs and oil and grease. Samples were stored at -22°±3°C prior to analysis. Oil and grease in sediment was determined according to "SOP for the Analysis of Solvent-Extractable Residue from Whole Sediment" taken from EPA-LLRS-GROSSE and supplied by the Great Lakes Large Lakes Lab. Twenty-three water samples were analyzed for PAHs, PCBs and oil and grease. Samples were stored at 4°±2°C prior to analysis. Since the organics lab extracted the entire sample for PAH and PCB analysis, and oil and grease used most of the duplicate sample, re-extractions were virtually impossible. On one occasion the organic samples were logged in incorrectly, as though each sample (including the duplicates) was a separate sample with each receiving an individual sample ID. In these

instances, the organics analyst extracted each sample in it's entirety, leaving no sample for oil and grease. To compensate for this error, metals samples or TOC samples collected from the same time and point of the processor were extracted for oil and grease. Although the metals and TOC samples had been preserved with acid, according to Standard Methods, acidifying an oil and grease sample does not affect the results. Oil and grease in water was determined following Standard Methods, 5520B, substituting methylene chloride for freon. Most water samples posed a problem using this method due to a high content of particulate matter in the sample. After some discussion with Eric Crecelius (program manager), the analyst was instructed to decant and extract the liquid layer. The particulate fraction was not extracted, but was archived for possible analysis in the future.

Water samples for PAHs and PCBs were extracted by shaking with methylene chloride in a large separatory funnel. Three consecutive extractions were performed on each sample, exchanging solvent after each extraction period following SOP #MSL-M-41. Samples were then cleaned using Silica/Alumina (5% deactivated) chromatography, followed by HPLC cleanup (Krahn et al. 1988). PAH extracts were analyzed using Gas Chromatography/Mass Spectrometry (GC/MS) in the selected ion mode (SIM). PCB extracts were analyzed using Gas Chromatography/Electron Capture Detection (GC/ECD). The column used was a J&W DB-5 capillary column (30m x 0.25mm I.D.). Sediment samples for PAHs and PCBs were extracted with methylene chloride using the ambient rolling technique. Three consecutive extractions were performed on each sample, exchanging solvent after each extraction period following SOP #MSL-M-42. Samples were then cleaned using Silica/Alumina (5% deactivated) chromatography followed by HPLC cleanup (Krahn et al. 1988). Extracts for PAHs were analyzed using Gas Chromatography/Mass Spectrometry (GC/MS) in the selected ion mode (SIM). Extracts for PCBs were analyzed using Gas Chromatography/Electron Capture Detection (GC/ECD). The column used was a J&W DB-5 capillary column (30m x 0.25mm I.D.).

For the majority of water samples to be analyzed for PAHs and PCBs, extraction exceeded the recommended 7-day holding time. However, due to the stable nature of PCB compounds and storage methods, the quality of the data should not be affected. Holding times from extraction to initial analyses were generally within EPA's recommended holding time of 40 days (EPA 1986). However, diluted samples were run approximately 30 to 40 days outside of these holding times. Values for diluted sample analyses generally agreed well with the initial quantitation, therefore, this added time does not appear to have biased the diluted results. Sediment samples for PAHs were extracted in 5 batches from 2/6/92 to 3/4/92 and analyzed from 3/31/92 to 4/18/92. Samples that required re-analysis were extracted on 4/22/92 and analyzed on 5/4/92. Samples that required dilution were analyzed on 5/1/92. One batch of sediment analyses requested as a rush by EPA GLNPO were extracted on 10/10/91 and analyzed on 10/14/92. Sediment samples for PCBs were extracted simultaneously with those for PAHs and analyzed from 4/20/92 through 4/26/92.

Target detection limits of 0.02  $\mu$ g/L for PAHs in water were slightly exceeded in a number of cases. Detection limits ranged from 0.007  $\mu$ g/L to 0.07  $\mu$ g/L. In general, levels of PAHs exceeded these amounts in all but three samples. Target detection limits of 0.01  $\mu$ g/L for PCBs in water were slightly exceeded for Aroclors. Detection limits averaged 0.05  $\mu$ g/L to 0.2  $\mu$ g/L for undiluted samples and from 0.5 to 2  $\mu$ g/L for diluted samples. In most cases, PCBs in the samples analyzed exceeded these amounts. Sediment PAH target detection limits of 0.02  $\mu$ g/Kg were slightly exceeded, ranging from 0.004 to 0.053  $\mu$ g/Kg. Sediment PCB target detection limits of 0.02  $\mu$ g/Kg were slightly exceeded, ranging from 0.025 to 0.060  $\mu$ g/Kg. Detection limits reported were instrument detection limits based on a minimum area, background noise and the analyst's judgement on the level that was quantifiable.

# SAMPLE IDENTIFICATION

Spansor ID	Sample Type	Analyses	Battelle ID
Sponsor ID 07OCT12:341SAO	Sediment	PAH, Oil & Gr	379GLBR*13
	Sediment	PAH, Oil & Gr	379GLBR*14
07OCT1:101SBO		PAH, Oil & Gr	379GLBR*16
07OCT12:401SAO	Sediment	PAH, Oil & Gr	379GLBR*18
07OCT1:331SCO	Sediment	•	379GLBR*19
07OCT2:041SDO	Sediment	PAH, Oil & Gr	
07OCT1:441SCO	Sediment	PAH, Oil & Gr	379GLBR*20
07OCT1:011SBO	Sediment	PAH, Oil & Gr	379GLBR*23
07OCT2:121SDO	Sediment	PAH, Oil & Gr	379GLBR*24
08OCT5:402SD1O	Sediment	PAH, Oil & Gr	379GLBR*51
08OCT5:302SD2O	Sediment	PAH, Oil & Gr	379GLBR*53
09OCT11:502SA3O	Sediment	PAH, Oil & Gr	379GLBR*57
09OCT11:282SA1O	Sediment	PAH, Oil & Gr	379GLBR*59
09OCT10:152SB2O	Sediment	PAH, Oil & Gr	379GLBR*66
09OCT10:352SB3O	Sediment	PAH, Oil & Gr	379GLBR*67
09OCT4:352SC2O	Sediment	PAH, Oil & Gr	379GLBR*74
09OCT4:162SC3O	Sediment	PAH, Oil & Gr	379GLBR*75
22OCT5:563SA2O	Sediment	PAH, Oil & Gr	379GLBR*111
23OCT1:303SA2O	Sediment	PAH, Oil & Gr	379GLBR*113
23OCT4:284SA2O	Sediment	PAH, Oil & Gr	379GLBR*122
230CT4:294SA2O	Sediment	PAH, Oil & Gr	379GLBR*124
24OCT2:203SA3O	Sediment	PAH, Oil & Gr	379GLBR*141
240CT5:503SA3O	Sediment	PAH, Oil & Gr	379GLBR*143
	Sediment	PAH, Oil & Gr	379GLBR*151
25OCT9:224SA3O	= = =	PAH, Oil & Gr	379GLBR*152
25OCT9:224SA3O	Sediment	-	379GLBR*176
250CT2:153SB10	Sediment	PAH, Oil & Gr	
25OCT2:294SB1O	Sediment	PAH, Oil & Gr	379GLBR*182
25OCT2:284SB1O	Sediment	PAH, Oil & Gr	379GLBR*183
300CT2:493SB2O	Sediment	PAH, Oil & Gr	379GLBR*198
300CT4:413SB2O	Sediment	PAH, Oil & Gr	379GLBR*206
310CT9:264SB2O	Sediment	PAH, Oil & Gr	379GLBR*220
310CT9:254SB2O	Sediment	PAH, Oil & Gr	379GLBR*221
310CT10:453SB3O	Sediment	PAH, Oil & Gr	379GLBR*242
310CT2:303SB3O	Sediment	PAH, Oil & Gr	379GLBR*244
31OCT2:384SB3O	Sediment	PAH, Oil & Gr	379GLBR*247
310CT2:364SB30	Sediment	PAH, Oil & Gr	379GLBR*249
18NOV2:553SC1O	Sediment	PAH, Oil & Gr	379GLBR*280
18NOV4:403SC1O	Sediment	PAH, Oil & Gr	379GLBR*284
19NOV9:004SC1O	Sediment	PAH, Oil & Gr	379GLBR*303
19NOV9:014SC1O	Sediment	PAH, Oil & Gr	379GLBR*304
19NOV2:203SC2O	Sediment	PAH, Oil & Gr	379GLBR*313
19NOV2:2035020 19NOV3:553SC2O	Sediment	PAH. Oil & Gr	379GLBR*315
	Sediment	PAH, Oil & Gr	379GLBR*324
19NOV4:504SC2O	Sediment	PAH, Oil & Gr	379GLBR*325
19NOV4:504SC2O	Sediment	PAH, Oil & Gr	379GLBR*342
20NOV1:003SC3O		PAH, Oil & Gr	379GLBR*344
20NOV1:553SC3O	Sediment	PAH, Oil & Gr	379GLBR*351
20NOV3:154SC3O	Sediment	•	379GLBR*352
20NOV3:154SC3O	Sediment	PAH, Oil & Gr	3/3GLDN 332

21NOV12:003SD1O	Sediment	PAH, Oil & Gr	379GLBR*376
21NOV2:433SD1O	Sediment	PAH, Oil & Gr	379GLBR*380
21NOV5:224SD1O	Sediment	PAH, Oil & Gr	379GLBR*396
21NOV5:224SD1O	Sediment	PAH, Oil & Gr	379GLBR*397
070CT1211SCO	Sediment	PAH, PCB, Oil & Gr	379GLBR*15
07OCT12:091SAO	Sediment	PAH, PCB, Oil & Gr	379GLBR*17
07OCT12:531SBO	Sediment	PAH, PCB, Oil & Gr	379GLBR*21
07OCT1:521SDO	Sediment .	PAH, PCB, Oil & Gr	379GLBR*22
08OCT5:132SD3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*46
09OCT11:382SA2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*58
09OCT9:542SB1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*65
09OCT4:562SC1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*73
220CT11:317SA10	Sediment	PAH, PCB, Oil & Gr	379GLBR*104
220CT11:378SA10	Sediment	PAH, PCB, Oil & Gr	379GLBR*107
22OCT4:203SA2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*108
23OCT4:274SA2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*123
24OCT10:457SA2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*136
24OCT10:508SA2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*139
24OCT6:203SA3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*145
25OCT9:214SA3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*153
25OCT9:307SA3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*166
25OCT9:368SA3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*167
250CT12:153SB10	Sediment	PAH, PCB, Oil & Gr	379GLBR*174
25OCT2:254SB1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*181
25OCT3:527SB1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*193
25OCT3:578SB1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*196
30OCT2:573SB2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*199
31OCT9:027SB2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*210
31OCT9:078SB2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*213
31OCT9:244SB2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*222
310CT11:503SB3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*243
310CT2:354SB30	Sediment	PAH, PCB, Oil & Gr	379GLBR*248
1NOV10:208SB3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*268
1NOV10:157SB3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*269
18NOV3:503SC1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*282
19NOV9:347SC1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*288
19NOV9.5473C10	Sediment	PAH, PCB, Oil & Gr	379GLBR*302
19NOV9:238SC1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*307
19NOV11:303SC2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*311
19NOV4:504SC2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*323
20NOV8:157SC2O	Sediment	PAH, PCB, Oil & Gr	379GLBR*337
	Sediment	PAH, PCB, Oil & Gr	379GLBR*340
20NOV11:443SC3O		PAH, PCB, Oil & Gr	379GLBR*350
20NOV3:154SC3O	Sediment Sediment	PAH, PCB, Oil & Gr	379GLBR*357
20NOV3:337SC3O	Sediment Sediment	-	379GLBR*360
20NOV3:278SC3O	Sediment Sediment	PAH, PCB, Oil & Gr PAH, PCB, Oil & Gr	379GLBR 360 379GLBR*378
21NOV1:353SD1O 21NOV5:078SD1O	Sediment Sediment	PAH, PCB, Oil & Gr	379GLBR 376 379GLBR*384
	Sediment	PAH, PCB, Oil & Gr	379GLBR*388
21NOV5:107SD1O 21NOV5:224SD1O	Sediment	PAH, PCB, Oil & Gr	379GLBR*395
230CT4:459LA20	Oil	PAH, PCB, Oil & Gr	379GLBR 395 379GLBR*128
230014.433LA20	OII	FAN, FUB, UII & UI	3/3GLBN 120

0000TE:0010LA20	Water	PAH, PCB, Oil & Gr	379GLBR*132
23OCT5:2010LA2O	Water	PAH, PCB	379GLBR*160*
250CT10:1810LA30		PAH, PCB	379GLBR*161*
250CT10:1910LA30	Water		379GLBR*163**
25OCT10:2010LA3M	Water	Oil & Gr (metals)	
250CT9:549LA3O	Oil	PAH, PCB	379GLBR*164*
25OCT10:009LA3C	Oil	Oil & Gr (TOC)	379GLBR*165**
25OCT3:0810LB1O	Water	PAH, PCB, Oil & Gr	
300CT4:206LA30	Water -	PAH, PCB, Oil & Gr	379GLBR*204
310CT10:119LB20	Oil	PAH, PCB, Oil & Gr	379GLBR*226
310CT10:2310LB20	Water	PAH, PCB, Oil & Gr	379GLBR*227
310CT3:119LB30	Oil :	PAH, PCB	379GLBR*252*
310CT3:109LB3O	Oil	PAH, PCB	379GLBR*253*
310CT2:5710LB3M	Water	Oil & Gr (metals)	379GLBR*254**
31OCT3:069LB3M	Oil	Oil & Gr (metals)	379GLBR*255**
310CT3:0110LB30	Water	PAH, PCB	379GLBR*256*
310CT3:0010LB30	Water	PAH, PCB, Oil & Gr	379GLBR*257
6NOV12:003LO	Water	PAH, PCB, Oil & Gr	379GLBR*275
18NOV5:559LC1O	Oil	PAH, PCB, Oil & Gr	379GLBR*286
18NOV6:1510LC1O	Water	PAH, PCB, Oil & Gr	379GLBR*287¥
19NOV5:519LC2O	Oil	PAH, PCB, Oil & Gr	379GLBR*326
	Water	PAH, PCB, Oil & Gr	379GLBR*331
19NOV5:0510LC2O		PAH, PCB, Oil & Gr	379GLBR*361
20NOV2:193LC3O	Water		
20NOV2:419LC3O	Oil	PAH, PCB, Oil & Gr	379GLBR*366
20NOV3:0110LC3O	Water	PAH, PCB, Oil & Gr	379GLBR*370
21NOV3:2610LD1O	Water	PAH, PCB, Oil & Gr	379GLBR*398
21NOV4:169LD1O	Oil	PAH, PCB, Oil & Gr	379GLBR*404

# ARCHIVED SAMPLES

MIGHTED OWN FED			
Sponsor ID	Sample Type	<u>Analyses</u>	Battelle ID
210CT12:483SA10	Sediment	PAH, Oil & Gr	379GLBR*83
210CT12:493SA10	Sediment	PAH, Oil & Gr	379GLBR*84
21OCT5:444SA1O	Sediment	PAH, Oil & Gr	379GLBR*92
21OCT5:464SA1O	Sediment	PAH, Oil & Gr	379GLBR*93
22NOV12:153SD2O	Sediment	PAH, Oil & Gr	379GLBR*408
22NOV1:153SD2O	Sediment	PAH, Oil & Gr	379GLBR*409
22NOV3:104SD2O	Sediment	PAH, Oil & Gr	379GLBR*418
22NOV3:104SD2O	Sediment	PAH, Oil & Gr	379GLBR*419
25NOV1:003SD3O	Sediment	PAH, Oil & Gr	379GLBR*436
25NOV1:403SD3O	Sediment	PAH, Oil & Gr	379GLBR*438
25NOV4:004SD3O	Sediment	PAH, Oil & Gr	379GLBR*444
25NOV4:004SD3O	Sediment	PCB, Oil & Gr	379GLBR*450
08OCT5:102SD3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*46-T1
08OCT5:112SD3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*46-T2
08OCT5:122SD3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*46-T3
08OCT5:132SD3O	Sediment	PAH, PCB, Oil & Gr	379GLBR*46-M1
210CT12:473SA10	Sediment	PAH, PCB, Oil & Gr	379GLBR*82

<sup>\*</sup>Samples extracted for PAH and PCB only.
\*\*Samples extracted for oil/grease and metals or TOC.
\*\*Sample was not analyzed.

210CT5:454SA10	S	ediment		PAH, PCB, Oil 8	e Gr	379GLBR*91
30OCT2:473SB2O		ediment		PAH, PCB, Oil &		379GLBR*199-T1
30OCT4:013SB2O		ediment		PAH, PCB, Oil &		379GLBR*199-T2
30OCT2:523SB2O		ediment		PAH, PCB, Oil &		379GLBR 199-12 379GLBR*199-M1
300CT4:453SB2O		ediment		PAH, PCB, Oil &		
19NOV4:504SC2O		ediment				379GLBR*199-M2
19NOV4:504SC2O	,	ediment		PAH, PCB, Oil &		379GLBR*323-T1
				PAH, PCB, Oil &		379GLBR*323-T2
19NOV4:504SC2O		ediment -		PAH, PCB, Oil &		379GLBR*323-M1
19NOV4:504SC2O		ediment	•	PAH, PCB, Oil 8		379GLBR*323-M2
20NOV2:193LC3O		ediment		PAH, PCB, Oil 8		379GLBR*361-1
21NOV5:078SD1O		ediment		PAH, PCB, Oil 8		379GLBR*384-T1
21NOV5:078SD10		ediment		PAH, PCB, Oil 8		379GLBR*384-T2
21NOV5:078SD1O		ediment		PAH, PCB, Oil 8		379GLBR*384-M1
21NOV5:078SD1O		ediment		PAH, PCB, Oil 8	& Gr	379GLBR*384-M2
22NOV1:453SD2O		ediment		PAH, PCB, Oil 8	& Gr	379GLBR*412
22NOV3:104SD2O	Se	ediment		PAH, PCB, Oil 8	4 Gr	379GLBR*417
22NOV3:308SD2O	Se	ediment		PAH, PCB, Oil 8	Gr	379GLBR*423
25NOV2:203SD3O	Se	ediment		PAH, PCB, Oil 8		379GLBR*440
25NOV4:004SD3O		ediment		PAH, PCB, Oil 8		379GLBR*449
	41			,,		0.0022
210CT6:1810LA10	W	ater		PAH, PCB, Oil 8	Gr	379GLBR*97
210CT6:2010LA10		ater		PAH, PCB, Oil 8		379GLBR*97-T1
210CT6:2210LA10		ater		PAH, PCB, Oil &		379GLBR*97-T2
210CT6:1610LA10		ater		PAH, PCB, Oil &		379GLBR*97-T3
230CT4:459LA20		ater		PAH, PCB, Oil &		379GLBR*128-1
230CT4:459LA20		ater				
230CT4:459LA20		ater		PAH, PCB, Oil &		379GLBR*128-2
230CT5:2010LA20				PAH, PCB, Oil &		379GLBR*128-3
		ater		PAH, PCB, Oil &		379GLBR*132-1
23OCT5:2010LA2O		ater		PAH, PCB, Oil &		379GLBR*132-2
23OCT5:2010LA2O		ater		PAH, PCB, Oil &		379GLBR*132-3
25OCT3:0710LB1O		ater		PAH, PCB, Oil &		379GLBR*187-1
300CT4:206LA30		ater		PAH, PCB, Oil &		379GLBR*204-1
310CT10:129LB20	Oi			PAH, PCB, Oil &		379GLBR*226-1
310CT10:2110LB20		ater		PAH, PCB, Oil &		379GLBR*227-1
6NOV12:003LO	W	ater		PAH, PCB, Oil &	Gr	379GLBR*275-1
18NOV5:559LC1O	Oi			PAH, PCB, Oil &	Gr	379GLBR*286-1
18NOV5:559LC1O	Oi			PAH, PCB, Oil &	Gr	379GLBR*286-T1
.18NOV5:559LC1O	Oi			PAH, PCB, Oil &	Gr	379GLBR*286-T2
18NOV5:559LC1O	Oi	}		PAH, PCB, Oil &		379GLBR*286-M1
18NOV5:559LC1O	Oi			PAH, PCB, Oil &		379GLBR*286-M2
18NOV6:1510LC1O	Wa	ater		PAH, PCB, Oil &		379GLBR*287-1
19NOV5:519LC2O	Oi			PAH, PCB, Oil &		379GLBR*326-1
19NOV5:0510LC2O		ater		PAH, PCB, Oil &		379GLBR*331-T1
19NOV5:0510LC2O		ater		PAH, PCB, Oil &		379GLBR*331-T2
19NOV5:0510LC2O		ater		PAH, PCB, Oil &		379GLBR*331-M1
19NOV5:0510LC2O		ater		PAH, PCB, Oil &		379GLBR*331-M2
20NOV2:419LC3O	Oil			PAH, PCB, Oil &		379GLBR*366-1
20NOV3:0110LC3O		ater		PAH, PCB, Oil &		379GLBR*370-1
21NOV3:2610LD10		iter				
				PAH, PCB, Oil &		379GLBR*398-1
21NOV4:169LD1O	Oil			PAH, PCB, Oil &	GI	379GLBR*404-1

21NOV4:169LD1O	Oil	PAH, PCB, Oil & Gr	379GLBR*404-T1
21NOV4:169LD1O	Oil	PAH, PCB, Oil & Gr	379GLBR*404-T2
21NOV4:169LD1O	Oil	PAH, PCB, Oil & Gr	379GLBR*404-M1
21NOV4:169LD1O	Oil	PAH, PCB, Oil & Gr	379GLBR*404-M2
22NOV2:3010LD2O	Water	PAH, PCB, Oil & Gr	379GLBR*426
22NOV2:3010LD2O	Water	PAH, PCB, Oil & Gr	379GLBR*426-1
22NOV2:539LD2O	Oil	PAH, PCB, Oil & Gr	379GLBR*431
22NOV2:539LD2O	Oil -	PAH, PCB, Oil & Gr	379GLBR*431-1
25NOV4:0010LD3O	Water	PAH, PCB, Oil & Gr	379GLBR*452
25NOV4:0010LD3O	Water:	PAH, PCB, Oil & Gr	379GLBR*452-1
25NOV4:009LD3O	Oil	PAH, PCB, Oil & Gr	379GLBR*453
25NOV4:009LD3O	Oil	PAH, PCB, Oil & Gr	379GLBR*453-1
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# OIL AND GREASE

Analysis of oil and grease in water following the SOP which we received from the Large Lakes Lab was not possible. Most of the samples had a very high content of oil and fine sediment. When the sample was shaken, only one phase was apparent instead of two as described in the method. Consequently, after discussion with Eric Crecelius (program manager), the analyst allowed the sediment to settle, decanted and analyzed the liquid, and archived the sediment. Some sediment samples analyzed for oil and grease were rerun due to the formation of a drying agent residue in the extract which caused higher values. In some cases, ash passed through the filter into the extract, which caused higher values. In other cases, the replication between field replicates was not in good agreement. We wanted to ensure that the poor agreement was due to some artifact other than the methodology. If the reruns differed substantially from the original value obtained, the rerun value was reported. If the differences were slight, the original value was reported. All samples were analyzed outside the standard EPA holding time of 28 days. This was due in part to the addition of this analysis to the sampling scheme after the program was underway and partially to sample backlog in the organics laboratory. The quality of the data should not be affected since the sediments were stored at -220±50C and the water samples were stored at 40+20C prior to analysis. Matrix spikes for sediments were within the criteria outlined in the QAPP for organic samples, except for samples 379GLBR\*182 and 384 which were treated sediment. Recoveries were higher in those samples probably due to matrix interference.

#### PAHS AND PCBS

### Water

Matrix problems were evident in these samples due to high concentrations of oil. Many spike and surrogate recoveries were outside of the criteria. EPA GLNPO (Rick Fox) indicated they wanted the entire sample extracted, including the oil adhered to the sides of the bottles. When the analysts extracted the samples, they found that the methylene chloride formed an emulsion with the oily water which could not be separated out. This caused a problem in the clean-up step and apparently caused some matrix interference in the samples. Evidence for this assumption comes from spike blank recoveries, replicate RSDs and blank data, which were within the established ARCS criteria.

One method blank was extracted and analyzed for PAHs with the samples. Naphthalene and Benzo(ghi)perylene were detected at levels near detection limits in the blank. These levels were less than five times the levels found in all but three samples. The corresponding sample values for these samples were flagged with a "B" to indicate a possible bias due to blank contamination. One method

blank was extracted and analyzed for PCB Aroclors with the samples. No PCBs were detected in the method blanks.

Three stable isotopically labelled PAH compounds were added as surrogates prior to extraction to assess the efficiency of the analysis. The majority of recoveries for all three surrogates were generally below the lower QC limits (40-120%). This is mainly due to very high PAH concentrations and oily material associated with these samples. Performing an efficient extraction on these samples was very difficult. Samples with little or no PAHs had much higher surrogate recoveries, including the method blank. Due to limited sample volumes, holding times and extremely difficult sample matrices, no re-extractions were performed. Overall, PAH levels may be somewhat biased low based on the surrogate recoveries. However, the values for some of the higher weight PAH compounds are nearing their solubility limit in water and the levels quantified are more likely a function of the amount of oily material in the sample rather than a truly dissolved quantity. Two compounds, tetrachlorometaxylene (TCMX) and octachloronaphthalene (OCN) were added as surrogates to all samples prior to extraction of PCBs to assess the efficiency of the analysis. Recoveries of four samples for TCMX and OCN slightly exceeded the QC guidelines of 40-120%. All recoveries were above 20%, therefore no re-extractions were performed.

One sample was spiked in duplicate with a PAH standard (see MSL-M-42). However, the level spiked was generally five to ten times lower than the amount in the native sample. This precluded accurate determination of spike recoveries for all but one compound, benzo(k)fluoranthene, which was not present above detection limits in the native sample. Recoveries for PAHs were generally poor due to matrix interference and non-homogenous samples. In addition, spike concentrations were generally lower than the sample concentration, therefore were difficult to detect. For PCBs, one sample was spiked in duplicate with Aroclor 1254. Unfortunately, it appears that one of the two samples was not spiked after all, therefore matrix spike recoveries were only reported for one of the two samples. Aroclor 1254 spike recovery was 112% for this sample.

One sample was extracted in triplicate to assess the precision of PAH analyses. RSD values ranged from 4 to 40%. The majority of RSD values were between 20-30%, which exceeds the precision goal of 20%. These values indicate relatively good precision, considering high levels of PAHs in the samples and the difficulty of performing representative extractions on these oily, complex matrices. One sample was extracted in triplicate to assess the precision of PCB analyses. The sample analyzed contained high levels of Aroclor 1248 and needed dilution prior to quantification. The RSD value for the triplicate analyses was 41%. This exceeded the QAPP precision goal of 20%. Some error was introduced due to dilution which contributed to the higher RSD value. In addition, these water samples contained high levels of PCBs and oily material which are difficult to extract entirely from the samples. Some variability may come from non-homogenous field replicates. The combination of these factors most likely contributed to high RSD values.

Standard reference materials (SRMs) are not available for organics in water samples.

# **Sediments**

Matrix problems were evident in these samples due to high concentrations of oil. Many spike and surrogate recoveries were outside of the criteria. When the analysts extracted the samples, they found that the methylene chloride formed an emulsion with the oily water content of the sediments which could not be separated out. This caused a problem in the clean-up step and apparently caused some matrix interference in the samples. Evidence for this assumption comes from spike blank recoveries, replicate RSDs and blank data, which were within the established ARCS criteria.

Seven method blanks, one with each batch, were extracted and analyzed for PAHs. Naphthalene and Phenanthrene were detected at levels near detection limits. Sample concentrations were five times these levels in all samples but three. One method blank was extracted with each batch for PCBs. No PCBs were detected in the blanks.

our stable isotopically labelled PAH compounds were added as surrogates prior to extraction to assess the efficiency of the analyses. Recoveries of two of the surrogates d8 naphthalene and d10 acenaphthalene were occasionally low (<40%) due to their volatile nature. The surrogate d14 Dibenzo (a,h) Anthracene was detected both above and below the acceptable limit. The lower values indicate that this particular surrogate may be susceptible to degradation. We are presently replacing d14 dibenzo (a,h) anthracene with d10 pyrene in an effort to achieve better recoveries. Two compounds, tetrachlorometaxylene (TCMX) and octachloronaphthalene (OCN) were added to all samples prior to extraction for PCBs to assess the efficiency of the analyses. Recoveries for TCMX were within the QC guidelines of 40-120%, except for one sample. OCN recoveries were generally high due to underspiking, which caused difficulty in quantification of this surrogate.

Five samples and three blanks were spiked in duplicate with a PAH combined stock standard. Most samples contained much higher concentrations of PAHs than were spiked, therefore spike recoveries were usually outside the required criteria (40-120%). Matrix spikes with poor recoveries in which the spike concentration was approximately the same as the sample or higher, are probably a result of matrix interference. Matrix spikes for sample 379GLBR\*46 were not reported because the sample results were suspect from the first analysis, the sample was rerun producing very different results, but the spikes were not rerun. Spike data for the initial analysis of sample 379GLBR\*111 were not reported as the results were questionable and the sample and spikes were re-analyzed. The reruns were reported. Two samples and two method blanks were spiked in duplicate with Aroclor 1254 for PCBs. Several recoveries were slightly above the acceptable limit (40-120%). One of the blank spike recoveries was abnormally high, possibly due to an accidental duplicate spike on that sample.

Five samples were extracted in triplicate for PAHs to assess the precision of the analyses. Precision was measured by calculating the relative standard deviation (RSD) between the replicate results for each of 17 compounds. RSD values ranged from 3 to 25% for with one RSD of 52%. The majority of the RSD values were between 10 and 20%, indicating good precision. Two samples were extracted in triplicate for PCBs to assess the precision of the analyses. Sample 379GLBR\*199 did not replicate well with an RSD of 89% for the Aroclors detected, possibly due to uneven oil distribution within the sediment matrix.

The SRM generally used for sediments (NIST 1941) is not certified for PCB Aroclors or PAHs, only individual congeners. One other SRM is available and is certified for PCB Aroclor 1254, (HS-2 from NRCC), however, it was originally certified using a packed column. Our experience has shown that there is little or no 1254 pattern when capillary column GC is used. Therefore, we do not use it as a SRM for Aroclors. SRM data is reported for PAHs and compared using RSD values.

PROGRAM:

**Buffalo River Pilot Project** 

PARAMETER:

Polynuclear Aromatic Hydrocarbons (PAHs)

LABORATORY:

Twin City Testing, Inc.

MATRIX:

Air

SAMPLE NUMBER: 6

Reference
Method

Range of Recovery Relative Precision

Detection Limit

8270

40-120%

±20%

N/A

HOLDING TIMES

Not specified.

DETECTION LIMITS Detection limits were different for each sample and each compound. Detection limits ranged from 0.75 to 3.8 µg/sample. Please refer to the summary table for specific detection limits.

METHOD BLANKS

A laboratory method blank was prepared and analyzed with each sample extraction batch. The blanks were free of the target PAH analytes, with the exception of a trace background level (77 nanograms) of naphthalene. The naphthalene levels determined for the affected samples were all higher than the naphthalene level in the blank by 20 times or more. This indicates that the sample processing steps did not contribute significantly to the levels reported for the samples.

MATRIX SPIKES

The amount of material was insufficient to prepare matrix spikes. Two laboratory spike samples were prepared with the air sample batch. Spike recoveries ranged from 52-132%, which are all within the 50-135% target ranges designated for these analyses.

REPLICATES

The amount of material was insufficient for the preparation of replicates.

SRMS

SRMs are not available for PAHs in air samples.

SURROGATES

The designated range for the surrogate compounds in the PAH samples is 50-150% for at least two of the three surrogates in each sample. All the surrogate recoveries in the PAH samples fell within this range, with the exception of perdeuterated pyrene (227%) in sample 379GLBR\*112ABE. Since the remaining two surrogates in this sample were recovered at acceptable levels, the recovery criteria were met and no corrective action was required. The raw area count for the perdeuterated naphthalene internal standard in sample 379GLBR\*272ABD was 269% of the value for the corresponding standard in the daily continuing calibration analysis. THe target range for internal standard areas in the sample extracts is 50-200% of the daily continuing calibration values. Upon dilution of this sample extract, the naphthalene internal standard area fell into the acceptable range.

PROGRAM:

Buffalo River Pilot Project

PARAMETER:

Polychlorinated biphenyls (PCBs)

LABORATORY: MATRIX:

Twin City Testing, Inc.

SAMPLE NUMBER: 6

Reference Method

Range of Recovery Relative Precision

Detection Limit

680

40-120%

+20%

N/A

HOLDING TIMES

Not specified.

DETECTION LIMITS Detection limits were different for each sample and each compound. Detection limits ranged from 60 to 120 ng/sample. Please refer to the summary table for specific detection limits.

METHOD BLANKS

A laboratory method blank was prepared and analyzed with each sample extraction batch. The blanks were free of the target PCB analytes. A low recovery was achieved for the 2-Fluorobiphenyl surrogate in the PCB blank due to inadvertent volatilization of this compound during the concentration steps. Since the entire sample was consumed in the extraction process, any reprocessing was not possible. The blank associated with the impinger samples exhibited a low recovery (35%) for the perdeuterated anthracene surrogate. Since good recoveries were achieved for the other two surrogates in this blank, no corrective action was required.

MATRIX SPIKES

The amount of material was insufficient to prepare matrix spikes. Two laboratory spike samples were prepared with each batch. Spiked native compounds were recovered at levels ranging from 52-132%, which are all within the 50-135% target ranges designated for these analytes.

REPLICATES

The amount of material was insufficient for preparation of replicates.

SRMS

SRMs are not available for PCBs in air samples.

SURROGATES

The recoveries of the surrogate compounds fell within the 50-125% guidelines specified in Method 680, with the exception of the 2-Fluorobiphenyl recovery (47%) in sample 379GLBR\*112F.

PROGRAM:

**Buffalo River Pilot Project** 

PARAMETER:

Dioxins/furans

LABORATORY:

Twin City Testing, Inc.

MATRIX:

Air

SAMPLE NUMBER: 6

Reference

Range of

Relative

Detection

Method

Recovery

Precision

Limit

**EPA Method 23** 

Not specified

Not specified

Not specified

HOLDING TIMES

Not specified.

DETECTION LIMITS Detection limits were different for each sample and each compound. Generally, they varied from 0.013 to 0.140 ng/sample. Please refer to the summary table for specific detection limits.

METHOD BLANKS

One laboratory method blank was prepared and analyzed with the sample extraction batch. The blanks were free of dioxins and furans, with the exception of trace background levels of PeCDD (19 picograms), HpCDD (6.3 picograms) and OCDD (92 picograms). The levels determined for the affected isomers in the actual samples were higher than the corresponding blank levels by 3-100 times. It should be noted, however, that levels less than five times higher than the background are not generally considered statistically different from the background.

MATRIX SPIKES

The amount of sample material was insufficient to prepare matrix spikes. Two quality control dioxin/furan spike samples were prepared with the sample batch. The data show that the spiked native compounds were recovered at levels ranging typically from 87-130%. The only compound with recoveries outside of this range was 1,2,3,4,7,8,9-HpCDF, which exhibited a recovery of 160% in each of the spike samples. It should be noted, that quality control ranges for native spike sample recoveries are not specified in the method.

REPLICATES

The amount of sample material was insufficient for the preparation of replicates.

SRMS

SRMS are not available for dioxin/furans in air samples.

SURROGATES

The recoveries of the isotopically-labeled dioxin/furan internal and surrogate standards generally ranged from 70-130%. All the recoveries were within the target ranges specified in the method, with the exceptions of the labeled 1.2.3.7.8-PeCDD in samples 379GLBR\*112F (37%), 379GLBR\*272ABD (37%), and the lab spike duplicate (36%). Slightly elevated recoveries were obtained for selected surrogate compounds in samples 379GLBR\*233ABD (labeled 1,2,3,4,7,8-HxCDD, 145%), 379GLBR\*272ABD (labeled 1,2,3,4,7,8-HxCDD, 148%), the laboratory spike (labeled 1,2,3,4,7,8,9-HpCDF, 135%), and the laboratory spike duplicate (labeled 1,2,3,4,7,8,9-HpCDF, 135%). The native 1,2,3,7,8-PeCDD concentrations should be accurate for these samples since

quantitation is based on isotope dilution. The native 1,2,3,4,7,8-HxCDD and 1,2,3,4,7,8,9-HpCDF concentrations in these four samples may, however, be slightly elevated since both the native and surrogate isomers are compared to a separate labeled isomer.

PROGRAM:

**Buffalo River Pilot Project** 

PARAMETER:

Oil and grease

LABORATORY:

Battelle Marine Science Laboratories

MATRIX:

Water

SAMPLE NUMBER: 23

Reference Method

Range of Recovery

Relative Precision

Detection Limit

5520B

70-130%

±20%

Not specified

HOLDING TIMES

Not specified.

DETECTION LIMITS The detection limit for this method was determined to be 1.1 mg/L.

METHOD BLANKS

Eight method blanks were prepared and analyzed, at least one with each batch

extracted. Oil and grease was less than the detection limit in all blanks.

MATRIX SPIKES

Not required by the QAPP. Two samples were spiked in duplicate with a known concentration of pump oil. Recoveries ranged from 95 to 134%. Laboratory spike blanks (not required) were prepared and analyzed with recoveries

ranging from 76 to 78%.

REPLICATES

Two samples were extracted and analyzed in triplicate. Relative standard

deviations were 3 and 17%.

SRMS

SRMs are not available for oil and grease.

PROGRAM:

**Buffalo River Pilot Project** 

PARAMETER:

Oil and grease

LABORATORY:

Battelle Marine Science Laboratories

MATRIX:

Sediment

SAMPLE NUMBER: 97

Reference

Range of

Relative

Detection

Method

Recovery

Precision

Limit

**EPA-LLRS-GROSSE** 

70-130%

+20%

N/A

HOLDING TIME

Not specified.

DETECTION LIMIT

The detection limit was determined as 630  $\mu$ g/g.

METHOD BLANKS

Nine blanks were prepared and analyzed; at least one with each batch. Oil and

grease was not detected in any of the blanks.

MATRIX SPIKES

Not required in the QAPP. Five matrix spikes in duplicate were spiked with pump oil, one with each batch. All recoveries were within 70-130%, with the exception of 379GLBR\*182 and 379GLBR\*384, where recoveries ranged from 142 to 158%. These two samples were ash material which possibly caused some matrix interference in this method. Laboratory blank spikes were prepared and analyzed, with recoveries ranging from 87 to 115%.

**REPLICATES** 

Five samples were extracted and analyzed in triplicate; at least one per batch. All triplicates were within the range of precision, with the exception of

All triplicates were within the range of precision, with the exception of 379GLBR\*111 and 379GLBR\*384. Both samples replicated with a RSD of 22%, possibly caused by a residue from dissolution of sodium sulfate (drying agent) when mixed with the sediment that passed through the filtration step into

the extract.

SRMS

SRMs are not available for oil and grease.

PROGRAM:

**Buffalo River Pilot Project** 

PARAMETER:

Polynuclear Aromatic Hydrocarbons (PAHs)

LABORATORY:

Battelle Marine Science Laboratories

MATRIX:

Water

SAMPLE NUMBER: 23

Reference Method

Range of Recovery Relative Precision Detection Limit

MSL-M-41

40-120%

+20%

0.02µg/L

HOLDING TIME

Holding times for extraction were exceeded for all samples by approximately 60 days. However, all samples were stored at 4°C preventing biodegradation of the samples. All samples were analyzed within 40 days of extraction, which meets the established criteria.

DETECTION LIMITS Detection limits ranged from 0.007 to 0.07 µg/L. The higher detection limits were associated with samples requiring dilution or those with high PAH concentrations that required smaller extraction volumes.

METHOD BLANKS

One method blank was analyzed with the samples. The blank was free of PAH compounds except Naphthalene and benzo(ghi)perviene were detected at levels near detection limits in the blank. These levels were less than five times the levels found in all but three samples. Surrogate recoveries in the blanks ranged from 61 to 67%.

MATRIX SPIKES

One sample was spiked in duplicate for PAHs. The matrix spike recoveries were all negative percentages except for Benzo(a)anthracene (2026%), benzo(k)fluoranthene (84%) and dibenzo(a,h)anthracene (4%). The concentration of the spike was generally much lower than the sample concentration, causing difficulty in detecting the spike signal. The spike duplicate showed recoveries ranging from 3 to 197% with a negative recovery for benzo(b)fluoranthene. This indicates some matrix interference.

REPLICATES

One sample was extracted and analyzed in triplicate. Relative standard deviations were generally between 25 and 35%. Dibenzo(a,h)anthracene RSD was 47%. Naphthalene, acenaphthalene and acenaphthene had RSDs below 20%, which is within the established criteria.

SRMS

SRMs are not available for PAHs in water.

SURROGATES

Most surrogates were outside the established criteria, probably due to matrix interference and high sample concentrations relative to surrogate

concentrations used.

PROGRAM:

**Buffalo River Pilot Project** 

PARAMETER: LABORATORY: Polychlorinated biphenyls (PCBs) Battelle Marine Science Laboratories

MATRIX:

Water

SAMPLE NUMBER: 23

Reference Method

Range of Recovery

Relative Precision Detection Limit

MSL-M-41

40-120%

+20%

0.01µg/L

HOLDING TIME

Holding times for extraction were exceeded for all samples by approximately 60 days. However, all samples were stored at 4°C preventing biodegradation of the samples. All samples were analyzed within 40 days of extraction, which meets the established criteria.

DETECTION LIMITS The detection limits ranged from 0.05μg/L to 0.2 μg/L for undiluted samples and from 0.5µg/L to 2µg/L for diluted samples.

METHOD BLANK

One method blank was prepared and analyzed with the samples. No PCBs were detected in the blank. Surrogate recoveries were 62 and 96% in the blank.

MATRIX SPIKE

One matrix spike was prepared and analyzed with the samples for Aroclor 1254. The recovery was 112% and the surrogate recoveries were 44 and 50%. A duplicate spike was set up but was not spiked.

REPLICATES

One sample was extracted and analyzed in triplicate with an RSD of 41%.

SURROGATES

Most samples were within the criteria for surrogate recovery of 40 to 120%. Seven of 23 samples had one surrogate recovery outside the required criteria. Both surrogate recoveries for 1 sample were below the required criteria.

PROGRAM:

**Buffalo River Pilot Project** 

PARAMETER:

Polynuclear Aromatic Hydrocarbons (PAHs)

LABORATORY:

Battelle Marine Science Laboratories

MATRIX:

Sediments

SAMPLE NUMBER: 97

Reference Method

Range of Recovery

Relative Precision

Detection Limit

MSL-M-42

40-120%

±20%

0.02μg/Kg

HOLDING TIMES

Samples were held frozen up to 3 months prior to extraction and most were analyzed within the EPA extract holding time of 40 days (EPA 1986).

DETECTION LIMITS Detection limits ranged from 0.004 to 0.053 μg/g.

METHOD BLANKS

Seven method blanks were extracted and analyzed for PAHs; one with each batch of samples. PAHs were not detected in the blanks.

MATRIX SPIKES

Eight samples were spiked in duplicate with a known concentration of PAH standard. One sample had suspect results and was re-analyzed. However, the spikes were not re-analyzed with it, therefore, that data has not been included. A second sample had suspect results and was rerun along with the spikes. The rerun results were reasonable and have been included in the data package. For the 17 PAH compounds analyzed, spike 379GLBR\*111 had recoveries within the 40-120% criteria and the duplicate spike had 4 compounds within the criteria. The spike 379GLBR\*247 had 12 of 17 and the duplicate had 10 of 17 compounds within the. Both the spike 379GLBR\*247 (rerun) and the duplicate had 14 of 17 compounds within the criteria. The spike 379GLBR\*268 had 8 of 17 and the duplicate had 16 of 17 compounds within the criteria. Both the spike 379GLBR\*388 and the duplicate had 12 of 17 compounds within the criteria. The spike 379GLBR\*388 (rerun) had 14 of 17 and the duplicate had 13 of 17 compounds within the criteria.

SRMs

SRMs certified for PAHs in sediments are not available.

REPLICATES

Five samples were extracted and analyzed in triplicate. Of those triplicates, one had 17 of 17 compounds within the  $\pm 20$  criteria, two had 14 of 17 and two had 11 of 17 within the criteria. Those compounds with higher RSDs were

associated with low concentrations near the detection limits.

SURROGATES

Four surrogates were added to all samples. Of the 97 samples analyzed, 41 had one surrogate outside the recovery criteria of 40-120%, 8 had two surrogates outside the criteria and 2 had three surrogates outside the criteria.

PROGRAM:

**Buffalo River Pilot Project** 

PARAMETER: LABORATORY:

Polychlorinated biphenyls (PCBs)
Battelle Marine Science Laboratories

MATRIX:

Sediments

SAMPLE NUMBER: 46

Seament

Reference Method Range of Recovery

Relative <u>Precision</u> Detection Limit

MSL-M-42

40-120%

±20%

 $0.02\mu g/Kg$ 

**HOLDING TIMES** 

Samples were held frozen for up to 3 months prior to extraction and were most were analyzed within the EPA extract holding time of 40 days (EPA 1986).

**DETECTION LIMITS** 

Detection limits ranged from 0.025 to 0.060µg/Kg.

METHOD BLANKS

One method blank was extracted and analyzed with each batch. No PCBs were

detected in the blanks.

MATRIX SPIKES

One sample was spiked with Aroclor 1254. Four samples were spiked in duplicate with Aroclor 1254. Three of the seven recoveries were within the criteria of 40-120%.

**SRMs** 

Only one SRM is certified for PCBs in sediments, which is HS-2 from the National Research Council of Canada. However, only Aroclor 1254 is certified for packed column chromatography. We used capillary column chromatography. Therefore, no certified SRMs are available for PCBs in sediment using the method we follow.

REPLICATES

Two samples were extracted and analyzed in triplicate. Sample 379GLBR\*199 had an RSD for Aroclor 1254 of 89%, and an RPD of 117% for Aroclor 1248. The second replicate, 379GLBR\*323 had RSDs within the criteria for all compounds.

**SURROGATES** 

Two surrogates were added to each sample. Thirty-three of 46 samples had one surrogate outside the criteria of 40-120%. Thirty-two of those 33 samples were outside the criteria because the amount of surrogate octachloronaphthalene added was too low relative to the sample concentrations and was difficult to resolve.

BUFFALO RIVER PILOT PROJECT (CF# 379) DOXINS/FURANS IN AIR SAMPLES

(Concentrations in ng/sample)	ng/sample)													
		2378-	TOTAL	2378-	TOTAL	1	23478-	TOTAL	12378-	TOTAL		123678-	123789.	_
MSL Code	Sponsor ID	TCDF	TCDF	TCDO	TCDO	PeCDF	PeCDF	PecDF	PeCDO	PeCDF	PeCDF HxCDF	HXCDF	HXCDF	
20000	OF CAROLITACION	-	9	•	;									,
3/80LDH-112ADE		0.086	0.100	0.0/9 C	۷ ۲	0.033	0.056 U	0.380	0.330	0.320	0.042	0.053	0.110	
379GLBR-112F		0.057	0.260	0.027 U	N N	0.031	0.048	0.400	0.023 U	0.150	0.043	0.046	0.140	
379GLBR-232ABD		0.037	0.480	0.036	0.290	0.040	0.056	0.530	0.079	0.670	0.078	0.076	0.150	
379GLBR-233ABD	24OCT5:3011GA3O	0.000	0.830	0.041	0.400	0.057	0.087	1.200	0.086	0.770	0.140 U	0.130	0.220	
379GLBR-234ABD	250CT1:4511GB10	0.059	1.100	0.021	0.210	0.055	0.063	0.840	0.036 U	0.490	0.048	0.054	0.043	
379GLBR-272ABD	379GLBR-272ABD 31OCT1:0011GB3O	0.380	3.800	0.089	1.100	0.360	0.340	3.700	0.180 U	2.600	0.390	0.330	0.230	
Method Blank	Method Blank	0.0260 U	Y Y	0.0530 U	¥ V	0.0120 U	0.0082 U	¥.	0.0110 U	Y Y	0.0076 U	0.0094 U	0.0058 U	
MATRIX SPIKE RESULTS	SULTS											•		
Spike													•	
Quantity Spiked		0.200	0.200	0.200	0.200	1.000	1.000	2.000	1.000	1.000	1.000	1,000	1,000	
Quantity Measured		0.230	0.230	0.250	0.250	1.100	1.100	2.200	1.100	1.100	0.970	0.890	0.870	
Percent Recovery		115%	115%	125%	125%	110%	110%	110%	110%	110%	%16	89%	87%	
Spike Duplicate														
Quantity Spiked		0.200	0.200	0.200	0.200	1.000	1.000	2.000	1.000	1.000	1.000	1.000	1,000	
Quantity Measured		0.240	0.240	0.240	0.240	1.100	1.200	2.300	1.100	1.100	0.960	0.930	0.930	
Percent Recovery		120%	120%	120%	120%	110%	120%	115%	110%	110%	<b>%</b> 96	<b>%</b> 26	83%	

NA = Not applicable.
\* - Outside of Internal QC criteria (40-120%).

Technical Control   Cont	ations in	(Concentrations in ng/sample)	024670	TOTAL		02000	001001	, is a contract of	0100	001	, , , , ,				
1.000 4.000 1.000		9	2346/8-	2 S	1234/8- 1	-8/957	-68/821	וסואר.	2346/8-	1234/89-	IOIAL I	234678-	TOTAL		
0.042 0.560 0.056 0.091 0.130 1.500 0.510 0.100 0.710 1.600 3.300 1.300 0.042 0.590 0.0013 U 0.022 0.011 U 0.100 0.620 0.120 1.200 0.210 0.390 1.600 0.028 0.890 0.031 0.050 0.025 0.660 0.750 0.110 1.100 0.490 0.031 0.050 0.025 0.660 0.750 0.110 1.000 0.780 2.300 1.000 0.023 U 0.440 0.026 U 0.038 U 0.020 0.490 0.250 0.010 1.900 0.780 2.300 1.600 0.023 U 0.440 0.026 U 0.038 U 0.020 0.490 0.250 0.010 1.900 0.790 0.790 0.790 0.790 0.790 0.790 0.010 0.000 0	Sponso	2	HCD+	Ž Ž Ž	ACDO H	CDOX 1	HCD0	9 2 2 2 2 2	호	HPCDF	100g	HOCDO	000 <del>1</del>	8	8
0.042 0.590 0.013 U 0.022 0.011 U 0.100 0.650 0.120 1.200 0.210 0.200 1.000 0.028 0.890 0.031 0.050 0.025 0.011 U 0.100 0.750 0.110 1.100 0.250 0.031 0.050 0.025 0.001 1.200 0.120 0.100 0.250 0.025 0.010 1.200 0.039 0.001 0.002 0.001 0.000 1.200 0.120 0.110 1.900 0.250 0.020 0.090 1.000 0.002	220C	T5:0011GA10	0.076 U	0.560	0.050		0 130	1 500	0.510	0 100	0 710	1 600	000	7	4
1.000 4.000 1.000 1.000 1.000 3.000 1.000 1.000 2.000 1.000		TS-0011GA10	0.040	0090	0 0 1 2 1		1 1 1 1	2	9 6 9			9 6	900	5 6	9.60
15:3011GA2O 0.028 0.890 0.031 0.050 0.025 0.660 0.750 0.110 1.100 0.450 0.900 1.000 T5:3011GA2O 0.054 1.100 0.049 0.071 0.050 1.000 1.200 0.180 1.900 0.780 2.300 1.600 T1:4511GB1O 0.023 U 0.440 0.026 U 0.038 U 0.020 0.490 0.250 0.023 0.410 0.260 0.680 0.160 T1:4511GB1O 0.023 U 0.440 0.0120 0.130 0.110 2.900 1.600 0.110 1.900 0.780 2.300 1.600 T1:4511GB1O 0.023 U 0.440 0.026 U 0.039 U 0.020 0.049 0.250 0.010 1.900 0.110 1.900 0.150 0.010 T1:4511GB1O 0.023 U 0.044 2.800 0.120 0.130 0.110 2.900 1.000 0.010 1.900 1.000 1.000 1.000 0.050 T1:4511GB1O 0.024 2.800 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 2.000 1.000 0.970 0.970 2.300 T1:4511GB1O 0.024 2.800 1.000 1		מועסווסיים	0.046	0.00	20.0			3	0.020	0.120	1.200	0.210	0.390	1.600	0.910
Ti-3011GA3O 0.054 1.100 0.049 0.071 0.050 1.000 1.200 0.180 1.900 0.790 2.300 1.600 Ti-4511GB1O 0.023 U 0.440 0.026 U 0.038 U 0.020 0.490 0.250 0.023 0.410 0.260 0.680 0.160 Ti-4511GB1O 0.023 U 0.440 0.026 U 0.038 U 0.020 0.490 0.250 0.023 0.410 0.260 0.680 0.160 Ti-4511GB1O 0.023 U 0.440 0.026 U 0.038 U 0.020 0.490 0.100 1.600 0.110 1.900 1.500 1.500 0.650 Ti-4511GB1O 0.023 U 0.044 2.800 0.030 U 0.0120 U NA 0.0190 U 0.0077 U NA NA 0.0210 Ti-4511GB1O 0.023 U 0.0083 U 0.0097 U 0.0120 U NA 0.0190 U 0.0077 U NA NA 0.0210 Ti-4511GB1O 0.023 U 0.0083 U 0.0097 U 0.0120 U NA 0.0190 U 0.0077 U NA NA 0.0210 Ti-4511GB1O 0.023 U 0.0097 U 0.0120 U NA 0.0190 U 0.0077 U NA NA NA 0.0210 Ti-4511GB1O 0.023 U 0.0097 U 0.0120 U NA 0.0190 U 0.0077 U NA NA NA 0.0210 Ti-4511GB1O 0.023 U 0.0097 U 0.009 U 0.000	2300	T4:4511GA20	0.028	0.890	0.031		0.025	0.660	0.750	0.110	1.100	0.450	0.900	1.000	1.600
T1:4511GB1O 0.023 U 0.440 0.026 U 0.038 U 0.020 0.490 0.250 0.023 0.410 0.260 0.680 0.160 T1:0011GB3O 0.044 2.800 0.120 0.130 0.110 2.900 1.600 0.110 1.900 1.500 0.050  d Blank 0.0077 U NA 0.0083 U 0.0097 U 0.0120 U NA 0.0190 U 0.0077 U NA NA NA 0.0210  1.000 4.000 1.000 1.000 1.000 1.000 1.000 1.100 0.100 1.000 1.000 1.000 1.100 0.97	2 <del>4</del> 00	T5:3011GA3O	0.054	1.100	0.049		0.050	1.000	1.200	0.180	1.900	0.780	2.300	1.600	3.000
T1:0011GB3O 0.044 2.800 0.120 0.130 0.110 2.900 1.600 0.110 1.900 1.500 4.000 0.0031 U 0.0097 U 0.0120 U NA 0.0190 U 0.0077 U NA NA 0.0210	2500	T1:4511GB10	0.023 U	0.440	0.026 U	0.038	0.020	0.490	0.250	0.023	0.410	0.260	0.680	0.160	1.300
1.000 4.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 2.000 1.000 2.000 1.000 2.000 1.000 2.000 1.000	300	T1:0011GB3O	0.044	2.800	0.120	0.130	0.110	2.900	1.600	0.110	1.900	1.500	4.000	0.650	4.900
1.000       4.000       1.000       1.000       1.000       1.000       1.000       1.000       1.000       2.000       1.000       2.000         0.980       3.700       1.200       1.200       1.200       1.200       1.200       0.970       0.970       2.300         98%       93%       120%       120%       123%       110%       160%       155%       97%       115%         1.000       4.000       1.000       1.000       1.000       1.000       1.000       1.000       1.000       2.000         1.000       3.800       1.200       0.990       0.990       3.200       1.200       1.60%       1.100       1.100       1.100       2.400         100%       85%       120%       99%       107%       120%       140%       110%       110%       120%	Meth	od Blank	0.0077 U	Š	0.0083 U	0.0097 L		<b>A</b> N	0.0190			NA :	N A	0.0210	X A
4.000       1.000       1.000       1.000       1.000       1.000       1.000       1.000       1.000       1.000       2.000       1.000       2.000       1.000       2.000       1.000       2.000       1.000       2.000       2.000       1.000       2.000       1.000       2.000       1.000       2.000       1.000       2.000       1.000       2.000 <td< td=""><td>MATRIX SPIKE RESULTS</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>•</td><td></td><td></td></td<>	MATRIX SPIKE RESULTS												•		
4.000       1.000       1.000       1.000       1.000       1.000       1.000       2.000       1.000       2.000         3.700       1.200       1.200       1.200       1.200       1.100       1.100       0.970       0.970       2.300         83%       120%       120%       123%       110%       160%       135%       97%       97%       115%         4.000       1.000       1.000       1.000       1.000       1.000       1.000       2.000         3.800       1.200       0.990       0.990       1.200       1.200       1.100       1.100       1.100       2.400         95%       120%       99%       107%       120%       160%       140%       110%       110%       120%															
3.700 1.200 1.300 1.200 3.700 1.100 1.600 2.700 0.970 0.970 2.300 83% 120% 130% 120% 120% 120% 1000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 2.000 1.000 2.000 3.800 1.200 0.990 0.990 3.200 1.200 1.600 2.800 1.100 1.100 2.400 85% 120% 99% 99% 107% 120% 160% 140% 110% 110% 120%			1.000	4.000	1.000	1.000	1.000	3.000	1.000	1.000	2,000	1 000	1 000	0000	000
93%       120%       130%       120%       123%       110%       160%       135%       97%       97%       115%         4.000       1.000       1.000       1.000       1.000       1.000       1.000       1.000       2.000         3.800       1.200       0.990       0.990       3.200       1.200       1.600       2.800       1.100       1.100       2.400         95%       120%       99%       99%       107%       120%       140%       110%       110%       120%			0.980	3.700	1.200	1.300	1.200	3.700	1.100	1.600	2.700	0.970	0.970	2300	2 100
4.000 1.000 1.000 1.000 3.000 1.000 1.000 2.000 1.000 1.000 2.000 3.800 1.200 0.890 0.890 3.200 1.200 1.600 2.800 1.100 1.100 1.100 2.400 85% 120% 89% 107% 120% 120% 110% 110% 120%			%86	83%	120%	130%	. 120%	123%	. 110%	160%	135%	%16	%26	115%	105%
4.000         1.000         1.000         1.000         1.000         1.000         1.000         2.000         1.000         2.000           3.800         1.200         0.990         0.990         3.200         1.200         1.600         2.800         1.100         1.100         1.100         2.400           95%         120%         99%         89%         107%         120%         140%         110%         110%         120%		**. **********************************													
3.800 1.200 0.990 0.990 3.200 1.200 1.600 2.800 1.100 1.100 2.400 95% 120% 99% 99% 107% 120% 160% 140% 110% 110% 120%			1.000	4.000	1.000	1.000	1.000	3.000	1.000	1.000	2.000	1.000	1.000	2.000	2.000
95% 120% 99% 99% 107% 120% 160% 140% 110% 110% 120%			1.000	3.800	1.200	0.890	0.890	3.200	1.200	1.600	2.800	1.100	1.100	2.400	2.100
			100%	82%	120%	<b>%</b> 66	<b>%</b> 68	107%	120%	160%	140%	110%	110%	120%	105%

NA = Not applicable.
• = Outside of Internal QC criteria (40-120%).

BUFFALO RIVER PILOT PROJECT (CF# 379) DOXINS/FURANS IN AIR SAMPLÉS

INTERNAL STANDARDS

% Весоину												
		2378-	2378-	12378-	23478-	12378-	123478-	123678-	123789-	234678-	12378- 123478- 123678- 123789- 234678- 123478-	123678-
		<b>1</b> 00	70 00 00 00 00 00 00 00 00 00 00 00 00 0	PecDF	Pecor	Pecco	FACDE	HACDF	<b>FCDF</b>	<b>F</b> CDF	HKCDO	HXCDD
MSL Code	Sponsor ID	-C13	-C13	-C13	-C13	-C13	-C13	-C13	-C13	-C13	-C13	-C13
379GLBR-112ABE	379GLBR-112ABE 22OCT5:0011GA10	92	6	7.0	8	99	106	83	Z	N N	122	72
379GLBR-112F	22OCT5:0011GA10	78	73	63	Ä	37	₹	86	¥	NA	Y Y	80
379GLBR-232ABD	230CT4:4511GA20	66	88	73	111	42	93	93	¥	Ä	115	83
379GLBR-233ABD	24OCT5:3011GA3O	104	101	79	103	62	69	102	¥	¥	145	83
379GLBR-234ABD	250CT1:4511GB10	78	77	61	113	4	98	79	₹	¥	115	73
379GLBR-272ABD	379GLBR-272ABD 31OCT1:0011GB3O	88	88	68	100	37	68	88	¥.	A A	148	73
Method Blank	Method Blank	82	80	73	124	57	96	92	X Y	N	120	77
MATRIX SPIKE RESULTS	SULTS											•
Spike Dunicate	(% Recovery)	181	4 6	77	103	46	40	80 0	¥ S	¥ S	130	72
and and		2	;	3	<b>P</b>	9	<b>D</b>	70	Ž	<b>≦</b>	90-	0

NA = Not applicable.
• = Outside of internal QC criteria (40-120%).

BUFFALO RIVER PILOT PROJECT (CF# 379) DOXINS/FURANS IN AIR SAMPLES

% Весоиелу								
		234678-	1234789-1234678	34678-		1234.	123789-	2378.
		FOD!	HPCDF HPCDD	Hocoo	88	<b>1</b> C00	HXCDD	TCDD
MSL Code	Sponsor ID	-C13	-C13	-C13	-C13	C13	-C13	-C13

		1234678	1234678- 1234789-1234678-	234678-		1234.	123789.	2378.	
		HPCDF	HOCDF	H <del>C</del> C00	88	<b>1</b> CD0	HXCDD	TCDD	
MSL Code	Sponsor ID	-C13	-C13	-C13	-C13	-C13	-C13	-C13	
379GLBR-112ABE	220CT5:0011GA10	77	119	87	102	₹	¥.	100	
379GLBR-112F	220CT5:0011GA10	69	AN .	73	61	₹	¥.	¥	
379GLBR-232ABD	230CT4:4511GA20	74		83	83	¥	¥	<b>6</b> 6	
379GLBR-233ABD	24OCT5:3011GA3O	82		91	95	¥	ž	101	
379GLBR-234ABD	250CT1:4511GB10	99	•	73	29	≨	Y Z	66	
379GLBR-272ABD	31OCT1:0011GB3O	70	•	9/	74	ş	Y Y	96	
Method Blank	Method Blank	76	105	72	59	¥	¥ Z	100	
METHOD BLANK RESULTS	ESULTS								
Spike Spike Duplicate	(% Recovery) (% Recovery)	53	135	77	67	<b>3 3</b>	¥ ×	93	
•					,	•	<b>§</b>	2	

NA = Not applicable.
• a Outside of internal QC criteria (40-120%).

# BUFFALO RIVER PILOT PROJECT (#379) SIR/PAH ANALYSIS IN AIR SAMPLES

MATRIX: XAD		(Concentrations in ng/sample)	s in ng/sam			3			
MSL Code	Sponsor ID	Naph- thalene	Acenaph- thylene	Acenaph- thene	Flourene	Phenan- threne	Anthra-	Fluoran- thene	Pyrene
379GLBR-112AB 379GLBR-232AB 379GLBR-233AB 379GLBR-234AB 379GLBR-272AB	379GLBR-112ABE 22OCT5:0011GA10 379GLBR-232ABD 23OCT4:4511GA2O 379GLBR-233ABD 24OCT5:3011GA3O 379GLBR-234ABD 25OCT1:4511G31O 379GLBR-272ABD 31OCT1:0011GB3O	155261 BD(1) 19086 BD(2) 13944 BD(2) 8922 BD(2) 111623 BD(1)	7529 D 82 168 187 541 D	14897 D(1) 305 414 478 1663 D	6766 D 448 470 854 3841 D	51605 D(1) 3568 D(2) 4044 D(2) 3743 D(2) 44750 D(1)	5492 D 330 477 813 4423 D	12605 D 1289 1650 1779 D(2)	22876 D(1) 728 1296 2691 11945 D
Method Blank-XAD	Q	11	n 09	0 0 0	009	n 09	0 0 9	009	n 09
MATRIX SPIKE RESULTS	TESULTS								
Amount Spiked Method Blank Blank + Spike Amount Recovered Percent Recovery		1500 77 1137 1060 71%	1500 60 U 1097 1097 73%	1500 60 U 1395 1395 93%	1500 60 U 1154 1154 77%	1500 60 U 1159 1159	1500 60 U 957 957 64%	1500 60 U 1381 1381 92%	1500 60 u 1211 1211 81%
Amount Spiked Method Blank Blank + Spike Duplicate Amount Recovered Percent Recovery	uplicate *d *d	1500 77 1573 1496 100%	1500 60 U 1401 1401 93%	1500 60 U 1973 1973 132% •	1500 60 U 1662 1662 111%	1500 60 U 1615 1615	1500 60 U 1324 1324 88%	1500 60 U 1962 1962	1500 60 U 1689 1689

<sup># =</sup> All benzofluoranthene isomers (b, j & k) are quantified together D(2) = Secondary analysis performed at dilution factor of 1:20 D(1) - Third analysis performed at dilution factor of 1:100 B = Analyte was also detected in the associated blank
D = Secondary analysis performed at dilution factor of 1:5 U = Undetected at the given method detection limit
• Outside EPA and internal QC criteria (40-120%).

# BUFFALO RIVER PILOT PROJECT (#379) SIR/PAH ANALYSIS IN AIR SAMPLES

in na/samole)	
(Concentrations	
MATRIX: XAD	

MSL Code	Sponsor ID	Benz[a]- anthracene	Chrysene	Benzofluor- anthenes #	Benzo[a]- pyrene	Indeno [1,2,3-cd]- pyrene	Dibenz[a,h]- anthracene	Benzo[ghi] perylene
379GLBR-112ABE	22OCT5:0011GA10	54520 D	5370 D	260 <b>6</b> D	2956 D	7110	0 999 0	31180
379GLBR-232ABD	230CT4:4511GA20		159	313	69	0 09	09 n	77
379GLBR-233ABD	24OCT5:3011GA3O	268	286	363	124	64	0 09	26
379GLBR-234ABD	250CT1:4511GB10		669	839	223	214	09 n	121
379GLBR-272ABD	310CT1:0011GB30	50110	3629 D	6656 D	805 D	1234 D	009	434 D
Method Blank-XAD		0 0 0 n	09 n	120 u	<b>n</b> 09	n 09	n 09	09
MATRIX SPIKE RESULTS	OULTS							
Amount Spiked		1500	1500	1500	1500	1500	1500	1500
Method Blank		0 0 0	09	120 U	009	09	n 09	
Blank + Spike		1225	1153	2611	804	1292	1331	
Amount Recovered		1225	1153	2611	804	1292	1331	
Percent Recovery		<b>8</b> 5%	<b>4</b>	87%	54%	86%	<b>%68</b>	81%
Amount Spiked		1500	1500	1500	1500	1500	1500	1500
Method Blank		0 0 9	0 0 O	120 U	0 09	09	0 09	n 09
Blank + Spike Duplicate	icate	1708	1579	3749	1000	1812	1852	1678
Amount Recovered		1708	1579	3749	1000	1812	1852	1678
Percent Recovery		114%	105%	125%	%29	121%	123%	112%

<sup># =</sup> All benzofluoranthene isomers (b, j & k) are quantified together B = Analyte was also detected in the associated blank

Page 2

D - Secondary analysis performed at dilution factor of 1:5

D(1) - Third analysis performed at dilution factor of 1:100

D(2) = Secondary analysis performed at dilution factor of 1:20 U = Undetected at the given method detection limit
• • Outside EPA and Internal QC criteria (40-120%).

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### BUFFALO RIVER PILOT PROJECT (#379) SIRVPAH ANALYSIS IN AIR SAMPLES

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		%	% Surrogate Recovery		
		D10-	D10-	D10-	
MSL Code	Sponsor ID	Fluorene	Anthracene	Pyrene	
379GLBR-112A	379GLBR-112ABE 22OCT5:0011GA10	162% D	107% D	204% D •	
379GLBR-232A	379GLBR-232ABD 23OCT4:4511GA2O	%09	<b>%</b> 99	<b>65%</b>	
379GLBR-233A	379GLBR-233ABD 24OCT5:3011GA3O	28%	63%	%19	
379GLBR-234	379GLBR-234ABD 25OCT1:4511GB1O	108%	113%	116%	
379GLBR-272/	379GLBR-272ABD 31OCT1:0011GB3O	94% D	101% D	111% D	
Method Blank-XAD	(AD	103%	79%	109%	
MATRIX SPIKE RESULTS	: RESULTS		•		
Amount Spiked		₹	¥	₹	
Method Blank		103%	79%	109%	
Blank + Spike		71%	<b>63%</b>	<b>%98</b>	
Amount Recovered	ered	¥	₹	<b>≨</b>	
Percent Recovery	өгу	¥	¥	¥	
Amount Spiked		<b>V</b>	Ą	<b>4</b> 2	
Method Blank		103%	79%	109%	
Blank + Spike	Spike Duplicate	107%	87%	120%	
Amount Recovered	peae	¥	¥	\$	
Percent Recovery	өгу	¥	<b>≨</b>	<b>*</b>	

# = All benzolluoranthene isomers (b, j & k) are quantified together

B = Analyte was also detected in the associated blank
D = Secondary analysis performed at dilution factor of 1:5

D(2) - Secondary analysis performed at dilution factor of 1:20 D(1) - Third analysis performed at dilution factor of 1:100

U = Undetected at the given method detection limit
• - Outside EPA and internal QC criteria (40-120%).

MATRIX: WATER		(Concentration	(Concentrations in ng/L)							ſ
MSL Code	Sponsor ID	Naph- thatene	Acenaph- thylene	Acenaph-	Flourene	Phenan- threne	Anthra-	Fluoran- thene	Pyrene	
379GLBR-112CD	22OCT5:0011GA10	299	41	103	123	2975 D	233	1433 0	4602 D	1
379GLBR-232C	230CT4:4511GA20	80	45 U	45 U	45 U	61	45 U	45 U	46	
379GLBR-233C	24OCT5:3011GA30	56	50 u	50 C	50 u	55	50 U	50 U	55	
379GLBR-234C	250CT1:4511GB10	92	57 U	57 U	57 U	96	57 U	187	186	
379GLBR-272C	31OCT1:0011GB3O	6	74 U	740	74 U	74 U	74 U	740	74 U	
Method Blank-WATER	TEA	20 U	20 U	20 U	20 U	20 U	20 U	20 U	20 U	
MATRIX: SOLVENT BLANK	IT BLANK	(Concentrati	(Concentrations in ng/L)					•		

# - All benzofluoranthene isomers (b, j & k) are quantified together

1132

2544

400 U

10686

1472

633

400 U

4571 B

22OCT5:0011GA10

379GLBR-112F

Sponsor ID

MSL Code

Pyrene

Fluoranthene

Anthracene

Phenanthrene

Flourene

thene

Acenaph-

Acenaphthylene

Naphthatene B - Analyte was also detected in the associated blank

D - Secondary analysis performed at dilution factor of 1:5

U = Undetected at the given method detection limit I = Interference present

• - Outside EPA and internal QC criteria (40-120%).

MATRIX: WATER		(Concentrations in ng/L)	in ngA)					
		Benz[a]-	•	Benzofluor-	Benzo[a]-	Indeno [1,2,3-cd]-	Dibenz[a,h]-	Benzo[ghi]
MSL Code	Sponsor ID	anthracene	Chrysene	anthenes #	pyrene	pyrene	anthracene	perylene
379GLBR-112CD	22OCT5:0011GA10	647	890	235	149	57	70	170
379GLBR-232C	23OCT4:4511GA20	450	45 U	910	45 U	45 U	45 U	
379GLBR-233C	24OCT5:3011GA3O	005	50 U	100 0	0.05	50 U	50 U	50 U
379GLBR-234C	250CT1:4511GB10	0 22 0	57 U	1140	57 u	57 U	57 U	,
379GLBR-272C	31OCT1:0011GB3O	740	740	148 U	740	74 U	74 U	
Method Blank-WATER	TER	20 U	20 U	40 n	20 U	20 U	20 U	20 U
MATRIX: SOLVENT BLANK	IT BLANK	(Concentrations in ng/L	i in ng/L)					
						ouepul		

# - All benzofluoranthene isomers (b, j & k) are quantified together

400 U

400 n

400 U

400 U

800 U

400 n

400 U

220CT5:0011GA10

379GLBR-112F

Benzo[ghi] perylene

Dibenz[a,h]anthracene

[1,2,3-cd]-

Benzo[a]pyrene

Benzofluoranthenes #

Chrysene

anthracene

Sponsor 1D

MSL Code

Benz[a]-

pyrene

B - Analyte was also detected in the associated blank

D - Secondary analysis performed at dilution factor of 1:5

U - Undetected at the given method detection limit i - Interference present

- Outside EPA and Internal QC criteria (40-120%).

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## BUFFALO RIVER PILOT PROJECT (#379) SIR/PAH ANALYSIS IN AIR SAMPLES

MATRIX: WATER

		%	% Surrogate Recovery	
		D10-	D10-	D10-
MSL Code	Sponsor ID	Fluorene	Anthracene	Pyrene
			i	
3/9GLBH-112CD		<b>8</b> 8%	82%	149% 1
379GLBR-232C	230CT4:4511GA20	74%	19%	<b>%68</b>
379GLBR-233C	24OCT5:3011GA3O	25%	54%	<b>%</b> 89
379GLBR-234C	250CT1:4511GB10	75%	71%	87%
379GLBR-272C	31OCT1:0011GB3O	%69	65%	87%
Method Blank-WATER		25%	35%	72%

MATRIX: SOLVENT BLANK

MSL Code Sponsor ID Fluorene Anth			%	<ul> <li>Surrogate Recovery</li> </ul>	
MSL Code Sponsor ID Fluorene Anth			D10-	D10-	D10-
	MSL Code	Sponsor ID	Fluorene	Anthracene	Pyrene

MSL Code	Sponsor ID	D10- Fluorene	D10- Anthracene	D10- Pyrene
379GLBR-112F	22OCT5:0011GA10	101%	80%	116%

# - All benzofluoranthene isomers (b, j & k) are quantified together

B = Analyte was also detected in the associated blank
D = Secondary analysis performed at dilution factor of 1:5

U - Undetected at the given method detection limit

Interference present
 Outside EPA and internal QC criteria (40-120%).

# BUFFALO RIVER PILOT PROJECT (#379) PCB/PESTICIDE ANALYSIS IN AIR SAMPLES

MATRIX: XAD		(Concentrations	in ug/sample)		-				
		Monochloro-	Dichloro-	Trichloro-	Tetrachloro-	Pentachloro-	Hexachloro-	Heptachloro-	Octachloro-
MSL Code	Sponsor ID	biphenyl	biphenyl	biphenyl	biphenyl	biphenyl	biphenyl	biphenyl	biphenyl
379GLBH-112ABE	22OCT5:0011GA10	0.75 U	0.75 U	0.75 U	1.5.	J 1.5 L	1.5	U 2.3 U	2.3 U
379GLBR-232ABD	230CT4:4511GA20	0.75 U	0.75 U	0.75 U		J 1.5 U	1.5	U 2.3 U	2.3 U
379GLBR-233ABD	240CT5:3011GA30		0.75 U	0.75 U			1.5	U 2.3 U	2.3 U
379GLBR-234ABD	250CT1:4511GB10	0.75 U	0.75 U	0.75 U	1.5 L	1.5 L	1.5	U 2.3 U	2.3 U
379GLBR-272ABD	31OCT1:0011GB3O	0.75 U	0.75 U	3.6	2.3		1.5	U 2.3 U	2.3 U
Method Blank-XAD		0.75 U	0.75 U	0.75 U	1.5 (	1.5.1	1.5 U	U 2.3 U	2.3 U
MATRIX SPIKE RESULTS	ULTS								
Amount Spiked		12	12	12	24	24	24	36	36
Method Blank		0.75 U	0.75 U	0.75 U	1.5 (	J 1.5 L	1.5 U	2 	
Blank + Spike		9.9	7.8	8.7		21	18		27
Amount Recovered		9.9	7.8	8.7	18	17	18	27	
Percent Recovery		55%	<b>65%</b>	73%	75%	71%	75%	75%	7
Amount Spiked		12	12	12	24	24	24	<b>9</b>	36
Method Blank		0.75 U	0.75 U	0.75 U	1.51	1.5 U		U 2.3 U	2.3 U
Blank + Spike Duplicate	cate	7.3	7.7	7.8	9	13		10	19
Amount Recovered		7.3	7.7	7.8	16	13	13	6	19
Percent Recovery		61 <b>%</b>	64%	<b>%</b> 59	<b>67%</b>	54%	54%	23%	23%
MATRIX: SOLVENT BLANK	BLANK	(Concentrations in ug/L)	In ug/L)						

15 U Octachlorobiphenyl 15 U Hexachloro- Heptachlorobiphenyl 10 U biphenyl 10 U Trichloro- Tetrachloro- Pentachloroblphenyl 10 U biphenyl 5.0 U biphenyl 5.0 U Dichlorobiphenyl 5.0 U Monochlorobiphenyl 220CT5:0011GA10 Sponsor ID 379GLBR-112F MSL Code

U - Undetected at the given method detection limit.

<sup>• -</sup> Outside EPA and internal QC criteria (40-120%).

# BUFFALO RIVER PILOT PROJECT (#379) PCB/PESTICIDE ANALYSIS IN AIR SAMPLES

MATRIX: XAD		(Concentration:	(Concentrations in ug/sample)		SIDO %	% Surrogate Recovery	_
		Nonachioro-	Decachloro-	2-Fluoro	١.	C13-Tetrachloro-	C13-Octachloro-
MSL Code	Sponsor ID	biphenyl	biphenyl	bloheny		biphenyl	bipheny
379GLBR-112ABE	22OCT5:0011GA10	2.3 U	3.8 U	62%	<b>₩</b>	71%	26%
379GLBR-232ABD	230CT4:4511GA20	2.3 U	3.8 ∪		*	107%	<b>%</b> 96
379GLBR-233ABD	24OCT5:3011GA3O	2.3 U	3.8 ∪	77	*	112%	105%
379GLBR-234ABD	250CT1:4511GB10	2.3 U	3.8 ∪	%09	*	94%	95%
379GLBR-272ABD	31OCT1:0011GB3O	2.3 U	3.8 U	53	*	82%	<b>88</b> %
Method Blank-XAD		2.3 U	3.8 U	23%	•	%19	64%
MATRIX SPIKE RESULTS	SULTS						
Amount Spiked		22	09	Z	¥	¥	<b>4</b> 2
Method Blank		2	3.8 U	23%	. *	67%	64%
Blank + Spike		\$	45	25	*	97%	85%
Amount Recovered		\$	45	¥	⋖	¥Z	<b>A</b> N
Percent Recovery		22	75%	2	¥	¥	<b>A</b> N
Amount Spiked		\$2	09	~	¥	¥	<b>4</b> X
Method Blank		\$2	3.8 U	23%	*	%29	49
Blank + Spike Duplicate	dicate	22	32	64%	*	71%	%29
Amount Recovered		<u>\$</u>	32		⋖	¥	¥X
Percent Recovery		8	23%		NA V	N N	<b>*</b>
MATRIX: COI VENT BI ANY					3		
MAINIA. SOLVEN		Concentrations in ug/L)	S in ug/L)	i		% Surrogate Hecovery	را الا
MSL Code	Sponsor ID	Nonachioro- biphenvi	Decachioro- biphenyl	2-Fluoro- biphenvi		C13-1 etrachioro- biohenvi	C13-Octachloro-

Undetected at the given method detection limit.
 Louiside EPA and internal QC criteria (40-120%).

94%

83%

47%

25

220CT5:0011GA10

379GLBR-112F



662 CROMWELL AVENUE ST. PAUL, MN 55114 PHONE 612/645-3601

PROJECT:

PCB/PAH ANALYSES

DATE: January 9, 1992

ISSUED TO:

Battelle Pacific Northwest Division

**INVOICE NO: 4410 92-0442B** 

Attn: Ms. Linda Bingler Marine Sciences Laboratory 439 West Sequim Bay Road

Sequim, WA 98382

#### INTRODUCTION

This report summarizes the results from analyses performed on eleven samples which were submitted by a representative of Battelle Pacific Northwest Division. Six of the samples were analyzed for the presence or absence of polychlorinated biphenyls (PCBs) using a modified version of USEPA Method 680 and all of the samples were analyzed for polynuclear aromatic hydrocarbons (PAHs) using a version of USEPA Method 8270 adapted for selected-ion-monitoring analyses.

#### SAMPLE IDENTIFICATION

Client ID	Sample Type	Analyses	TCT ID
379GLBR*112ABE 379GLBR*112CD 379GLBR*112F 379GLBR*232ABD 379GLBR*233C 379GLBR*233ABD 379GLBR*233C 379GLBR*234ABD 379GLBR*234C	Air Impinger Blank Solvent Air Impinger Air Impinger Air Impinger Air	PCB/PAH PAH PCB/PAH PCB/PAH PAH PCB/PAH PCB/PAH PCB/PAH PAH PAH	268734 268743 268741 268735 268744 268736 268750 268737 268751
379GLBR*272ABD 379GLBR*272C	Air Impinger	PCB/PAH PAH	268738 268752

PROJECT: PCB/PAH ANALYSES DATE: January 9, 1992

PAGE: 2 INVOICE NO: 4410 92-0442B

#### **METHODOLOGY**

#### Sample Extraction

The XAD-2 resin and filter from each air sample component set were combined in a Soxhlet extractor and spiked with the following surrogate standard compounds:

	<u>μg Spiked</u>
2-Fluorobiphenyl	30
"C <sub>1</sub> -Tetrachlorobiphenyl	9.6
"C <sub>n</sub> -Octachlorobiphenyl	9.6
<sup>2</sup> H <sub>10</sub> -Fluorene	1.5
<sup>2</sup> H <sub>10</sub> -Anthracene	1.5
<sup>2</sup> H <sub>10</sub> -Pyrene	1.5

Each sample was extracted with methylene chloride and each extract was combined with the respective train rinse solvent component. The extracts were transferred to Kuderna-Danish flasks, concentrated to 3.0 mL, and split into three equal portions for PCB, PAH, and PCDD/PCDF analyses. (The results from the PCDD/PCDF analyses were reported previously in TCT report #4410 92-0442A.) The PCB portions were solvent exchanged to hexane and spiked with 10 ug of each of the following perdeuterated internal standards:

'H.,-Phenanthrene

'H.,-Chrysene

The impinger catch samples were spiked with 0.5  $\mu$ g of each of the three perdeuterated PAH surrogates listed above, extracted with methylene chloride in separatory funnels, and the extracts were concentrated to 1.0 mL using Kuderna-Danish glassware. All of the final PAH extracts were then spiked with 0.5  $\mu$ g of each of the following perdeuterated internal standards:

<sup>2</sup>H<sub>8</sub>-Naphthalene <sup>2</sup>H<sub>10</sub>-Acenaphthene <sup>2</sup>H<sub>10</sub>-Phenanthrene <sup>2</sup>H<sub>12</sub>-Chrysene <sup>2</sup>H<sub>12</sub>-Perylene

PROJECT: PCB/PAH ANALYSES DATE: January 9, 1992

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#### **PCB** Analyses

PCB analyses were performed according to a modified version of USEPA Method 680. A 1-uL aliquot of each sample extract was injected by autosampler onto a 30 m DB-5 capillary column in a Hewlett-Packard Model 5890A gas chromatograph. The column exit was interfaced directly into the ion source of a VG Trio-2 quadrupole mass spectrometer operating in the positive ion electron impact (EI) ionization mode at 70 eV. The GC/MS operating conditions for these analyses are listed in Table 1. Data were acquired in the selected-ion-monitoring mode and processed using a VG 11-250J data system.

A five point initial calibration curve was generated by analyzing standard solutions containing the target compounds at concentrations ranging from 0.5-125 ug/mL as shown in Table 2. Each solution contained internal standards at fixed concentrations of 10 ug/mL. Response factors were generated for each target analyte relative to the corresponding internal standard using the measured area responses for characteristic ions and the known concentrations. Continuing calibration check standards were analyzed daily prior to sample analysis in order to verify the validity of the initial calibration. All calculations were performed as specified in Method 680. The specific ions that were monitored for quantitation and confirmation of the PCB compounds are listed in Table 3.

#### PAH Analyses

The PAH analyses were performed by selected-ion-monitoring (SIM) gas chromatography/mass spectrometry (GC/MS) using procedures from USEPA Method 8270. 2-uL aliquots of the sample extracts were injected by autosampler onto a 30 m DB-5 capillary column in a Hewlett-Packard Model 5890A gas chromatograph. The column exit was interfaced directly into the ion source of a VG Trio-2 quadrupole mass spectrometer operating in the positive ion electron impact (EI) ionization mode at 70 eV. Data were acquired in the selected-ion-monitoring mode and processed using a VG 11-250J data system. The GC/MS operating conditions for these analyses are summarized in Table 1A.

A five point initial calibration curve was generated by analyzing standard solutions containing each of the target analytes at levels ranging from 20-1000 ng/mL and the internal standards at fixed concentrations of 500 ng/mL as indicated in Table 2A. Quantifications of the target compounds were performed by comparing the integrated areas of the chromatographic peaks with those of the internal standards as specified in Method 8270. Continuing calibration standard analyses were performed daily prior to sample analyses in order to verify the validity of the initial calibration. The specific ions that were monitored for the PAH analyses are listed in Table 3A.

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#### RESULTS

The results from the analyses are included in the following appendices:

Appendix A	Chain of Custody Documentation
Appendix B	PCB Sample Analysis Results
Appendix C	PCB QA/QC Analysis Results
Appendix D	PCB Sample Chromatograms
Appendix E	PCB QA/QC Chromatograms
Appendix F	PAH Sample Analysis Results
Appendix G	PAH QA/QC Analysis Results
Appendix H	PAH Sample Chromatograms and Raw Data
Appendix I	PAH QA/QC Chromatograms and Raw Data

#### **DISCUSSION**

The recoveries of the surrogate compounds in the PCB samples fell within the 50-125% guidelines specified in Method 680, with the exception of the 2-Fluorobiphenyl recovery (47%) in sample 379GLBR\*112F. The designated range for the surrogate compounds in the PAH samples is 50-150% for at least two of the three surrogates in each sample. All of the surrogate recoveries in the PAH samples fell within this range, with the exception of the perdeuterated pyrene (227%) in sample 379GLBR\*112ABE. This elevated recovery resulted from the presence of an interference in the sample extract that was not resolved from the surrogate peak. However, since the remaining two surrogates in this sample were recovered at acceptable levels, the recovery criteria were met and no corrective action was required. The only other deviation from the target QC ranges was that of the raw area count for the perdeuterated naphthalene internal standard in sample 379GLBR\*272ABD, which was 269% of the value for the corresponding standard in the daily continuing calibration analysis. (The target range for internal standard areas in the sample extracts is 50-200% of the daily continuing calibration values.) However, upon analysis of a dilution of this sample extract, the naphthalene internal standard area fell into the acceptable range.

A laboratory method blank was prepared and analyzed with each sample extraction batch as part of our routine quality control/quality assurance procedures. The results, found at the beginnings of Appendices C and G, show the blanks to be free of the target PCB and PAH analytes, with the exception of a trace background level (77 nanograms) of naphthalene in the blank associated with the PAH portions of the air

PROJECT: PCB/PAH ANALYSES

DATE: January 9, 1992

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#### **DISCUSSION** (Continued)

samples. The naphthalene levels determined for the affected samples were all higher than the naphthalene level in the blank by 20 times or more. This indicates that the sample processing steps did not contribute significantly to the levels reported for the samples. A low recovery was achieved for the 2-Fluorobiphenyl surrogate in the PCB blank due to inadvertent volatilization of this compound during the concentration steps. Since the entire sample was consumed in the extraction process, any reprocessing in order to improve the recovery was not possible. Also, the blank associated with the impinger samples exhibited a low recovery (35%) for the perdeuterated anthracene surrogate. Since good recoveries were achieved for the other two surrogates in this blank, no corrective action was required.

Two laboratory quality control PCB/PAH spike samples were prepared with the air sample batch by extracting aliquots of clean resin that had been fortified with native standard materials. The results, included in Appendices C and G, show that the spiked native compounds were recovered at levels ranging from 52-132%, which are all within the 50-135% target ranges designated for these analyses.

#### **REMARKS**

The sample extracts will be retained for a period of 60 days from the date of this report and then discarded unless other arrangements are made. The raw mass spectral data will be archived on magnetic tape for a period of not less than one year. Questions regarding the data contained in this report may be addressed to the authors at the numbers provided below.

#### TWIN CITY TESTING CORPORATION

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High Resolution Mass Spectrometry

Approved by:

Charles V. Sueper, Supervisor

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David P. Zimmerman, Scientist Low Resolution Mass Spectrometry

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PROJECT:

PCDD/PCDF ANALYSES

DATE: January 6, 1992

**INVOICE NO: 4410 92-0442A** 

ISSUED TO:

Battelle Pacific Northwest Division

Attn: Ms. Linda Bingler Marine Sciences Laboratory

Sequim, WA 98382

#### INTRODUCTION

This report summarizes the results from the analyses performed on six air samples which were submitted by a representative of Battelle Pacific Northwest Division. The samples were analyzed for the presence or absence of polychlorinated dibenzo-p-dioxins (PCDDs) and polychlorinated dibenzofurans (PCDFs) using a modified version of EPA Method 23. Polychlorinated biphenyl (PCB) and polynuclear aromatic hydrocarbons (PAH) data will be reported under separate cover.

#### SAMPLE IDENTIFICATION

Client ID **	Sample Type	TCT ID
379GLBR*112ABE	Air	268734
379GLBR*112F	Blank	268741
379GLBR*232ABD	Air	268735
379GLBR*233ABD	Air	268736
379GLBR*234ABD	Air	268737
379GLBR*272ABD	Air	268738

<sup>\*\*</sup> Samples and sample components were split as per instructions from Battelle personnel included in Appendix A.

#### <u>METHODOLOGY</u>

#### PCDD/PCDF Extraction

The XAD-2 resin portion of each sample component set was spiked with isotopically-labeled PCDD/PCDF internal standards (Table 1), combined with the filter, and placed in a Soxhlet extractor thimble. The train rinse solvents containing particulate were filtered and the filters were added to the respective Soxhlet extractor thimbles. The filtrate was then concentrated in the Soxhlet flask and the Soxhlet charged with methylene chloride. The sample components were extracted for eighteen hours and the methylene chloride was removed and concentrated. The Soxhlet was then recharged with benzene and extracted for an additional eighteen hours. One third of each of the methylene chloride and benzene extracts were then

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PCDD/PCDF ANALYSES

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#### PCDD/PCDF Extraction (Continued)

combined and quantitatively transferred to Kuderna Danish concentrators, concentrated, and solvent exchanged to hexane. The hexane extracts were then processed through the analyte enrichment procedures described below.

#### Analyte Enrichment for PCDD/PCDF Analyses

The extraction procedure often removes a variety of compounds, in addition to the PCDDs and PCDFs, from the sample matrix. Some of these compounds can directly interfere with the analyses while others can overload the capillary column causing degradation in chromatographic resolution or sensitivity. The analyte enrichment steps described below were used to remove interferences from the extracts.

The extracts were diluted to 100 mL with hexane, transferred to separatory funnels, and washed with 1N sodium hydroxide, concentrated sulfuric acid, and distilled water. The hexane layers were concentrated to 1 mL and quantitatively transferred to liquid chromatography columns containing alternating layers of silica gel, 44% concentrated sulfuric acid on silica gel, and 33% 1 N sodium hydroxide on silica gel. The columns were eluted with 60 mL of hexane and each entire eluate was collected and concentrated, under a gentle stream of dry nitrogen, to a volume of 1 mL.

The extracts were then fractionated on liquid chromatography columns containing 4 g of activated alumina. The columns were eluted with 10 mL of hexane followed by 7 mL of 2.0% methylene chloride/hexane and 25 mL of 60% methylene chloride in hexane. The 60% methylene chloride/hexane fractions were concentrated to 1 mL under a stream of dry nitrogen and applied to the tops of chromatography columns containing 1 g of 5% AX-21 activated carbon on silica gel. Each column was eluted with cyclohexane/methylene chloride (50:50 V/V) and cyclohexane/methanol/benzene (75:20:5 V/V) in the forward direction, and then with benzene in the reverse direction. Each benzene fraction was collected, spiked with recovery standards (1,2,3,4-TCDD-13C<sub>12</sub> and 1,2,3,7,8,9-HxCDD-13C<sub>12</sub>) and concentrated to a final volume of 20 uL.

#### PCDD/PCDF Analyses

The extracts were analyzed for the presence of PCDDs and PCDFs using combined capillary column gas chromatography/high resolution mass spectrometry (HRGC/HRMS). The instrumentation consisted of a Hewlett Packard Model 5890 gas chromatograph and a VG Model 70SE high resolution mass spectrometer. The capillary column was interfaced directly into the ion source of the mass spectrometer, thus providing the highest possible sensitivity while minimizing degradation of the chromatographic resolution.

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#### PCDD/PCDF Analyses (Continued)

The mass spectrometer was operated in the electron impact ionization mode at a mass resolution of 10,000-11,000 (M/ $\Delta$ M, 10 percent valley definition). This resolution is sufficient to resolve most interferences, such as PCBs, thus providing the highest level of confidence that the detected levels of PCDD/PCDF are not false positives resulting from interferences. Typical operating parameters for the HRGC/HRMS analyses are summarized in Table 2.

The data were acquired by selected-ion-recording (SIR) monitoring the groups of ion masses described in EPA method 23. The five groups corresponded to the tetrachlorinated through octachlorinated congener classes. Each group contained three ion masses for the PCDDs (with the exception of TCDD which contained two ion masses), two ion masses for the PCDFs, the corresponding ion masses from the two isotopically labeled internal standards, and the ion mass characteristic of the polychlorinated diphenylether (PCDPE) which, if present, could cause false responses in the dibenzofuran channels. The third PCDD ion mass monitored in the pentachloro through octachlorodibenzo-p-dioxin groups prevented the possibility of misinterpretation of a polychlorinated biphenylene isomer as a PCDD. The two ion masses monitored for TCDD also fulfilled this purpose.

Each group of ion masses also contained a lock mass which was monitored during the analyses to detect suppressive interferences. It is particularly important to detect this type of interference since it can cause the quantification of congener class levels to be artificially high if it occurs during the elution of an internal standard or low if it occurs during the elution of the native analytes.

The lock mass was also used by the data system to automatically correct the mass focus of the instrument. The data system determined the centroid of the lock mass during each data acquisition cycle and corrected the mass focus of the analyte and internal standard ion masses to assure that the centers of the mass peaks were being monitored.

The criteria used to judge positive responses for the PCDD/PCDF isomer included:

- Simultaneous response at both ion masses of the PCDD or PCDF
- Signal to noise ratio equal to or greater than 2.5:1.0 for both ion masses
- Chlorine isotope ratio within 15% of the theoretical value

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PCDD/PCDF ANALYSES

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#### PCDD/PCDF Analyses (Cont.)

- Chromatographic retention time within -1 to +3 seconds of the authentic standards (where applicable)
- Chromatographic retention times within elution windows determined from analyses of standard mixtures
- Absence of simultaneous response between the PCDF and diphenylether ion traces

A list of the exact ion masses monitored for the determination of PCDD/PCDF isomers and the PCDPE interferences is presented in Table 3. Also included are the theoretical chlorine isotope ratios for the ten congener classes.

#### Quantification and Calculations

The PCDD/PCDF isomers were quantified by comparison of their responses to the responses of the labeled internal standards as described EPA Method 23. Relative response factors were calculated from analyses of standard mixtures containing representatives of each of the PCDD/PCDF congener classes at five concentration levels, and each of the internal standards at one concentration level, as shown in Table 4. The PCDD/PCDF response factors were calculated by comparing the sum of the responses from the two ion masses monitored for each chlorine congener class to the sum of the responses from the two ion masses of the corresponding isotopically labeled internal standard. Table 5 shows the response factor at each of the calibration levels as well as the average response factors and the relative percent deviation for each. The formula for the response factor calculation is:

 $Rf = \frac{An \times Ois}{Ais \times On}$ 

#### where:

Rf = Response factor

An = Sum of integrated areas for native isomer

Qis = Quantity of labeled internal standard

Ais = Sum of integrated areas for labeled internal standard

Qn = Quantity of native isomer

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PCDD/PCDF ANALYSES

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#### Quantification and Calculations (Cont.)

The levels of PCDD/PCDF in the samples were quantified using the following equation:

 $C = \frac{An \times Ois}{Ais \times W \times Rf}$ 

where:

C = Concentration of target isomer or congener class

An = Sum of integrated areas for the target isomer or congener class

Qis = Quantity of labeled internal standard added to the sample

Ais = Sum of integrated areas for the labeled internal standard

W = Sample weight, volume or area

Rf = Response factor

Each pair of ion mass peaks in the selected-ion-current chromatograms was evaluated manually to determine if it met the criteria for a PCDD or PCDF isomer. Areas of all peaks exhibiting correct ion ratios and having retention times within the correct windows were then summed for calculations of total congener concentrations. A summary of the high resolution initial calibration chlorine isotope ratios is presented in Table 6. The toxic equivalency factors used to calculate the 2,3,7,8-TCDD equivalency are listed in Table 7.

A limit of detection (LOD) based on producing a signal that is 2.5 times the noise level, was calculated for each undetected 2,3,7,8-substituted isomer of any tetra through octa chlorinated congener class. The noise heights used to calculate the detection limits were measured at the retention time of the specific isomer. The formula used for calculating the LOD is:

 $LOD = \frac{Hn \times Ois \times 2.5}{His \times W \times Rf}$ 

where:

LOD=Single isomer limit of detection

Hn =Sum of noise heights at native isomer retention time

Qis =Quantity of labeled internal standard added to the sample

His =Sum of peak heights for labeled internal standard

W = Sample weight, volume or surface area

Rf =Response factor

PROJECT:

PCDD/PCDF ANALYSES .

DATE: January 6, 1992

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#### Quantification and Calculations (Cont.)

The recovery of the 2,3,7,8-TCDD-<sup>37</sup>Cl<sub>4</sub> enrichment efficiency standard and each <sup>13</sup>C<sub>12</sub>-labeled internal standard, relative to either 1,2,3,4-TCDD-<sup>13</sup>C<sub>12</sub> or 1,2,3,7,8,9-HxCDD-<sup>13</sup>C<sub>12</sub>, was calculated using the following equation:

 $%R = \frac{Ais \times Ors \times 100\%}{Rfr \times Ars \times Ois}$ 

where:

%R = Percent recovery of labeled internal standard

Ais = Sum of integrated areas of labeled internal standards

Qrs = Quantity of recovery standard

Ars = Sum of integrated areas of recovery standard

Rfr = Response factor of the specific labeled internal standard relative to the recovery standard

Qis = Quantity of the labeled internal standard congener added to the sample

#### **RESULTS**

Sample analysis results are included in the following:

Appendix A - Chain of Custody Documentation

Appendix B - Sample Analysis Results

Appendix C - QA/QC and Daily Calibration Results

Appendix D - Sample Chromatograms and Raw Data

Appendix E - Standard Chromatograms and Raw Data

Appendix F - QA/QC Chromatograms and Raw Data

#### **DISCUSSION**

The recoveries of the isotopically-labeled PCDD/PCDF internal and surrogate standards in the air samples generally ranged from 70-130%, indicating a high level of efficiency through the extraction and enrichment steps. Somewhat lower recovery values were obtained for selected internal standards in each of the samples, many due to the presence of interfering substances in the final sample extracts. These interferences, evidenced by suppressions in the lock mass ion traces, caused short-term fluctuations in the

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PCDD/PCDF ANALYSES

DATE: January 6, 1992

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INVOICE NO: 4410 92-0442A

#### **DISCUSSION** (Continued)

sensitivity of the mass spectrometer, thereby decreasing the apparent recoveries for the affected standards. (Actual recoveries are typically consistent throughout a given sample or show gradual trends instead of abrupt changes.) All of the recoveries were, however, within the target ranges specified in the method, with the exceptions of the labeled 1,2,3,7,8-PeCDD in samples 379GLBR\*112F (37%), 379GLBR\*272ABD (37%), and the lab spike duplicate (36%). Also, slightly elevated recoveries were obtained for selected surrogate compounds in samples 379GLBR\*233ABD (labeled 1,2,3,4,7,8-HxCDD, 145%), 379GLBR\*272ABD (labeled 1,2,3,4,7,8-HxCDD, 148%), the laboratory spike (labeled 1,2,3,4,7,8,9-HpCDF, 135%), and the laboratory spike duplicate (labeled 1,2,3,4,7,8,9-HpCDF, 135%). The native 1,2,3,7,8-PeCDD concentrations should be accurate for these samples since quantitation is based on isotope dilution. The native 1,2,3,4,7,8-HxCDD and 1,2,3,4,7,8,9-HpCDF concentration values in these four samples may, however, be slightly elevated since both the native and surrogate isomers are compared to a separate labeled isomer.

A laboratory method blank was prepared and analyzed with the sample extraction batch as part of our routine quality control/quality assurance procedures. The data, included at the beginning of Appendix C, show the blank to be free of PCDDs and PCDFs, with the exceptions of trace background levels of PeCDD (19 picograms), HpCDD (6.3 picograms), and OCDD (92 picograms). The levels determined for the affected isomers in the actual samples were higher than the corresponding blank levels by 3-100 times. It should be noted, however, that levels less than five times higher than the background are not generally considered to be statistically different from the background.

Two quality control PCDD/PCDF spike samples were also prepared with the sample batch by extracting clean resin that had been fortified with native standard materials. The data, included in Appendix C, show that the spiked native compounds were recovered at levels ranging typically from 87-130%. The only compound with recoveries outside of this range was 1,2,3,4,7,8,9-HpCDF, which exhibited a recovery of 160% in each of the spike samples. It should be noted, however, that quality control ranges for native spike sample recoveries are not specified in the method.

PROJECT:

PCDD/PCDF ANALYSES

DATE: January 6, 1992

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#### **REMARKS**

The sample extracts will be retained for a period of 60 days from the date of this report and then discarded inless other arrangements are made. The raw mass spectral data will be archived on magnetic tape for a period of not less than one year. Questions regarding the data contained in this report may be addressed to the authors at the numbers provided below.

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SWH/CVS/SDM/Im1

MSL CODE	SPONSOR ID	OIL & GREASE (mg/L)
	BIN A	
379GLBR- 128 Rep 1	23OCT4:459LA2O	284.0
379GLBR- 128 Rep 2	230CT4:459LA20	287.0
379GLBR- 128 Rep 3	230CT4:459LA20	271.0
379GLBR- 132	23OCT5:2010LA2O	109.5
379GLBR- 163	250CT10:2010LA3M	214.0
379GLBR- 165	25OCT10:009LA3C	112.0
379GLBR- 204	300CT4:196LA30	1.1 U
	BIN B	
379GLBR- 187	250CT3:0710LB10	28.5
379GLBR- 226	31OCT10:129LB2O	62.0
379GLBR- 227	310CT10:2110LB20	69.5
379GLBR- 254	31OCT2:5710LB3M	25.0
379GLBR- 255	31OCT3:069LB3M	44.0
	BIN C	
379GLBR- 286 Rep 1	18NOV5:559LC1O	72.4
379GLBR- 286 Rep 2	18NOV5:559LC1O	95.2
379GLBR- 286 Rep 3	18NOV5:559LC1O	102.4
379GLBR- 326	19NOV5:509LC2O	81.5
379GLBR- 331	19NOV5:0510LC2O	30.4
379GLBR- 361	20NOV2:193LC3O	2.0
379GLBR- 366	20NOV2:419LC3O	112.8
379GLBR- 370	20NOV3:0110LC3O	16.3
	BIN D	
379GLBR- 398	21NOV3:2610LD1Q	71.2
379GLBR 404	21NOV4:169LD1O	57.0
	DILUTION WATER	
379GLBR- 275	6NOV12:003LO	1.1 U

U = Analyte detected below detection limits.

MSL CODE	SPONSOR ID		OIL & GREASE (mg/L)	·
BLANKS	<b>:</b>			
BLANK-1			0.12	
BLANK-2			0	1.1.1.4.8
BLANK-3			0	
BLANK-4			0.67	
BLANK-5			0	
BLANK-6			0	
BLANK-7			0.80	
BLANK-8			0	
MATRIX SPIKE RESU	LTS		% F	RECOVERY
379GLBR- 128 *	230CT4:459LA20			
379GLBR- 128 MATR			280.7	
379GLBR- 128 MATR			347.5	134% • •
	MOINE BOILDATE		<b>3</b> 35.0	109%
379GLBR- 132	23OCT5:2010LA2C	)	109.5	
379GLBR- 132 MATR	IX SPIKE		157.5	96%
379GLBR- 132 MATR	IX SPIKE DUPLICATE		157.0	95%
				9976
555146455				
REPLICATE ANALYSE	ES			
379GLBR- 128 Rep 1	00007.47-4			
379GLBR- 128 Rep 2	230CT4:459LA20		284.0	
379GLBR- 128 Rep 3			287.0	
	230CT4:459LA20	D0D 44	271.0	
379GLBR- 286 Rep 1	18NOV5:559LC10	RSD %	3%	
379GLBR- 286 Rep 2			72.4	
379GLBR- 286 Rep 3	18NOV5:559LC10		95.2	
	10110 43.5532.010	RSD %	102.4	
		13U %	17%	

U = Analyte detected below detection limits.

<sup>• =</sup> Mean of replicated sample.

<sup>\*\* =</sup> Outside of QC criteria (40-120%).
RSD % = Relative Standard Deviation.

MSL CODE	SPONICOD ID	OIL & GREASE
WIGE CODE	SPONSOR ID	ug/g
	BIN A	
	· · · · · · · · · · · · · · · · · · ·	
379GLBR- 13	07OCT12:341SAO	1211.6
379GLBR- 16	07OCT12:401SAO	1389.2
379GLBR- 17	07OCT12:091SAO	1644.3
379GLBR- 57	09OCT11:502SA3O	1765.7
379GLBR- 58	09OCT11:382SA2O	1819.5
379GLBR- 59	09OCT11:282SA1O	1426.2
379GLBR- 104	220CT11:317SA10	7232.5
379GLBR- 107	220CT11:378SA10	3133.0
379GLBR- 108	220CT4:203SA2O	<b>25</b> 65. <b>5</b>
379GLBR- 111 Rep 1	220CT5:563SA2O	2867.7
379GLBR- 111 Rep 2	220CT5:563SA2O	1839.4
379GLBR- 111 Rep 3	220CT5:563SA2O	2283.9
379GLBR- 113	230CT1:303SA2O	1855.0
379GLBR- 122	230CT4:284SA20	94.6 U R
379GLBR- 123	230CT4:274SA20	306.2 U R
379GLBR- 124	230CT4:294SA20	300.9 U R
379GLBR- 136	240CT10:457SA20	2390.8
379GLBR- 139	240CT10:508SA2O	696.4
379GLBR- 141	24OCT2:203SA3O	1690.4
379GLBR- 143	24OCT5:503SA3O	2669.4
379GLBR- 145	24OCT6:203SA3O	2390.8
379GLBR- 151	250CT9:224SA30	632.8 R
379GLBR- 152	250CT9:224SA30	490.2 U
379GLBR- 153	250CT9:214SA30	537.7 U
79GLBR- 166	25OCT9:307SA3O	2442.7
79GLBR- 167	250CT9:368SA30	1900.9

U = Analyte detected below detection limits.
R = Reruns.

		OIL & GREASE
MSL CODE	SPONSOR ID	ug/g
	BIN B	
379GLBR- 14	07OCT1:101SBO	1144.5 R
379GLBR- 21	07OCT12:531SBO	1537.6
379GLBR- 23	07OCT1:011SBO	2174.0
379GLBR- 65	09OCT9:542SB1O	2005.5
<b>3</b> 79GLBR- 66	09OCT10:152SB2O	2082.0
379GLBR- 67	09OCT10:352SB3O	1511.7
379GLBR- 174	250CT12:153SB10	2357.2
379GLBR- 176	250CT2:153SB1O	1753.9 R
379GLBR- 181	250CT2:254SB10	560.4 U
379GLBR- 182	<b>2</b> 50CT2:294SB1O	396.7 U
379GLBR- 183	250CT2:284SB10	464.2 U
379GLBR- 193	250CT3:527SB10	3770.7
379GLBR- 196	250CT3:578SB1O	1898.7
379GLBR- 198	300CT2:493SB2O	2071.2
379GLBR- 199 Rep 1	30OCT4:013SB2O	1634.5
379GLBR- 199 Rep 2	300CT4:013SB2O	1306.0
379GLBR- 199 Rep 3	30OCT4:013SB2O	1610.2 R
379GLBR- 206	300CT4:413SB2O	2148.9
379GLBR- 210	31OCT9:027SB2O	1231.0
379GLBR- 213	31OCT9:078SB2O	. 449.3
379GLBR- 220	31OCT9:264SB2O	203.7
379GLBR- 221	31OCT9:254SB2O	312.1
379GLBR- 222	31OCT9:244SB2O	144.0 U
379GLBR- 242	31OCT10:453SB3O	1192.5
379GLBR- 243	31OCT11:503SB3O	1232.5 R
379GLBR- 244	310CT2:303SB30	1549.8
379GLBR- 247	310CT2:384SB30	235.9 U R
379GLBR- 248	310CT2:354SB30	413.2 U
379GLBR- 249	31OCT2:364SB3O	520.0 U
379GLBR- 268	1NOV10:208SB3O	586.2 U
379GLBR- 269 Rep 1	1NOV10:157SB3O	1436.9
379GLBR- 269 Rep 2	1NOV10:157SB3O	1428.3
379GLBR- 269 Rep 3	1NOV10:157SB3O	1633.9

U = Analyte detected below detection limits. R = Reruns.

lacksquare	MSL CODE	SPONSOR ID	OIL & GREASE ug/g
	1	• Company of the Comp	

		BIN C		
379GLBR- 15		070CT1:211SCO		2779.2
379GLBR- 18		07OCT1:331SCO		2180.1
379GLBR- 20		07OCT1:441SCO		1822.6
379GLBR- 73		09OCT4:562SC1O		3995.4
379GLBR- 74		09COT4:352SC2O	· .	1761.2
379GLBR- 75		09OCT4:162SC3Q		2398.5
379GLBR- 280		18NOV2:553SC1O		2374.9 R
379GLBR- 282		18NOV3:503SC1O		1845.4 R
379GLBR- 284		18NOV4:403SC1O		2105.6 R
379GLBR- 288		18NOV6:1510LC1O		6290.3
379GLBR- 302		19NOV8:594SC1O		527.6 U
379GLBR- 303		19NOV9:004SC1O		786.6 R
379GLBR- 304		19NOV9:014SC1O		371.5 U
379GLBR- 307		19NOV9:238SC1O		2538.7
379GLBR- 311		19NOV11:303SC2O		2729.1 R
379GLBR- 313		19NOV2:203SC20		1663.3
379GLBR- 315		19NOV3:553SC2O		1641.1
379GLBR- 323		19NOV4:504SC2O		507.7 U
379GLBR- 324		19NOV4:504SC2O		471.6 U R
379GLBR- 325		19NOV4:504SC2O		549.3 U
379GLBR- 337		20NOV8:157SC2O		2416.0
379GLBR- 340		20NOV11:443SC3O		4897.3
379GLBR- 342		20NOV1:003SC3O		4759.8
379GLBR- 344		20NOV1:553SC3O		3107.3
379GLBR- 350		20NOV3:154SC3O		2695.4
379GLBR- 351		20NOV3:154SC3O		4609.4
379GLBR- 352		20NOV3:154SC3O		3549.0
379GLBR- 357		20NOV3:337SC3O		4388.9
379GLBR- 360 Re	•	20NOV3:278SC3O		762.4
379GLBR- 360 Re		20NOV3:278SC3O		505.3 U
379GLBR- 360 Re	p 3	20NOV3:278SC3O	•	668.9 R

U = Analyte detected below detection limits. R = Reruns.

	,	OIL & GREASE
MSL CODE	SPONSOR ID	ug/g
	•	

	:	
	BIN D	
379GLBR- 19	07OCT2:041SDO	
379GLBR- 22		2105.9
379GLBR- 22	07OCT1:521SDO	1342.1
	07OCT2:122SDO	1671.9
379GLBR- 46	08OCT5:132SD3O	2347.2
379GLBR- 51	08OCT5:402SD1O	2416.3
379GLBR- 53	08OCT5:302SD2O	3038.9
379GLBR- 376	21NOV12:003SD1O	3197.3 R
379GLBR- 378	21NOV1:353SD1O	1054.8 R
379GLBR- 380	21NOV2:433SD1O	2921.6 R
379GLBR- 384 Rep 1	21NOV5:078SD1O	974.5
379GLBR- 384 Rep 2	21NOV5:078SD1O	748.9
379GLBR- 384 Rep 3	21NOV5:078SD1O	1172.9
379GLBR- 388	21NOV5:107SD1O	5368.3
379GLBR- 395	21NOV5:224SD1O	238.4 U
379GLBR- 396	21NOV5:224SD1O	790.9
379GLBR- 397	21NOV5:224SD1O	907.7
BLANK-1		0.0060
BLANK-2		0.0010
BLANK-3		0.0020
BLANK-4		0.0008
BLANK-5		0.0020
BLANK-6		0.0020
BLANK-7		0.0033
BLANK-8		0.0066
BLANK-9		0.0000
		5.0000

U = Analyte detected below detection limits. R = Reruns.

	,	OIL & GREASE
MSL CODE	SPONSOR ID	ug/g
L		

MATRIX SPIKE RESULTS		% RECOVERY
379GLBR- 111 * * 220CT5:563SA2O 379GLBR- 111 MATRIX SPIKE	2330.	_
379GLBR- 111 MATRIX SPIKE DUPLICATE	3932.0 3369.1	•
379GLBR- 182 25OCT2:294SB1O 379GLBR- 182 MATRIX SPIKE	610.( 2190.7	
379GLBR- 182 MATRIX SPIKE DUPLICATE	2159.0	
379GLBR- 269 * * 1NOV10:157SB3O 379GLBR- 269 MATRIX SPIKE	1499.7 2478.5	et a constant and a c
379GLBR- 269 MATRIX SPIKE DUPLICATE	2533.9	30.0
379GLBR- 360 * * 20NOV3:278SC30 379GLBR- 360 MATRIX SPIKE	645.5 1271.9	
379GLBR- 360 MATRIX SPIKE DUPLICATE	1590.8	
379GLBR- 384 * * 21NOV5:078SD1O 379GLBR- 384 MATRIX SPIKE	965.4 2784.3	
379GLBR- 384 MATRIX SPIKE DUPLICATE	2824.7	— , •

<sup>\*\* =</sup> Mean of replicated sample.

U = Analyte detected below detection limits.

 <sup>=</sup> Outside control limits.

	MSL CODE	SPONSOR ID		OIL & GREASE ug/g	
	REPLICATE ANALYSES				
	379GLBR- 111 Rep 1	220CT5:563SA2O		2007.7	
	379GLBR- 111 Rep 2	220CT5:563SA2O		2867.7	
	379GLBR- 111 Rep 3	220CT5:563SA2O		1839.4	
		220070.0000720	RSD %	2283.9 <b>22% *</b>	
	379GLBR- 199 Rep 1	300CT4:013SB2O		1634.5	
	379GLBR- 199 Rep 2	300CT4:013SB2O		1306.0	
	379GLBR- 199 Rep 3	300CT4:013SB2O		1610.2 R	
			RSD %	12%	
	379GLBR- 269 Rep 1	1NOV10:157SB3O		1436.9	
	379GLBR- 269 Rep 2	1NOV10:157SB3O		1428.3	
	379GLBR- 269 Rep 3	1NOV10:157SB3O		1633.9	
			RSD %	8%	
	379GLBR- 360 Rep 1	20NOV3:278SC3O		762.4	
	379GLBR- 360 Rep 2	20NOV3:278SC3O		610.0 U	
;	379GLBR- 360 Rep 3	20NOV3:278SC3O		668.9 R	
			RSD %	11%	
;	379GLBR- 384 Rep 1	21NOV5.078SD10		974.5	
;	379GLBR- 384 Rep 2	21NOV5:078SD1O		748.9	
;	379GLBR- 384 Rep 3	21NOV5:078SD1O		1172.9	
	•		RSD %	22% •	
Į	U = Analyte detected b	pelow detection limits.		ZZ 70	

R = Reruns.

RSD% = Relative Standard Difference.

Outside control limits.

BUFFALO RIVER PILOT PROJECT (CF #379)
PAH ANALYSIS IN SEDIMENT SAMPLES
(ANALYZED 10/91)

		(Concentrations In	(g/gu uj su									
MSL CODE	SPONSOR ID	Naph- thalene	Acenaph- thylene	Acenaph- thene	Fluorene	Phenan-	Anthra-	Fluoran-	0	Benzo(a)-		
							2	91911	A I A I A	Anthracene	Chrysene	7
379GLBR-15A	07OCT1:211SCO	47.16	34.74 U	52.92	75.80	633.88	157.45	1160 98	1017 21	240 00		
379GLBH*15B	07OCT1:211SCO	38.15	34.60 U	53.73	82 98	682 24	178 70	100.00	10000	20.246	6/5/3	
379GLBR*15C	07OCT1:211SCO	35.59	32.13 U	51.81	83.40	627.06	B / O / F	1100.09	1003.38	5/8/8	691.00	
379GLBR*17	07OCT12:091SAO	37.64	44.49.11	50 75 11		027.00	90.60	100.10	984.28	517.84	649.86	
379G! BB*24	0200113:631600	5.00	2 1 1 1	007.00		222.95	110.44	1036.45	840.05	443.84	581.27	
070010010	0,00112.331380	34.39 U	44.27 U	58.55 U	51.40 U	522.85	118.72	1398.88	1137.65	631.32	756 90	
3/30LBH-22	0/OC11:521SDO	147.09	169.14	164.88	193.68	546.84	246.40	1027.16	859.27	-561.82	665.26	
Blank		16.79 U	21.61 U	28.58 U	25.09 U	15.56 U	18.44 U	11.83 U	12.24 U	10.57, U	9.36 U	
STANDARD REFI	STANDARD REFERENCE MATERIAL											
SRM 1941	certified value	831.66 NC	260.31 U NC	344.29 U NC	302.25 U NC	482.72	222.14 U 202.00	1041.68	988.04 NC	486.81	630.54 NC	
MATRIX SPIKE RESULTS	TESULTS										2	
Amount Spiked 379GLBR*22 07C 379GLBR*22 + Spike Amount Recovered Percent Recovery	07OCT1:521SDO Spike ed	885.00 147.09 275.16 128.07	885.00 169.14 319.31 150.17	885.00 164.88 297.06 132.18	885.00 193.68 325.32 131.64	885.00 546.84 542.86 -3.98	885.00 246.40 371.73 125.33	385.00 1027.16 850.89 -176.27	885.00 859.27 750.86 -108.41	885.00 561.82 583.86 22.04	885.00 665.26 629.73 -35.53	
Amount Spiked 379GLBR*22 0 379GLBR*22 + Spik Amount Recovered Percent Recovery	Amount Spiked 379GLBR*22 07OCT1:521SDO 379GLBR*22 + Spike DUPLICATE Amount Recovered Percent Recovery	880.00 147.09 487.15 340.06	880.00 169.14 714.45 545.31 62%	880.00 164.88 678.57 513.69 58%	880.00 193.68 773.71 580.03 66%	880.00 546.84 1177.08 630.24 72%	880.00 246.40 921.38 674.98	880.00 1027.16 1755.21 728.05 83%	880.00 859.27 1565.81 706.54 80%	880.00 561.82 1298.38 736.56 84%	880.00 665.26 1332.46 667.2 76%	

U = Detected below detection limits

= Recoveries outside of QC limits.

NA = Not applicable.

NC = Not certified.

(CF #379)

PAH ANALYSIS IN SEDIMENT SAMPLES

(ANALYZED 10/91)

BUFFALO RIVER PILOT PROJECT

Page 2

649.86 Chrysene 3 675.73 691.00 Anthracene 578.78 517.84 **%** 542.02 Benzo(a)-**4** 1063.39 984.28 1017.31 Pyrene 1160.98 1222.89 1106.10 5% Fluoranthene 157.45 178.79 159.06 Anthra-7 cene 633.88 682.24 627.06 2% Phenanthrene 85.98 83.49 75.80 Fluorene 2% 52.92 53.73 ž 51.81 Acenaphthene 34.74 U 34.60 U 32.13 U (Concentrations in ng/g) Acenaph-۲ thylene 35.59 47.16 38.15 15% Naphthalene **RSD%** 070CT1:211SCO 070CT1:211SCO 07OCT1:211SCO SPONSOR ID REPLICATE ANALYSIS 379GLBR\*15A 379GLBR\*15B 379GLBR\*15C MSLCODE

U = Detected below detection limit

• - Recoveries outside of QC limits.

NA - Not applicable.

NC = Not certified.

BUFFALO RIVER PILOT PROJECT (CF #379)
PAH ANALYSIS IN SEDIMENT SAMPLES
(ANALYZED 10/91)

Fluoranthane         Pyrene         Anthracena         Perylene         Anthracena         Perylene         Thalene           5         434.19         542.81         438.57         103.80         280.39         42%           7         454.13         560.96         453.05         114.59         287.02         36%*           7         454.13         560.96         453.05         114.59         287.02         36%*           8         425.19         542.81         446.39         106.08         272.14         34%*           7         454.13         560.96         453.05         114.59         287.02         36%*           8         563.44         491.21         116.89         303.74         41%           8         564.10         491.21         116.89         303.74         41%           9         544.0         6.95.0         560.12         331.44         338.60         55%           10         5.51.0         6.95.0         569.00         NC         516.00         NA           885.00         670.00         569.00         NC         516.00         NA           885.00         685.00         885.00         885.00         NA </th <th></th> <th></th> <th>(Concentrations in ng/g)</th> <th>s in ng/g)</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>% Surrogate Recovery</th> <th></th>			(Concentrations in ng/g)	s in ng/g)						% Surrogate Recovery	
Fluoranthene Fluoranthene Purene	,	!	Benzo(b)-	Benzo(k)-	Benzo(a)	Indeno(1,2,3)	Dibenzo(a,h)	Benzo(g,h,i)	1	D10 Acenaph-	
627.45 434.19 542.81 438.57 103.80 280.39 42% 644.37 454.13 560.96 453.05 114.59 287.02 36% 580.88 425.19 521.53 426.39 106.08 272.14 34% C 651.80 508.84 584.10 491.21 116.89 303.74 41% C 657.08 492.32 554.67 560.12 331.44 338.60 55%  1.1.  796.14 555.91 496.65 553.05 136.81 423.60 69%  885.00 885.00 885.00 885.00 885.00 885.00 885.00 C 657.08 492.32 554.67 560.12 331.44 338.60 55% C 688.4 631.97 649.59 669.13 764.99 488.70 78% C 688.4 631.97 649.59 669.13 764.99 488.42 NA C 72% 72% 74% 66% C 78% 74% 75% C 78% 74% 74% 75% C 78% 75%	MSCODE	SPONSORID	Fluoranthene	Fluoranthene	Pyrene	Pyrene	Anthracene	Perylene	thalene	thalene D12 Perylene	Perylene
64.37 454.18 562.56 438.57 103.00 280.39 42% 658.08 425.19 521.53 426.39 106.08 272.14 34% 667.08 492.32 554.67 560.12 331.44 338.60 55%  667.10 5.51 U 6.95 U 5.49 U 6.40 U 3.77 U 85%  11. 736.14 555.91 496.65 553.05 136.81 423.60 69%  11. 865.00 885.00 885.00 885.00 885.00 885.00 885.00 886.00 880.00	379GI BR*15A	070CT1-911SCO	E97 4E	424 10	10 01	6	0	•			
644.37 454.13 560.96 453.05 114.59 287.02 36%. 650.88 425.19 521.53 426.39 106.08 272.14 34%. C 591.80 508.84 477.87 496.35 94.88 261.79 49%. C 691.80 508.84 584.10 491.21 116.89 303.74 41%. C 657.08 492.32 554.67 560.12 331.44 338.60 55%.  ILL  796.14 555.91 496.65 553.05 136.81 423.60 69%.  885.00 885.00 885.00 885.00 885.00 885.00 NA 667.08 444.00 670.00 569.00 NA 567.2 450.56 37.32 NA -4%.  886.00 886.00 886.00 880.00 880.00 880.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55%.  888.00 880.00 880.00 880.00 880.00 880.00 NA 667.08 657.08 1134.3 338.60 55%.  677.0 880.00 880.00 880.00 880.00 880.00 NA 667.08 657.08 1135.4 338.0 55%.  688.4 631.97 649.59 583.13 764.99 498.42 NA 72% 72% 74%.	Carried Core	00011311000	C+. 120	704	242.81	438.5/	103.80	280.39	45%	48%	<b>64%</b>
580.88 425.19 521.53 426.39 106.08 272.14 34%** O 571.17 395.44 477.87 408.35 94.88 261.79 49%* O 691.80 508.84 584.10 491.21 116.89 303.74 41%* O 667.08 492.32 554.67 560.12 331.44 338.60 55%  ILL  796.14 555.91 496.65 553.05 136.81 423.60 69%* Allue 780.00 670.00 569.00 ND 569.00 ND 667.08 885.00 885.00 885.00 885.00 885.00 885.00 885.00 885.00 885.00 885.00 885.00 885.00 885.00 886.00 886.00 886.00 880.00	3/8GLBH-158	0/0011211500	644.37	454.13	560.96	453.05	114.59	287.02	. %98	20%	%/9
667.08 685.00 685.00 685.00 885.00 885.00 885.00 885.00 885.00 885.00 880.00 88	379GLBR*15C	07OCT1:211SCO	580.88	425.19	521.53	426.39	106.08	272.14	34%	20%	%09
667.08 691.80 508.84 584.10 491.21 116.89 303.74 41% 667.08 492.32 554.67 560.12 331.44 338.60 55%  1.	379GLBR17	07OCT12:091SAO	571.17	395.44	477.87	408.35	94.88	261.79	49%	57%	70%
667.08 492.32 554.67 560.12 331.44 338.60 55%  6.71 U 5.51 U 6.95 U 5.49 U 6.40 U 3.77 U 85%  1.1  796.14 555.91 496.65 553.05 136.81 423.60 69%  885.00 885.00 885.00 885.00 885.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55%.  629.73 510.06 549.36 507.53 450.56 375.92 40%  880.00 880.00 880.00 880.00 880.00 880.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55%  880.00 880.00 880.00 880.00 880.00 880.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55%  1774 2.6 531 -52.59 119.12 37.32 NA 4%  1880.00 880.00 880.00 880.00 880.00 880.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55%  1786.4 631.97 649.59 583.13 764.99 498.42 NA 78% 72% 74% 66%. 87% 57% NA	379GLBR*21	07OCT12:531SBO	691.80	508.84	584.10	491.21	116.89	303.74	41%	57%	84%
6.71 U 5.51 U 6.95 U 5.49 U 6.40 U 3.77 U 65%  **Malue*** 780.14 555.91 496.65 553.05 136.81 423.60 69%  **Malue*** 780.00 444.00 670.00 569.00 NC 569.00 NC 560.00 885.00 885.00 NC 560.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55%  **Malue*** 510.06 549.36 507.53 450.56 375.92 40%  **Malue*** 510.06 549.36 507.53 450.56 375.92 NA 4%  **Malue*** 37.35 17.74 -5.31 -52.59 119.12 37.32 NA 4%  **Malue*** 580.00 880.00 880.00 880.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55%  **Malue**** 1124.29 1204.26 1143.25 1096.43 837.02 52%  **Malue***** 688.4 631.97 649.59 583.13 764.99 498.42 NA 78%  **Malue************************************	379GLBR*22	07OCT1:521SDO	667.08	492.32	554.67	560.12	331.44	338.60	22%	. 62%	77%
Alue         796.14         555.91         496.65         553.05         136.81         423.60         69%           Alue         780.00         444.00         670.00         569.00         NC         516.00         NA           885.00         885.00         885.00         885.00         885.00         885.00         NA           667.08         492.32         554.67         560.12         331.44         338.60         55%           629.73         510.06         549.36         507.53         450.56         37.59         40%           -37.35         17.74         -5.31         -52.59         119.12         37.32         NA           -4%*         2%*         -1%*         -6%*         13%*         4%*         NA           -80.00         880.00         880.00         880.00         880.00         880.00         55%           1355.48         1124.29         1204.26         1143.25         1096.43         837.02         55%           688.4         631.97         649.59         583.13         764.99         498.42         NA           78%         72%         74%         66%         87%         57%         NA	Blank		6.71 U		6.95 U					, 85%	75%
796.14         555.91         496.65         553.05         136.81         423.60         69%           alue         780.00         444.00         670.00         569.00         NC         516.00         NA           885.00         885.00         885.00         885.00         885.00         885.00         NA           667.08         492.32         554.67         560.12         331.44         338.60         55%           629.73         510.06         549.36         507.53         450.56         375.92         40%           -37.35         17.74         -5.31         -52.59         119.12         37.32         NA           -4%*         2%*         -1%*         -6%*         13%*         4%*         NA           880.00         880.00         880.00         880.00         880.00         880.00         880.00         55%           135.48         1124.29         1204.26         1143.25         1096.43         837.02         55%           688.4         631.97         649.59         583.13         764.99         498.42         NA           78%         72%         74%         66%         87%         87%         NA	STANDARD REF	ERENCE MATERIAL									
### 780.00 444.00 670.00 569.00 NC 516.00 NA	SBM 1941		706 44	40 444	000	1 6 1		1			
885.00 885.00 885.00 885.00 885.00 885.00 NA 55% 657.67 560.12 331.44 338.60 55% 657.63 17.74 -5.31 -52.59 119.12 37.32 NA -4% 2% 2% -1% -6.31 560.12 331.44 338.60 55% 135.48 1124.29 1204.26 1143.25 1096.43 837.02 52% 688.4 631.97 649.59 56% 87% 57% NA 57% NA 57% NA 56% 87% 57% NA 57% NA 57% NA 56% 87% 57% NA 57% NA		certified value		955.91	496.65	553.05	136.81	423.60	<b>%</b> 69	74%	85%
885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       885.00       55%         629.73       510.06       549.36       567.53       450.56       375.92       40%         -37.35       17.74       -5.31       -52.59       119.12       37.32       NA         -4%       2%       -1%       -6%       13%       4%       NA         880.00       880.00       880.00       880.00       880.00       880.00       880.00       880.00         667.08       492.32       554.67       560.12       331.44       338.60       55%         1355.48       1124.29       1204.26       1143.25       1096.43       837.02       52%         688.4       631.97       649.59       583.13       764.99       498.42       NA         78%       72%       74%       66%       87%       57%       NA					0.00	00.600	<b>≥</b>	516.00	ž	¥	¥
885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         885.00         85%           667.08         492.32         554.67         560.12         331.44         338.60         55%           -37.35         17.74         -5.31         -52.59         119.12         37.32         NA           -4%*         2%*         -1%*         -6%*         13%*         4%*         NA           880.00         880.00         880.00         880.00         880.00         NA           667.08         492.32         554.67         560.12         331.44         338.60         55%           1355.48         1124.29         1204.26         1143.25         1096.43         837.02         52%           688.4         631.97         649.59         583.13         764.99         498.42         NA           78%         72%         74%         66%         87%         87%         NA	MATRIX SPIKE	RESULTS									
667.08 492.32 554.67 560.12 331.44 338.60 55% 652.07 560.12 331.44 338.60 55% 55% 657.53 450.56 375.92 40% 492.32 510.06 549.36 507.53 450.56 375.92 40% 45% 2% -1% -5.31 -52.59 119.12 37.32 NA -4% 2% -1% -6.31 -56.79 119.12 37.32 NA 667.08 492.32 554.67 560.12 331.44 338.60 55% 1355.48 1124.29 1204.26 1143.25 1096.43 837.02 52% 668.4 631.97 649.59 583.13 764.99 498.42 NA 72% 72% 74% 66% 87% 57% NA	Amount Soiled	æ	0			1	, 1				
629.73 510.06 549.36 507.53 450.56 375.92 40% 629.73 510.06 549.36 507.53 450.56 375.92 40% -37.35 17.74 -5.31 -52.59 119.12 37.32 NA -4%	200 100 100 100 100 100 100 100 100 100	Od0101-140050	993.00	00.00	885.00	885.00	885.00	885.00	¥	¥	ž
629.73 510.06 549.36 507.53 450.56 375.92 40% -37.35 17.74 -5.31 -52.59 119.12 37.32 NA -4% 2% -1% -6.31 -52.59 119.12 37.32 NA -4% 2% -1% -6.31 -52.59 119.12 37.32 NA 880.00 880.00 880.00 880.00 880.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55% 1355.48 1124.29 1204.26 1143.25 1096.43 837.02 52% 688.4 631.97 649.59 583.13 764.99 498.42 NA 78% 72% 74% 66% 87% 57% NA	37 BGLBN 22	0/06/136/190/0	667.08	492.32	554.67	560.12	331.44	338.60	55%	62%	77%
-37.35 17.74 -5.31 -52.59 119.12 37.32 NA -4%	3/90LBM 22 +	e birke	629.73	510.06	549.36	507.53	450.56	375.92	40%	43%	51%
880.00 880.00 880.00 880.00 880.00 880.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55% 1355.48 1124.29 1204.26 1143.25 1096.43 837.02 52% 688.4 631.97 649.59 583.13 764.99 498.42 NA 72% 74% 66% 87% 57% NA	Porces Decover	<b>.</b>	-37.35	17.74	-5.31	-52.59	119.12	37.32	Y Y	¥	AN AN
880.00 880.00 880.00 880.00 880.00 NA 667.08 492.32 554.67 560.12 331.44 338.60 55% 1355.48 1124.29 1204.26 1143.25 1096.43 837.02 52% 688.4 631.97 649.59 583.13 764.99 498.42 NA 72% 74% 66% 87% 57% NA	Leiceil newy	<u>.</u>	- 4%	* %	-1%	. %9-	13%	4%	¥ N	AN.	¥
667.08 492.32 554.67 560.12 331.44 338.60 55% 1355.48 1124.29 1204.26 1143.25 1096.43 837.02 52% 688.4 631.97 649.59 583.13 764.99 498.42 NA 78% 72% 74% 66% 87% 57% NA	Amount Spiked		880.00	880.00	880.00	880.00	880.00	880.00	Ą	<b>AN</b>	
1355.48 1124.29 1204.26 1143.25 1096.43 837.02 52% 688.4 631.97 649.59 583.13 764.99 498.42 NA 72% 74% 66% 87% 57% NA	379GLBR-22	07OCT1:521SDO	667.08	492.32	554.67	560.12	331.44	338.60	55%	82%	/9/./
688.4 631.97 649.5 <b>9</b> 583.13 764.99 498.42 NA 78% 72% 74% 66% 87% 57% NA	379GLBR*22 + S	Spike DUPLICATE	1355.48	1124.29	1204.26	1143.25	1096.43	837.02	£2%	8 70 C	2 700
78% 72% 74% 66% 87% 57% NA	Amount Recover	pe,	688.4	631.97	649 50	583 13	764.00	20.100	• 7C	<b>8</b> :	82%
,6% /2% /4% 66% 87% 57% NA	Percent Remove		/00/	) OC F	9.51	500	70+0A	498.42	Ž	¥ Z	¥
		•	<b>9</b> / <b>0</b> /	121	/4%	%99	87%	27%	¥	¥	¥

U - Detected below detection limit
- Recoveries outside of QC limits.
NA - Not applicable.
NC - Not certified.

(CF #379) BUFFALO RIVER PILOT PROJECT PAH ANALYSIS IN SEDIMENT SAMPLES (ANALYZED 10/91)

		(Concentrations in ng/	(g/gu uj si					5 %	% Surrogate Becovery
MSL CODE	SPONSORID	Benzo(b)· Benzo(k)· Fluoranthene Fluoranthene	Benzo(k)- Fluoranthene	Benzo(a) Pyrene	Indeno(1,2,3) Pyrene	Indeno(1,2,3) Dibenzo(a,h) Benzo(g,h,i) Pyrene Anthracene Perylene	Benzo(g,h,l) Perylene	D8 Naph D10 Acenaph- thalene thalene	0 Acenaph- thalene D12 Perviene
REPLICATE ANALYSIS	ALYSIS				j e				
379GLBR*15A 379GLBR*15B 379GLBR*15C	07OCT1211SCO 07OCT1211SCO 07OCT1211SCO RSD%	627.45 644.37 580.88 5%	434.19 454.13 425.19 3%	542.81 560.96 521.53	438.57 453.05 426.39	103.80 114.59 106.08	280.39 287.02 272.14	42% 36% • NA % •	48% 64% 50% 67% 50% 69% NA NA

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Fluoran- thene		8792	10929	16751	63737 D	37865 D		35555	25 U		93778 D		22030	14753 D		18615 D				1/4/9	40218	33314	24642	19474	80	27038	81464 E
Anthra- cene		15925	16862	18271	26274	11386	20580	39225	38 0		30532	239 #	6544	2759	1959	5948	14514			1440/	22973	9728	6750	5246	23 U	7011	25842
Phenan- threne		86591 D	104808	110202	111982 D	55951 D	95140 D	189784 D	36 U		114021 D		29804	32600 D	27611 D	29132 D	67219 D			03440 D	120301	44081	30611	23532	110	25498	91406 E
Flourene		37080 #	35122	32308	33598	12339	22862	64326	67 U		22981	2242	7796	8099	5939	5784	12089		30000	23023	28310	1669	5291	4018	33 N	4305	18667
Acenaph- thene		15805#	14358	12181#	9611 #	# 0268	7019#	19760 #	62 U		7333 #	926 *	2273#	2000 #	1896#	2198#	4294#		7161 #	* *	* 1940	2801 #	2271#		36 U	1697	8325
Acenaph- thylene		2361	2289	3069	4679	1751#	3277 #	9204	46 U		5964	125 #	2714	202	155	2084	3789		2691	3444	* * * * * * * * * * * * * * * * * * * *	/0/1	1504	1294	27 U	1358	2368
Naph- thalene		134123	106763	39236	43851	24162	36540	38413	43 U		27983	10474	18845	13540	11561	14293	21054		18313	20680	60004	5000	0110		80 B	5181	9430
Sponsor ID	BIN A	21OCT6:1810LA10	210C16:2010LA10	230C14:459LA20	230C15:2010LA20	250CT10:1810LA30	250C110:1910LA30	250CT9:549LA30	30OC14:206LA30	BIN B	25OCT3:0810LB1O	310CT10:119LB20	310CT10:2310LB20	310CT3:119LB30	310C13:109LB30	310C 13:0110LB30	31OC 13:0010LB3O	BINC	18NOV5:559LC10	19NOV5-509I C20	19NOV5-05101 C2O	19NOVE:05401 C20	19NOV5:0510LC2O	19NOV5:0510LC20	20NOV2:193LC3O	ZONOVZ:4Z9LU3U	20NOV3:0110LC3O
MSL Code		_	3/9GLBH-9/ ~	3/9GLBH-128	3/9GLBH-132	3/9GLBH-160	3/9GLBH-161	3/9GLBH-164	3/9GLBH-204		379GLBR-187	379GLBR-226	379GLBR-227	3/9GLBH-252	3/9GLBH-253	3/9GLBH-256	3/3GLBR-23/		379GLBR-286	379GLBR-326	379G( BR-331 Ren 1			370G1 00 264	370G1 BD 366	37 30LDN-388	3/3GLBH-3/0

(Concentrations in ng/L)

MSL Code	Sponsor ID	Pyrene	Benzo[a]- anthracene	Benzo(b)- Chrysene Fluoranthene		Benzo(k)- Fluoranthene	Benzo(a)- pyrene	Indeno [1,2,3-cd]- pyrene	
	BIN A							·	
379GLBR-97	210CT6:1810LA10	33900 D	11082	33172 D	8935	21 U	13481 #	1451	
379GLBR-97 ~	210CT6:2010LA10	39571	11015	40731	8966	84 U	13156	1169	
379GLBR-128	230CT4:459LA20	49386	17602	39751	10321	153 U	11148	1104	1.
379GLBR-132	230CT5:2010LA20	64875 D	24528	50826	32041	51 U	16437	4268	
379GLBR-160	250CT10:1810LA30	37935 D	12637	28396 D	31 U	10940	8325	2174	
379GLBR-161	250CT10:1910LA30	62018 D	19820	45983 D	38	17677	13742	3389	
379GLBR-164	250CT9:549LA30	94035 D	38129	77380 D	32084	37 U	28968	5098	
379GLBR-204	300CT4:206LA30	26 U	30 U	25 U	24 U	17 U	24 U	J 22 U	_
	BIN B								
379GLBR-187	25OCT3:0810LB10	71800 D	18980	30291 D	32 U	14581	7690	2579	
379GLBR-226	310CT10:119LB20	2328	603	1561	611	24 U	212	80	
379GLBR-227	310CT10:2310LB20	15136	5037	7478	6273	24 U	1585	614	
379GLBR-252	310CT3:119LB30	13079 D	3456	9659	3147	<b>∩</b> 6	1020	266	
379GLBR-253	310CT3:109LB30	10912 D	2989	5688	2684	80	972	225	
379GLBR-256	310CT3:0110LB30		4293	6228	3304	1580 #	1466	969	\
379GLBR-257	310CT3:0010LB30	35469 D	11296	17116	8869	21 U	3867	1517	
	BINC								
379GLBR-286	18NOV5:559LC10	39512 D	14062	30385 D	10454	22 U	8401	1369	
379GLBR-326	19NOV5:509LC2O	63531	23436	46161	18852	N 96 U	13019	2202	
379GLBR-331, Rep 1	19NOV5:0510LC20	28145	7718	13840	6160	2558	3801	1260	** <sub>1</sub>
	19NOV5:0510LC2O	20062	5570	9516	4514	2063	2425	925	
379GLBR-331, Rep 3	19NOV5:0510LC20	15593	4340	7121	3824	1461	1911	716	
379GLBR-361	20NOV2:193LC3O	89	18 U	31	17#	10 U	14 U	130	
379GLBR-366	20NOV2:429LC3O	21804	6941	10309	9689	Π 69	2958	1128	
379GLBR-370	20NOV3:0110LC3O	62530 E	17229	24776	14282	5931 #	6370	3062	

		D12- Perylene			27%	33%	23%	24% •	25%	48%	34%	83%		/65/3	* 200	31%	* %60	30%	32%	. %82	31 31 •	33%	27%	<b>36%</b>	37%	34%	38%	29%	32%
	% Surrogate Recovery	naphthalene			31%	. %62	22%	21%	23%	20%	28%	81%		9	* % * C	31%	33%	32%	30%	. 78%		31%	22%	. %62	33%	33%	31%	. %08	31%
	S %	Naphthalene			53%	50%	12%	16%	43%	41%	• %6	82%		%89	16%	24%	24% •	22%	21%	21%		16%	12%	50%	27%	24%	. 78%	18%	21% •
		·																											
s in ng/L)	Banzolobil	perylene			6622	7315	7981	7772	4423	6602	16790	27 #		3648	208	602	523	528	610	1525		5736	8312	1873	1223	882	118	1278	3062
(Concentrations in ng/L)	Dibenzo[a.h].	anthracene		3	3323 #	3229	2086#	3406#	1960#	3413#	£963 #	21 O		1616#	#89	211	188#	<b>#</b> 061	213	543		1702#	2373#	# 889	428#	261#	12 U	426	266
	Õ	Sponsor ID	BIN A	010 T8:1810	STOCIE: ISTOLATO	210C16:2010LA10	230CT4:459LA20	230CT5:2010LA20	250CT10:1810LA30	250C110:1910LA30	250C19:549LA30	300C14:206LA30	BIN B	25OCT3:0810LB1O	31OCT10:119LB2O	310CT10:2310LB20	31OCT3:119LB3O	31OCT3:109LB3O	310CT3:0110LB30	310C13:0010LB30	BINC	18NOV5:559LC10	19NOV5:509LC20	19NOV5:0510LC20			20NOV2:193LC30	20NOV2:429LC3O	20NOV3:0110LC3O
		MSL Code		379GI BB-07	370C1 BB 07 •	3/9GLBR-9/	3/9GLBH-128	379GLBR-132	379GLBH-160	3/9GLBR-161	3/9GLBH-164	3/30LBH-204		379GLBR-187	379GLBR-226	379GLBR-227	379GLBR-252	379GLBR-253	3/9GLBH-256	3/ 3GLBH-23/		379GLBR-286		ж ф (	д ф	3/9GLBH-331, Rep 3	379CLBH-361	3/9GLBH-366	3/9GLBH-3/0

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Fluoran- thene	15163	; ;	32	29 U		6410	63737 D	39157 -24580	-383%	7143	63737 D	71703	9962	112%
Anthra- cene	3992		16 U	44 U		6410	26274	16648 -9626	-150%	7143	26274	28647	2373	33%
Phenan- threne	19280 36954		34	41 U		6410	111982 D	68000 -43982	- %989-	7143	111982 D	126052 E	14070	197%
Flourene	4039		24 U	65 U		6410	33598	20300 -13298	-207%	7143	33598	34056	458	• %9
Acenaph- thene	1796#		26 U	70 U		6410	9611 #	6324 # -3287	-51%	7143	9611#	11133	1522	21%
Acenaph- thylene	819 2106		19 U	53 U		6410	4679	3869 -810	-13%	7143	4679	6735	2056	. %62
Naph- A thalene	5543 4211		30 B	82		6410	43851	-20212	-315%	7143	43851	48960	5109	72%
Sponsor ID	BIN D 21NOV3:2610LD10 21NOV4:169LD10	DILUTION WATER	6NOV12:003LO		ESULTS (1)		230CT5:2010LA20				230	pike DUPLICATE		
MSL Code	379GLBR-398 379GLBR-404		379GLBR-275	BLANK	MATRIX SPIKE RESULTS (1)	Amount Spiked	379GLBR-132	Amount Recovered	Percent Recovery	Amount Spiked	379GLBR-132	3/9GLBH-132 + Spike	Amount Recovered	Percent Hecovery

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MSL Code	Sponsor ID	Pyrene	Benzo[a]- anthracene	E Chrysene Fluo	Benzo(b)- Fluoranthene Fl	Benzo(k)- Fluoranthene	Benzo[a]- pyrene	Indeno [1,2,3-cd]- pyrene	
	BIN D								
379GLBR-398 379GLBR-404	21NOV3:2610LD10 21NOV4:169LD10	12281 30273	3051 9684	5001	4089 7395	57 3751	1097	537 1217	
	DILUTION WATER								
379GLB R-275	6NOV12:003LO	65	13 U	6	10 U	7 U	10 01	Ue.	
BLANK		30 U	34 U	29 U	27 U	20 U	27 U	25 U	
MATRIX SPIKE RESULTS	21.								
Amount Spiked		6410	6410	6410	6410	6410	6410	6410	
3/9GLBH-132	230C15:2010LA20	64875 D	24528	50826	32041	51 U	16437	4268	
3/3/GLBH-132 + SpiKe		40044	154397	30532	13969	5378	10568	3727	
Amount Recovered		-24831	129869	-20294	-18072	5378	-5869	-541	
Percent Hecovery		-387%	5026%	-317%	-282%	84%	-95%	-8%	
Amount Spiked		7143	7143	7143	7143	7143	7143	7143	
3/9GLBH-132	2300	64875 D	24528	5082 <b>6</b>	32041	51 U	16437	4268	
3/9GLBH-132 + Spike	DUPLICATE	71305	25861	53761	23306	10431	16661	6394	
Amount Hecovered		6430	1333	2935	-8735	10431	224	2126	
Percent Recovery		<b>%</b> 06	19%	41%	-122%	146%	• %	. %0€	

		(Concentrations in ng/L)	ns in ng/L)	٠			
					%	% Surrogate Recovery	
		Dibenzo[a,h]-	Benzo[ghi]		-8Q	D-10 Ace-	D12-
MSL Code	Sponsor ID	anthracene	perylene		Naphthalene	naphthalene	Perylene
		ſ					
	BIND	· ¬					
379GLBR-398	21NOV3:2610LD10	210	521		. %92	. %62	24% •
379GLBR-404	21NOV4:169LD10	386	1201		• %8	15%	13%
	DII IITION WATED						
379GLBR-275	6NOV12:003LO	Π 6	108		21%	28%	38%
							•
BLANK		24 U	33		61%	64%	%29
MATRIX SPIKE RESULTS	LTS						
Amount Spiked		6410	6410		\$	\$	¥
379GLBR-132	230CT5:2010LA20	3406#	7772		16%	21%	24%
379GLBR-132 + Spike	•	3654	5550		14%	21%	24%
Amount Recovered		248	-2222		¥	¥	¥
Percent Recovery		4%	-32%		<b>\S</b>	<b>X</b>	¥
Amount Spiked		7143	7143		V.	\$	<b>.</b>
379GLRB-132	230CT5-20101 A20	3406	2777		\$ \displays \dis	\$ 200 de 1	£ ;
07 50E EDIT 10E		# 00+0	7///		. %91	21%	. 54%
3/96LBH-132 + Spike	DUPLICALE	5462	9791		18%	23%	. 72%
Amount Recovered		2056	2019		₹	₹	¥
Percent Recovery		59%	28%		Ş	NA V	¥

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Fluoran-		33314 24642 19474 27%
Anthra-		9728 6750 5246 32% • •
Phenan- threne		44081 30611 23532 32% • •
Flourene		7669 5291 4018 33% • •
Acenaph- thene		2801# 2271# 1920
Acenaph- thylene		1707 1504 1294 14%
Naph- thalene		5689 6110 5821 4%
Sponsor ID		19NOV5:0510LC2O 19NOV5:0510LC2O 19NOV5:0510LC2O RSD %
MSL Code	REPLICATE ANALYSIS	379GLBR-331, Rep 1 19NOV5:0510LC2O 379GLBR-331, Rep 2 19NOV5:0510LC2O 379GLBR-331, Rep 3 19NOV5:0510LC2O RSD %

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indeno 2,3-cd]- pyrene		260	925	716	28% • •
Ë		•			•
Benzo[a]- pyrene		3801	2425	1911	36%
		2558	2063	1461	27%
)- B ne Fluo		. 09	4	24	52% • •
Benzo(b		61	4514	3824	25
Benzo(b)- Benzo(k)- Chrysene Fluoranthene		13840	9516	7121	34%
Benzo[a]- anthracene C		7718	5570	4340	29%
Pyrene a		28145	20062	15593	30%
Sponsor ID		379GLBR-331, Rep 1 19NOV5:0510LC2O	379GLBR-331, Rep 2 19NOV5:0510LC2O	379GLBR-331, Rep 3 19NOV5:0510LC2O	RSD %
	VALYSIS	Rep 1	Rep 2	Rep 3	•
MSL Code	REPLICATE ANALYSIS	379GLBR-331,	379GLBR-331,	379GLBR-331,	

#### Page 3c

### BUFFALO RIVER PILOT PROJECT (#379) PAH ANALYSIS IN WATER SAMPLES

(Concentrations in ng/L)

				%	% Surrogate Recovery		
_	Dibenzo[a,h]- Benzo[ghi]	Benzo[ghi]		-80	D-10 Ace-	D12-	
Sponsor ID	anthracene	perylene		Naphthalene	naphthalene	Perylene	
			•				,
REPLICATE ANALYSIS							
	:						
3/9GLBH-331, Hep 1 19NOV5:0510LC2O	<b>688</b>	1873		. %02	. %62	• %9E	
379GLBR-331, Rep 2 19NOV5:0510LC20	428#	1223		27%	33%	37%	•
379GLBR-331, Rep 3 19NOV5:0510LC2O	261#	882		24%	33%	34%	
RSD %	47%	38%		AN	AN	¥X	

U - Detected at or below detection limit.

B = Naphthalene and Benzo(ghi)perylene were detected at levels near detection limits.

~ = Field replicate.

# = Indicates confirming ion out of specification.

D = 10:1 sample dilution.

E - Indicates value outside of calibration.

RSD % - Relative standard deviation.

• - Recoveries exceed laboratory control limits (40-120%).

- Value exceeds precision goal of 20%.

MSL Code	Sponsor ID	Naph- thalene	Acenaph- thylene	Acenaph- thene	Flourene	Dibenzo- thiophene	Phenan- threne	Anthra- cene	Fluoran- thene
	BIN A								
379GLBR-13	07OCT12:341SAO	73	34	35	64	34	437	96	1101
379GLBR-16	07OCT2:401SAO	62	34	36	6.4	43	475	95	1160
379GLBR-57	09OCT11:502SA3O	102	42	52	80	42	552	120	1363
379GLBR-58	09OCT11:382SA2O	99	46	66	138	67	948	180	1731
379GLBR-59	09OCT11:282SA1O	29	31	39	69	39	473	104	1169
379GLBR-104	220CT11:317SA10	573	29	162#	260	1884	2716	373	. 2271
379GLBR-107	220CT11:378SA10	126	16	25#	102	167	593	141	1448
379GLBR-108	220CT4:203SA20	35	35	43	8	4 4	809	118	1326
379GLBR-111	220CT5:563SA20	158	88	109	160	82	1166	230	2726
379GLBR-111-R	220CT5:563SA20	36 (	J 44	53 U	4 6	32	446	66	978
379GLBR-113	230CT1:303SA20	65	33	40	59	38	462	91	1114
379GLBR-122	230CT4:284SA20	24	4	0 / I	0 S	4	21	4	14
379GLBR-122-R	230CT4:284SA20	45	3 -	8 ∪	<b>O</b> 9	15	38	4	20
379GLBR-123	230CT4:274SA20	39	7 6	13 U	100	G	29	Π9	21
379GLBR-124	230CT4:294SA20	47	4	J 7 U	g	<b>60</b>	34	7	26
379GLBR-124-R	230CT4:294SA20	61	<b>ກ</b> 9	110	0 V	.21	64	7	59
379GLBR-136	240CT10:457SA20	221	13	70	198	476	832	137	999
379GLBR-139	24OCT10:508SA2O	275	14 U	31#	97	218	405	65	250
379GLBR-141	24OCT2:203SA3O	23 (	1 49	38	26	36	543	82	1162
379GLBR-143	24OCT5:503SA3O	44	34	45	62	4	605	82	1308
379GLBR-145	24OCT6:203SA3O	9	29	46	29	39	453	80	1060
379GLBR-151	250CT9:224SA30	25	<b>∩9</b>	100	0 V	6	101	17	198
379GLBR-152	250CT9:224SA30	27	<b>⊃</b> 8	14 U	12	15	180	24	400
379GLBR-153	250CT9:214SA30	6	0 V	12 U	10 U		109	17	263
379GLBR-166	250CT9:307SA30	36	14	18	4 8	72	540	110	1890
379GLBR-167	250CT9:368SA30	33	<b>∩ 8</b>	15 U	18	28	187	38	584

MSL Code	Sponsor ID	Pyrene	Benzo[a]- anthracene	Chrysene	Benzo(b)- Fluoranthene	Benzo(k)- Fluoranthene	Benzo[a]- pyrene	Indeno [1,2,3-cd]- pyrene	
	BIN A								ı
379GLBR-13	07OCT12:341SAO	792	409	553	612	4 85	497	370	
379GLBR-16	07OCT2:401SAO	827	394	583	677	479	501	391	
379GLBR-57	09OCT11:502SA3O	962	483	629	790	521	519	449	
379GLBR-58	09OCT11:382SA2O	1220	638	767	987	658	634	545	
379GLBR-59	09OCT11:282SA10	845	410	569	663	458	471	376	
379GLBR-104	220CT11:317SA10	3071	1933	3326	2920	7 4	1821	657	
379GLBR-107	220CT11:378SA10	1114	888	1277	1740	# 000	972	749	
379GLBR-108	22OCT4:203SA2O	937	489	609	772	537	503	433	
379GLBR-111	220CT5:563SA20	1863	918	1335	1528	1022	845	816	
379GLBR-111-R	220CT5:563SA20	737	339	487	507	373	372	294	
379GLBR-113	230CT1:303SA20	805	433	585	680	476	447	372	
379GLBR-122	230CT4:284SA20	9	3 U	80	4	2 U	<b>Π</b> ε	2.0	
379GLBR-122-R	230CT4:284SA20	<b>1</b>	α	17	19	2 U	4	) 1 m	
379GLBR-123	230CT4:274SA20	15	o	15	=	* 50	4	) m	
379GLBR-124	230CT4:294SA20	19	10	21	19	2 0	) D	۰ ۵	
379GLBR-124-R	230CT4:294SA20	46	21	41	52	<u>∩</u> €	10	. ~	
379GLBR-136	240CT10:457SA20	620	381	610	744	340 #	337	302	
379GLBR-139	24OCT10:508SA2O	246	139	263	361		119	71	
379GLBR-141	24OCT2:203SA3O	788	360	589	676	496	368	698	
379GLBR-143	24OCT5:503SA3O	906	429	703	828	611	408	443	
379GLBR-145	24OCT6:203SA3O	777	367	521	629	477	459	362	
379GLBR-151	250CT9:224SA30	136	73	124	200	7 C	46	1 (C)	
379GLBR-152	250CT9:224SA30	248	148	267	326	218	96	151	
379GLBR-153	250CT9:214SA30	173	104	166	206	135	\$6		
379GLBR-166	250CT9:307SA30	1273	812	1155	1289	747 #	614	428	
379GLBR-167	250CT9:368SA30	380	350	536	783	424	306	240	

				_		Sur	% Surrogate Recovery		
MSL Code	Sponsor ID	Dibenzo[a,h]- anthracene	Benzo[ghi] perylene		d8 Naph- thalene	d10 Acena- phthene	D10- Fluorene	D14 Dibenzo- (a,h)Anthracene	
	BIN A								
379GI BB-13	07OCT12:341SAO	141	358		7%	73%	%66	131%	
379GLBR-16	07OCT2:401SAO	150	368		62%	<b>%99</b>	%96	132%	
379GLBR-57	09OCT11:502SA3O		397		<b>%</b> 06	72%	103%	129%	_
379GLBR-58	09OCT11:382SA2O		480		81%	48%	%16		
379GLBR-59	09OCT11:282SA1O	151	316		54%	54%	%98	116%	
379GLBR-104	220CT11:317SA10	501#	1269		52%	. 72%	88%	%26	
379GLBR-107	220CT11:378SA10	335	798		64%	34%	81%	102%	
379GLBR-108	220CT4:203SA20	124	385		. %68	. 792	, 79%	94%	
379GLBR-111	220CT5:563SA20	330	582		42%	, %96	. 15%	<b>8</b> 8%	
379GLBR-111-R	220CT5:563SA20	74	294		33%	72%	<b>65%</b>	91%	
379GLBR-113	230CT1:303SA20	150	364		43%	41%	75%	93%	
379GLBR-122	230CT4:284SA20	3 6	J 2 U		24%	• %6	. 52%	4%	
379GLBR-122-R	230CT4:284SA20	8	ო		%19	73%	75%	21%	
379GLBR-123	230CT4:274SA20	) E	4		<b>%89</b>	32%	*08	15%	
379GLBR-124	230CT4:294SA20	) E	5		. %66	, %92	. 63%	25%	
379GLBR-124-R	230CT4:294SA20	4	7		71%	%08	73%	34%	
379GLBR-136	240CT10:457SA20	140	314		20%	45%	74%	82%	
379GLBR-139	24OCT10:508SA2O	42	83		80%	71%	83%	82%	
379GLBR-141	24OCT2:203SA3O	123	345		• %4	48%	%69	%96	
379GLBR-143	24OCT5:503SA3O	163	399		23%	20%	82%	110%	
379GLBR-145	24OCT6:203SA3O	26	363		<b>%</b> 86	%68	%16	111%	
379GLBR-151	250CT9:224SA30	17	30		74%	%08	77%	41%	
379GLBR-152	250CT9:224SA30	29	135	•	%19	54%	81%	%06	
379GLBR-153	250CT9:214SA30	44	82		. %41	54%	72%	%92	
379GLBR-166	25OCT9:307SA3O	162	441		29%	%89	78%	%66	
379GLBR-167	250CT9:368SA30	96	239		61%	%29	19%	%88	

995GLBH-14 07CCT1-1018B0 79 57 34 64 38 425 108 1182 379GLBH-65 09CCT1-2015BO 199 46 41 87 49 593 123 1447 1172 179GLBH-65 09CCT1-2015BO 199 46 41 87 49 593 123 1447 1172 179GLBH-67 09CCT1-2015BO 153 39 62 91 56 610 117 1172 179GLBH-67 09CCT1-2015BBO 155 39 62 91 56 610 117 1172 179GLBH-67 09CCT1-2015BBO 156 37 64 9 16 62 125 125 1379 179GLBH-176 25CCT2-2045BIO 23 61 10 12 U 12 U 14 17 146 19 19 19 19 19 19 19 19 19 19 19 19 19	MSL Code	Sponsor ID	Naph- thalene	Acenaph- thylene	Acenaph- thene	Flourene	Dibenzo- thiophene	Phenan- threne	Anthra- cene	Fluoran- thene	
OYOCTI-0101SBO         79         57         34         64         38         425         108         1147           OWOCTI-011SBO         199         46         41         87         49         593         123         1447           OWOCTI-011SBO         195         46         41         87         49         564         144         172           OWOCTI-012SBSO         15         37         64         79         46         562         125         1379           250CT2-24SB10         76         32         49         68         42         425         181         957           250CT2-24SB10         23         49         74         47         564         106         124           250CT2-24SB10         27         70         12 U         16         14         144         38         36         274           40         250CT2-24SB10         26         11U         27         144         33         36         27         46         47         456         106         48         37         48         47         47         48         47         47         48         47         48         47         48		BIN B									
OFOCTIONISBO         109         46         41         87         49         593         123         1447           09OCTIO-1828BO         53         33         55         87         55         550         117         1172           09OCTIO-1828BO         115         38         62         87         56         66         125         137           25OCT2-1838BO         76         32         49         68         42         425         81         574           25OCT2-1838BO         23         49         68         42         425         81         104           25OCT2-2948BO         23         49         68         74         47         564         106         114           90 2         25OCT2-2948BO         22         110         12 U         16         14         136         27           90 2         25OCT2-2948BO         22         110         12 U         16         14         14         14         14         14         14         16         14         17         14         14         14         14         14         14         14         14         14         14         14         14	379GLBR-14	07OCT1:101SBO	79	57	34	64	38	425	108	1182	
90CT19542SB10         53         33         55         87         55         550         117         1172           99CT10:152SB2O         135         38         62         91         56         640         148         155           99CT10:32SB10         76         32         49         68         42         425         81         197           25CT12:35SB10         70         32         49         74         47         564         106         1245           25CCT2:254SB10         23         8         10 U         27         144         33         38         418           9p 2         25CCT2:254SB10         25         11 U         10 U         68         21         144         146         18         27           4p 2         25CCT2:254SB10         26         11 U         12 U         14         143         36         27           4p 2         25CCT2:254SB10         50         11 U         12 U         14         14         35         29           25CCT2:254SB10         50         18         28         101         14         13         29         27           25CCT2:254SB10         50	379GLBR-23	07OCT1:011SBO	109	4 6	4 1	87	4	593	123	1447	
09OCTIO:IFSSB2         135         62         91         56         640         148         1536           26OCTIO:IFSSB3         115         37         64         79         46         564         105         175         1379           26OCTIC:IFSSB10         40         32         49         64         47         564         106         125         1379           26OCTIC:IFSSB10         23         49         64         47         564         106         1245         1376           26OCTIC:IFSSB10         23         8         10U         27         14         338         418         418           pp 1         25OCTIC:2948B10         27         10U         57         16         14         133         35         277           pp 2         25OCTIC:2948B10         26         10U         52 #         16         14         143         35         277           pp 3         25OCTIC:2948B10         26         17         30 #         111         16         14         143         25         27         203         203         204         20         20         20         20         20         20         20         20	379GLBR-65	09OCT9:542SB1O	53	33	55	87	55	550	117	1172	
090CT10:3528130 115 37 64 79 46 562 125 1379 250CT2:254810 76 32 49 68 42 425 81 957 250CT2:254810 23 81 10 0 27 144 338 38 181 957 250CT2:254810 23 8 10 0 27 144 338 38 18 1248 10 0 27 11 0 0 99 2 250CT2:254810 22 11 0 0 99 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	379GLBR-66	09OCT10:152SB2O	135	88	62	16	26	640	148	1536	
250CT2:153SB10         76         32         49         68         42         425         81         957           250CT2:153SB10         40         32         49         74         47         564         106         1245           250CT2:254SB10         27         7 U         12 U         16         14         338         38         418           92         250CT2:294SB10         27         11 U         69 #         21         18         191         35         356           92         250CT2:294SB10         26         11 U         72 #         16         14         143         29         277           90         250CT3:278B10         26         17         30 #         111         116         88         20         203         207         250         203         250         203         203         207         250         203         250         203         250         203         250         203         203         203         203         203         203         203         203         203         203         203         203         203         203         203         203         203         203         203	379GLBR-67	09OCT10:352SB3O	115	37	64	62	46	562	125	1379	
250CT2:153SB10         40         32         49         74         47         564         106         1245           9P 1 250CT2:34SB10         23         8         10 U         27         144         338         38         418           9P 2 250CT2:234SB10         22         11 U         69 #         21         18         191         35         354           9P 2 250CT2:234SB10         26         11 U         72 #         16         14         143         29         277           250CT3:274SB10         26         11 U         72 #         16         14         143         29         277           250CT3:578SB10         26         17         30 #         111         16         88         277         203         259           300CT3:573SB20         44         32         59 #         105         55         727         152         123         99         200CT3:573SB20         49         44         47         47         49         49         203         40         61         44         472         59         40         61         44         472         59         90         300CT4:413SB20         30         46 #         44 </td <td>379GLBR-174</td> <td>250CT12:153SB10</td> <td>92</td> <td>35</td> <td>49</td> <td>68</td> <td>42</td> <td>425</td> <td>81</td> <td>957</td> <td></td>	379GLBR-174	250CT12:153SB10	92	35	49	68	42	425	81	957	
250CT2:2548B10         23         8         10 U         27         144         338         38         418           pp 2         250CT2:2548B10         22         11 U         12 U         16         11         146         18         274           pp 2         250CT2:294SB10         22         11 U         72 #         16         14         143         29         274           pp 2         250CT2:294SB10         26         11 U         72 #         16         14         143         29         274           250CT3:257SB10         65         17         30 #         111         16         88         191         29         277           250CT3:57SB10         65         17         30 #         111         16         887         191         230           250CT3:57SB20         62         31         52 #         74         48         503         91         1123           30CCT3:67SB20         63         42         69         40         424         81         1173           42         59         40         61         41         472         93         892           310CT3:67SB20         63 <td< td=""><td>379GLBR-176</td><td>250CT2:153SB10</td><td>40</td><td>35</td><td>49</td><td>74</td><td>47</td><td>564</td><td>106</td><td>1245</td><td></td></td<>	379GLBR-176	250CT2:153SB10	40	35	49	74	47	564	106	1245	
op 1         250CT2:2945B1O         27         7 U         12 U         16         11         146         18         274           op 2         250CT2:2945B1O         22         11 U         69 #         21         18         191         35         356           op 2         250CT2:2945B1O         26         11 U         58 #         12 U         10         115         19         209           250CT3:275B1O         65         17         30 #         111         116         887         191         201           250CT3:575B1O         65         17         30 #         101         88         942         203         269           250CT3:575B1O         65         17         30 #         105         55         77         152         123           250CT3:575B2O         62         31         52         74         48         503         91         1123           30CT3:575B2O         63         23         40         61         44         472         93           30CT3:575B2O         63         24         46 #         142         142         42         59           30CT3:575B2O         53         24		250CT2:254SB10	23	8	100	27	144	338	38	418	
op 2 SOCT2:294SB10         22         11 U         69 #         21         18         191         35         356           op 3 SOCT2:294SB10         26         11 U         72 #         16         14         143         29         277           250CT2:244SB10         26         17         30 #         111         116         887         191         290         277           250CT3:578SB10         50         18         28         101         88         942         203         259           250CT3:578SB10         50         18         28         105         55         727         152         230           300CT3:573SB20         62         31         52         74         48         503         91         1123           300CT3:573SB20         63         23         40         61         44         472         89           300CT3:573SB20         63         23         40         64         44         472         89           300CT3:573SB20         63         24         40         64         472         89         89           310CT9:27SB20         37         24         46 #         142         142		250CT2:294SB10	27	7 0		16	=	146	18	274	
ep 3         20CI2:2458B10         26         11 U         72 #         16         14         143         29         277           250CI2:2245B10         65         17         30 #         111         16         185         191         209           250CI2:2245B10         65         17         30 #         111         16         887         191         209           250CI3:5725B10         65         18         29         40         16         18         942         203         259           300CI2:493SB20         62         31         52         74         48         503         91         1123           9p 1         200CI3:573SB20         62         34         42         59         40         424         81         153           9p 2         200CI3:573SB20         63         43         268 #         222         147         47         49         173           9p 2         200CI3:573SB20         63         43         268 #         142         44         472         93         892           300CI4:413SB20         63         46 #         142         142         44         47         42         44		250CT2:294SB10	22	110		21	18	191	35	356	
250C12:264SB10         20         10 U         58 #         12 U         10         115         19         20           250C13:527SB10         65         17         30 #         111         116         887         191         2301           250C13:527SB10         65         17         30 #         101         88         203         259         203         259         203         259         203         259         203         259         203         259         203         259         203         259         203         259         203         259         203         259         203         259         203         259         203         259         203         259         40         424         81         1123         301         301         302         259         40         424         81         301 </td <td>Нөр</td> <td>250C12:294SB10</td> <td><b>5</b>6</td> <td>11 C</td> <td></td> <td>16</td> <td><b>*</b></td> <td>143</td> <td>29</td> <td>277</td> <td></td>	Нөр	250C12:294SB10	<b>5</b> 6	11 C		16	<b>*</b>	143	29	277	
250CT3:5278B10         65         17         30 #         111         116         887         191         230           250CT3:5278B10         50         18         28         101         88         942         203         259           90 1         200CT3:5738B10         50         18         52         74         48         503         91         1123           90 2         200CT3:5738B20         62         31         52         74         48         503         91         1123           90 2         200CT3:5738B20         63         43         40         61         44         472         93         892           300CT4:4138B20         63         43         268 #         222         127         2131         429         592           310CT9:26SB20         161         80         150         46 #         142         750         146         1173           310CT9:26SB20         161         80         150         42         53         287         47         420           310CT9:26SB20         16         170         280         220         140         140         170         140         170         140	3/9GLBH-183	250CT2:284SB10	50	10 U	28 *	12 U	10	115	19	209	
250C13:578SB10         50         18         28         101         88         942         203         2599           9p1         300C12:493SB2O         44         32         59 #         105         55         727         152         1239           9p1         200C13:573SB2O         62         31         52         74         48         503         91         1123           9p2         200C13:573SB2O         63         23         40         61         44         472         93         892           9p3         200C13:573SB2O         63         23         268 #         222         127         2131         429         292           300C14:413SB2O         63         43         268 #         142         72         93         892           310C19:027SB2O         161         80         61         142         750         146         1173           310C19:264SB2O         19         170         28 U         22 U         14 U         14         17 U           310C19:264SB2O         18         10         11         10         14 U         14 U         14 U         14 U         14 U         14 U         14 U <td< td=""><td>3/9GLBH-193</td><td>250CT3:527SB10</td><td>65</td><td>17</td><td>* 000</td><td></td><td>116</td><td>887</td><td>191</td><td></td><td></td></td<>	3/9GLBH-193	250CT3:527SB10	65	17	* 000		116	887	191		
30OCT2:493SB2O         44         32         59 #         105         55         727         152         1239           ap 1         20OCT3:73SB2O         62         31         52         74         48         503         91         1123           ap 2         20OCT3:73SB2O         63         42         69         40         424         81         931           ap 2         20OCT3:73SB2O         63         43         268 #         222         127         2131         429         292           30OCT4:413SB2O         63         43         268 #         222         127         2131         429         292           31OCT9:05RSB2O         161         8 U         15 U         42         53         287         47         420           31OCT9:264SB2O         19         17 U         28 U         42         51         14 U         10         11         11         11         11         11         10         11         11         11         11         11         11         11         11         11         11         11         11         11         11         11         11         11         11         11	3/9GLBH-196	250CT3:578SB10	20	18		101	88	942	203		
op 1         200CT3:5738B2O         62         31         52         74         48         503         91         1123           op 2         200CT3:5738B2O         49         29         42         59         40         424         81         931           op 2         200CT3:5738B2O         59         20         40         424         472         93         892           op 3         200CT3:5738B2O         63         43         268 #         222         127         2131         429         2920           30CT9:078B2O         161         80         150         42         53         287         47         420           310CT9:078B2O         161         80         150         140         10         10           310CT9:04SB2O         161         170         280         220         140         14         10           310CT9:24SB2O         18         100         160         10         10         14         4           310CT9:24SB2O         28         40         60         50         15         40         4           310CT9:24SB2O         24         90         150         110         80 <th< td=""><td></td><td>30OC 12:493SB2O</td><td>4</td><td>35</td><td></td><td>105</td><td>52</td><td>727</td><td>152</td><td>1239</td><td></td></th<>		30OC 12:493SB2O	4	35		105	52	727	152	1239	
op 2         200CT3:573SB2O         49         29         42         59         40         424         81         931           op 3         200CT3:573SB2O         59         23         40         61         44         472         93         892           300CT4:413SB2O         63         43         268 #         222         127         2131         429         2920           300CT9:027SB2O         375         24         46 #         142         750         146         1173           310CT9:078SB2O         161         8 U         15 U         42         53         287         47         420           310CT9:264SB2O         19         17 U         28 U         22 U         14 U         17 U         14 U         10           310CT9:264SB2O         18         10 U         11 U         8 U         6 U         19 U         4           310CT9:264SB2O         28         4 U         8 U         6 U         5 U         15 U         4 U           310CT9:254SB2O         24 U         8 U         6 U         5 U         15 U         4 U         4 U           310CT9:244SB2O         24 U         20 U         36 U <th< td=""><td>3/9GLBH-199, Hep 1</td><td>200CT3:573SB20</td><td>62</td><td>31</td><td></td><td>74</td><td>4 8</td><td>503</td><td>91</td><td>1123</td><td></td></th<>	3/9GLBH-199, Hep 1	200CT3:573SB20	62	31		74	4 8	503	91	1123	
ep 3         200CT3:573SB2O         59         23         40         61         44         472         93         892           300CT4:413SB2O         63         43         268 #         222         127         2131         429         2920           310CT9:027SB2O         375         24         46 #         142         750         146         1173           310CT9:027SB2O         161         8 U         15 U         42         53         287         47         420           310CT9:026SB2O         19         17 U         28 U         6 U         11 U         14 U         14 U         10           310CT9:264SB2O         30         6 U         11 U         8 U         6 U         14 U         10           310CT9:264SB2O         28         4 U         8 U         6 U         15 U         14 U         10           310CT9:254SB2O         28         4 U         8 U         6 U         15 U         14 U         4           310CT9:244SB2O         24 U         20 U         36 U         15 U         17 U         19 U         17 U           310CT9:244SB2O         44         9 U         15 U         11 U         10	Нер Г	200CT3:573SB20	49	53	42	59	40	424	81	931	
300CT4:413SB20         63         43         268 #         222         127         2131         429         2920           310CT9:027SB20         375         24         46 #         142         750         146         1173           310CT9:078SB20         161         8 U         15 U         42         53         287         47         420           310CT9:264SB20         19         17 U         28 U         14 U         12 U         14 U         10           310CT9:264SB20         30         6 U         11 U         8 U         6 U         19         5 U         7 U         6           310CT9:254SB20         28         4 U         8 U         6 U         15 U         17 U         19 U         17 U         19 U         17 U         10 U         10 <td< td=""><td>Яер</td><td>200CT3:573SB20</td><td>29</td><td>23</td><td>40</td><td>61</td><td>**</td><td>472</td><td>83</td><td>892</td><td></td></td<>	Яер	200CT3:573SB20	29	23	40	61	**	472	83	892	
310CT9:027SB20         375         24         46 #         142         750         146         1173           310CT9:07SB20         161         8 U         15 U         42         53         287         47         420           310CT9:07SB20         19         17 U         28 U         22 U         14 U         12 U         14 U         10           310CT9:264SB20         18         10 U         16 U         13 U         8 U         6 U         19         5 U         7 U         4           310CT9:254SB20         28         4 U         8 U         6 U         15 U         17 U         19 U         17           310CT9:254SB20         24 U         20 U         36 U         5 U         15 U         17 U         19 U         17           310CT9:24SB20         24 U         20 U         36 U         30 U         17 U         19 U         17           310CT9:24SB20         44         9 U         15 U         11 U         19 U         17           310CT9:24SB20         44         9 U         15 U         19 U         19 U         19 U         10 U	379GLBR-206	300CT4:413SB20	63		268#	222	127	2131	429	2920	
31OCT9:078SB2O         161         8 U         15 U         42         53         287         47         420           31OCT9:264SB2O         19         17 U         28 U         22 U         14 U         12 U         14 U         10           31OCT9:264SB2O         30         6 U         11 U         8 U         6 U         19         7         4           31OCT9:254SB2O         28         4 U         8 U         6 U         5 U         15         4 U         4           31OCT9:254SB2O         28         4 U         8 U         15         4 U         4           31OCT9:24SB2O         24 U         20 U         36 U         17 U         19 U         17           31OCT9:24SB2O         44         9 U         15 U         11 U         8 U         19 U         17           31OCT9:24SB2O         44         9 U         15 U         11 U         19 U         17           31OCT9:24SB3O         35         29         49         56         39         499         96         1005           31OCT1:503SB3O         60         34         36         56         37         426         87         1037 <td< td=""><td>379GLBR-210</td><td>31OCT9:027SB20</td><td></td><td></td><td>46#</td><td>142</td><td>142</td><td>750</td><td>146</td><td>1173</td><td></td></td<>	379GLBR-210	31OCT9:027SB20			46#	142	142	750	146	1173	
310CT9:264SB20         19         17 U         28 U         22 U         14 U         14 U         10 U         14 U         10 U         11 U         8 U         6 U         19         5 U         7 U         6 U         19         5 U         7 U         6 U         10 U         11 U         11 U         10 U         11	379GLBR-213	310CT9:078SB20	161	0 8	15 U	42	23	287	47	420	
31OCT9:264SB2O         30         6 U         11 U         8 U         6 U         19         5 U         7           31OCT9:254SB2O         18         10 U         16 U         13 U         8 U         10         8 U         10         8 U         4 U	3/9GLBH-220	310CT9:264SB20	19	17 U	28 U			12 U		10 U	
-R 310C19:254SB20 18 10 U 16 U 13 U 8 U 10 8 U 6 U 6 U 15 U 4 U 4 310C19:254SB20 28 4 U 8 U 6 U 5 U 15 U 17 U 19 U 17 U 17 U 19 U 17 U 17 U 19 U 17 U 17	3/9GLBH-220-H	310CT9:264SB20	30	<b>∩</b> 9	11 U			19		7	
-H 310C19:254SB20 28 4 U 8 U 6 U 5 U 15 4 U 4 U 310C19:254SB20 24 U 20 U 36 U 30 U 20 U 17 U 19 U 19	3/9GLBH-221	310CT9:254SB20		10 U				10		<b>n</b> 9	
310CT9:245B20 24 U 20 U 36 U 30 U 17 U 19 U 19	3/9GLBH-221-R	310CT9:254SB20	28	∪ 4				15		4	
-R 310CT9:245B20 44 9 U 15 U 11 U 8 U 19 7 U 6 310CT9:245SB30 35 29 49 56 39 499 96 1005 310CT10:453SB30 60 34 36 56 37 426 87 1035 310CT2:303SB30 47 32 103 # 70 49 614 128 1197 310CT2:3845B30 21 12 U 22 # 14 U 16 90 13 166	379GLBH-222	310CT9:244SB20	24 L	20 U	9			17 U		17 U	
310CT10:453SB3O 35 29 49 56 39 499 96 100 310CT11:503SB3O 60 34 36 56 37 426 87 103 310CT2:303SB3O 47 32 103# 70 49 614 128 119 310CT2:384SB3O 21 12 U 22# 14 U 16 90 13 16	379GLBR-222-R	310CT9:244SB20	44	<b>∩</b> 6		11 U		19			
310CT11:503SB3O 60 34 36 56 37 426 87 310CT2:303SB3O 47 32 103# 70 49 614 128 310CT2:384SB3O 21 12 U 22# 14 U 16 90 13	379GLBH-242	310CT10:453SB30	32	29		56	38	499	96	1005	
310CT2:303SB3O 47 32 103# 70 49 614 128 310CT2:384SB3O 21 12 U 22# 14 U 16 90 13	3/9GLBH-243	310CT11:503SB30	09		36		37	426	87	1032	
310CT2:384SB30 21 12 U 22 # 14 U 16 90 13 16	379GLBR-244	310CT2:303SB30	47		103#	70	49	614	128	1197	
	379GLBR-247	310CT2:384SB30	21	12 U		14 U	16	06	13	166	

indeno [1,2,3-cd]- pyrene		544	444		483				168	104		100	98	538	(1)	6	40	6	268	771			5 U	2 0	n e	2 U	10 U	4 U	340	4	378	29
[1,2						;																										
Benzo[a]- pyrene	·	654	564	519	655	585	453	397	196	29		94	58	836	638	510	447	383	343	1058	615	113	<b>∩</b> 8	3 0	2 0	3 0	16 U	5.0	434	423	512	53
Benzo(k)- Fluoranthene		546		511	581	558	416	622	# 681	147	154	137	111	<b>*</b> 696	858	515	457	378	335	1075	738	206#	Π9	3 0	7	2 U	13 U	. O 4	441	441	482	4
Benzo(b)- Fluoranthene F		789	797	723	874	791	596	859	349	243	239	231	176	1873	1386#	683	631	499	470	1364	1340	501	7 U	4	4 U	3 ∪	15 U	5 U	580	605	695	253
B Chrysene Fluo		630	695	583	742	695	480	959	371	187	217	195	151	1584 D	1354	614	517	433	410	1371	863	369	0 Z	2	<b>₹</b>	ന	13 U	2 0	508	200	603	132
Benzo[a]- anthracene (		455	491	451	571	520	347	561	508	86	145	122	87	1162	1001	472	376	322	298	1197	620	230	9 0	4 C	O 9	3 C	14 0	9 C	359	373	463	73
Pyrene		887	1021	898	1128	666	720	872	409	173	254	196	139	1616 D	1848	933	833	969	649	2310	775	258	∩ 6	~	S C	4	15 U	5 U	761	757	902	109
Sponsor ID	BIN B	07OCT1:101SBO	07OCT1:011SBO	09OCT9:542SB1O	09OCT10:152SB2O	09OCT10:352SB3O	250CT12:153SB10	250CT2:153SB10	250CT2:254SB10	250CT2:294SB10	250CT2:294SB10	250CT2:294SB10	250CT2:284SB10	250CT3:527SB10	250CT3:578SB10	30OCT2:493SB2O	200CT3:573SB20	200CT3:573SB20	200CT3:573SB20	300CT4:413SB20	31OCT9:027SB2O	310CT9:078SB20	310CT9:264SB20	310CT9:264SB20	310CT9:254SB20	310CT9:254SB20	310CT9:244SB20	310CT9:244SB20	310CT10:453SB30	310CT11:503SB3O	310CT2:303SB30	310CT2:384SB30
MSL Code		379GLBR-14	379GLBR-23	379GLBR-65	379GLBR-66	379GLBR-67	379GLBR-174	379GLBR-176				379GLBR-182, Rep 3	379GLBR-183	379GLBR-193	379GLBR-196	379GLBR-198			379GLBR-199, Rep 3	379GLBR-206	379GLBR-210	379GLBR-213	3/9GLBH-220	379GLBR-220-R	379GLBR-221	379GLBR-221-R	379GLBR-222	379GLBR-222-R	379GLBR-242	379GLBR-243	379GLBH-244	3/9GLBH-247

						Surre	% Surrogate Recovery	
MSL Code	Sponsor ID	Dibenzo[a,h]- anthracene	Benzo[ghi] perylene		d8 Naph- thalene	d10 Acena-	D10-	D14 Dibenzo-
	BIN B							(a,n/Ammacene)
3/9GLBH-14	07OCT1:101SBO	307	642		75%	<b>%</b> 69	<b>%/0</b>	7
3/9GLBR-23	07OCT1:011SBO	171	401		91%	78%	* 00° F	%271
379GLBR-65	09OCT9:542SB1O	161	386		, ee	% Y Y	%601 7000	145%
379GLBR-66	09OCT10:152SB2O	195	422		87.00 83.00	%C+	<b>%</b> 06	104%
379GLBR-67	09OCT10:352SB3O	182			8 28	\$45 \$4	107%	132%
379GLBR-174	250CT12:153SB10	118	340		84 % % 90 L	% <b>4</b> %	100%	123%
379GLBR-176	250CT2:153SB10	161	0 6		70%	%59	19%	%98 ·
379GLBR-181	250CT2:254SB10	73	000		% 40°	\$4 %	%62	102%
379GLBR-182, Rep 1	250CT2:294SB10	4	60		25%	<b>65%</b>	78%	83%
	250CT2:294SB10		o c		%Z9	45%	78%	<b>%</b> 68
379GLBR-182, Rep 3	250CT2:294SB10	- 0	n c		47%	43%	64%	73%
	250CT2:284SB10	<b>₽ ₹</b>	<b>0</b> 0		<b>%99</b>	<b>62%</b>	78%	87%
379GLBR-193	250CT3:527SB10	7 7 6	0 0		47%	43%	<b>63%</b>	73%
379GLBR-196	250CT3-578SB10	107	600		<b>%99</b>	28%	85%	101%
379GLBR-198	300CT2-493SB20	8/-	444		%69	26%	80%	83%
379GLBR-199, Rep 1	200CT3:573SR20	2.5	B ( )		46%	21%	72%	91%
379GLBR-199, Rep 2	200CT3:573SR20	90	500		87%	73%	94%	105%
379GLBR-199, Rep 3	200CT3:573SB20	90	187		74%	<b>62%</b>	78%	87%
•	300CT4:413SB20	9 4 6	5 0 0 1 0 0		20%	61%	78%	88%
379GLBR-210	310CT9:027SB20	- v	50 Y		54%	20%	75%	82%
379GLBR-213	310CT9:078SB20	9 40	0 0	•	87%	<b>%</b> 9 <i>L</i>	<b>%</b> 96	117%
379GLBR-220	310CT9:264SB20	3	)		%08 *	<b>65%</b>	<b>88%</b>	22%
379GLBR-220-R	310CT9:264SB20	) = (			47%	23%	<b>%</b> 09	2%
379GLBR-221	310CT9:254SB20		) = ) (		% : 2	<b>%</b> 99	<b>%</b> 59	3%
379GLBR-221-R	310CT9:254SB20	9 6	) (		45%	<b>36%</b>	21%	. %/
379GLBR-222	310CT9:244SB20	100	2 :		73%	74%	77%	3%
379GLBR-222-R	310CT9:244SB20	7 4	) = T		• %01	<b>40%</b>	71%	• %S
379GLBR-242	310CT10:453SB30		9 4 6		%//	<b>%</b> 08	75%	• %S
379GLBR-243	310CT11:503SB3O	120	320		40%	<b>39%</b>	%99	<b>%98</b>
379GLBR-244	31OCT2:303SB3O	900	926		74%	64%	85%	101%
379GLBR-247	310CT2:384SB30	60-	# · · ·		49%	48%	71%	95%
	)	9	4		20%	<b>36%</b>	25%	7689

		Signatura de la companione de la compani	, circ								r
Sec. Sec. Sec. Sec. Sec. Sec. Sec. Sec.	Change	<b>4</b>	Acenaph-	Acenaph-	i	Dibenzo-		Phenan-	Anthra-	Fluoran-	
IMSE COOR	Opolisor ID	maiene	thylene	thene	Flourene	Iniophene		Ihrene	Cene	thene	$\neg$
	a Nia										
379GLBR-247-R	31OCT2:384SB3O	45 U	39 U	0 89 0	<b>∩</b> 6	2	,	141	6	171	
379GLBR-248	310CT2:354SB30	21	7 U			· —	· œ	101	) <del></del>	191	
379GLBR-249	310CT2:364SB30	56	15 U	26 U	19 U	_	9	96	13	196	
379GLBR-268	1NOV10:208SB3O	81	9 0	15 U	34	74		364	09	763	
379GLBR-268-R	1NOV10:208SB3O	109	20 U	36 U	38	9.2	,c	450	85	177	
379GLBR-269	1NOV10:157SB3O	84	14	22	61	137		612	107	, 1253	
	BINC										
379GLBR-18, Rep 1	07OCT1:331SCO	147	99	92	147	105		923	264	1938	
379GLBR-18, Rep 2	07OCT1:331SCO.	94	4		96	75			167	1343	
379GLBR-18, Rep 3	07OCT1:331SCO	125	53	91	131	100		835	237	1793	
379GLBR-20	07OCT1:441SCO	105	34	59	101	77		570	143	1245	•
379GLBR-73	09OCT4:562SC10	101	53	97	153	105	:	875	193	1552	
379GLBR-74	09OCT4:352SC20	94	4-	78	105	78		661	164	1397	
379GLBR-75	09OCT4:162SC3O	121	<b>4</b> 8	69	105	73	-	629	151	1444	
379GLBR-280	18NOV2:553SC10	29	4 4	# 59	91	69	_	613	130	1139	
379GLBR-282	18NOV3:503SC10	68	32	72	108	67		269	136	1328	
379GLBH-284	18NOV4:403SC10	113	9	134	173	134		1155	244	1975	
379GLBR-288	18NOV6:1510LC10	115	4	57	128	216		1197	277	4360	
379GLBH-302	19NOV8:594SC10	33	7 U	13 U	11 U	16		86	15	212	
3/9GLBH-303	19NOV9:004SC10	23		18 U		22		125	22	286	
3/9GLBH-304	19NOV9:014SC10	27	11 C	21#	13 U	19	_	86	16	211	
3/9GLBH-30/	19NOV9:238SC10	281	13	# - 4	121	304		199	104	1069	
3/9GLBH-311	19NOV11:303SC2O	109	33	81	118	87		684	144	1334 D	_
3/9GLBH-313	19NOV2:203SC2O	78	<b>4</b>	87	111	88		713	153	1295	
	19NOV3:553SC20	34	29	54	82	67		550	133	1080	
	19NOV4:504SC2O	36	7 U	12 U	10 U	24		128	20	267	
	19NOV4:504SC2O	31	10	10 U	13	28		174	28	379	
379GLBR-323, Rep 3	19NOV4:504SC2O	31	7 U	1 C	<b>∩</b> 6	22		125	20	265	
379GLBR-324	19NOV4:504SC2O	34	12 U	21 U	17 U	56		142	19	229	

		7		٠,																														
	Indeno [1,2,3-cd]-		Q u	ก (	62	70	249	254	595			621	438	283	200	200	0 0	4 3 6	45/	407	9 7 9	4-0	1093	164	117	302	414	413	337	100	137	180	4-1	67
	Benzo[a]-		Ç	3 5	4 I	60	281	286	719			912	601	852	500	330		0 0	000	7/6	936	1664#	<b>*</b> 26	148	102	605	622	290	465	7 7	- 0	9 6	68	70
	Benzo(k)- Fluoranthene		100		- G - F	901	422 #	⊃ æ	# 406			777	513	969	475	634	537	700	200	503	826	101	. <del>4</del>		140	4	542	539	424	1 4	220	174	145	)  -  -
	Benzo(b)- Fluoranthene		262	163	47.	C/-	808	1217	1639			1039	166	1033	200	921	761	794	908	715	1054	4861	383	322	245	1566	764	755	618	484	361	308	245	
	Сһгуѕепе		156	131	18.0	- 1	562	150	1031			957	664	893	634	762	692	704	634	601	666	2446	184	264	199	1175	655	682	526	238	296	240	209	
ns in ng/g)	Benzo[a]- anthracene		87	70	83		360	900	00/			785	528	747	477	615	533	541	467	470	782	1879	101	157	114	633	473	<b>4</b> 0 <b>4</b>	407	131	178	126	113	
(Concentrations in ng/g)	Pyrene		121	116	129	475	U 1		279			1534	1077	1436	972	1211	1073	1098	626	1022	1597	3446	145	205	152		1057 D	1058	843	189	277	180	156	
	Sponsor ID	BIN B	310CT2:384SB30	310CT2:354SB30	310CT2:364SB30	1NOV10-2085B3O	1NOV10-208SB3O	1NOV10-1575B3O	000000000000000000000000000000000000000	BIN C	020040000	0,0011,331300	0.0011:331500	0/0C11:3315C0	0/0C11:441SC0	09OCT4:562SC10	09OCT4:352SC20	09OCT4:162SC3O	18NOV2:553SC10	18NOV3:503SC10	18NOV4:403SC10	18NOV6:1510LC10	19NOV8:594SC10	19NOV9:004SC10	19NOV9:0145C10	10NOV3:2385C1O	19NOV11.3035C2O	19NOV2:2035C2U	19NOV3:5535C2O	19NOV4:504SC20	19NOV4:504SC2O	19NOV4:504SC2O	19NOV4:504SC2O	
	MSL Code		379GLBR-247-R	379GLBH-248	379GLBR-249	379GLBR-268	379GLBR-268-R	379GLBR-269			379G BB.18 B.2	379GI BB-18 Boo 3	379GI BB. 19, 0ep 2		3/ 3GLBR-20	3/9GLBR-/3	3/9GLBH-74	3/9GLBH-75	379GLBR-280	379GLBR-282	3/9GLBH-284	3/9GLBH-288	3/9GLBH-302	379Gi BB 304	379GI BB.307	379GI BB.311	374GI BB.313	379GI BB.316		3/34LBR-323, Rep 1		3/9GLBH-323, Rep 3	3/ 9GLBH-324	

					% Surro	% Surrogate Recovery	
MSL Code	Sponsor ID	Dibenzo[a,h}- anthracene	Benzo[ghi] perylene	d8 Naph- thalene	d10 Acena- phthene	D10- Fluorene	D14 Dibenzo- (a,h)Anthracene
	BIN B						
379GLBR-247-R	310CT2:384SB30	30	62	• %1	131%	25%	%29
379GLBR-248	310CT2:354SB30	31	54	55%	26%	82%	%62
379GLBR-249	310CT2:364SB30	32	65	61%	41%	74%	74%
379GLBR-268	1NOV10:208SB3O	108	224	61%	31%	71%	64%
379GLBR-268-R	1NOV10:208SB3O	116	261	%9/	85%	78%	78%
379GLBR-269	1NOV10:157SB3O	249	571	<b>%0</b> 2	%59	91%	. 111%
	BINC						
379GLBR-18, Rep 1	07OCT1:331SCO	251	602	64%	26%	<b>%</b> 68	123%
	07OCT1:331SCO	179	388	21%	61%	84%	121%
379GLBR-18, Rep 3	07OCT1:331SCO	241	202	72%	<b>%89</b>	<b>%</b> 96	133%
379GLBR-20	070CT1;441SCO	161	345	80%	%69	100%	133%
379GLBR-73	09OCT4:562SC1O	195	475	84%	46%	104%	116%
379GLBR-74	09OCT4:352SC20	176	397	78%	%92	101%	129%
379GLBR-75	09OCT4:162SC3O	183	415	87%	61%	102%	122%
379GLBR-280	18NOV2:553SC10	150	394	29%	48%	79%	83%
379GLBR-282	18NOV3:503SC10	156	368	54%	61%	91%	106%
3/9GLBH-284	18NOV4:403SC10		585	<b>%</b> 59	. %06	87%	86%
3/9GLBH-288	18NOV6:1510LC10	4	1154	%69	<b>63%</b>	85%	124%
3/9GLBH-302	19NOV8:594SC10	4	104	<b>%</b> 06	<b>80%</b>	<b>%66</b>	104%
3/9GLBH-303	19NOV9:004SC10	92	165	<b>62%</b>	43%	<b>46</b>	91%
379GLBR-304	19NOV9:0145C10	25	117	54%	32%	71%	78%
3/9GLBH-30/	19NOV9:238SC10	- - - - -	456	28%	<b>%0</b> /	82%	100%
3/9GLBH-311	19NOV11:303SC20	<u> </u>	407	<b>%96</b>	<b>%68</b>	111%	130%
3/9GLBH-313	19NOV2:203SC2O	152	397	<b>65%</b>	54%	82%	%26
	19NOV3:553SC2O	117	336	37%	46%	80%	101%
	_	54	144	<b>%98</b>	77%	89%	%96
	_	71	189	84%	<b>%9</b> <i>L</i>	91%	101%
379GLBH-323, Rep 3	_	52	146	83%	74%	88%	<b>%</b> 66
3/9GLBH-324	19NOV4:504SC2O	<b>5</b> 2	128	25%	48%	74%	81%

thene		345	0	1076	1585	1102	599		279	735	622 735 2195 D
Cene		24	86	112	175	110	45	56		69	69 290
threne		147	517	553	761	530	268	235		280	280 2295 D
thiophene		<b>8</b>			7.4	50	32	24		ന	32 1219
Flourene		12 U	4 8	88	95		27	20 N	•	17	265
thene		16 U	19	56	69	44	13	26 U	14 U	•	* 69
thylene		0 6	13	39	37	27	12	14 U	15	•	
thalene		17	45	64	23	49	36	<u></u>	6	. 6	326
Sponsor ID	BINC	19NOV4:504SC2O	20NOV8:157SC2O	20NOV11:443SC3O	20NOV1:003SC3O	20NOV1:553SC3O	20NOV3:154SC3O	20NOV3:154SC30	20NOV3:154SC30	000000000000000000000000000000000000000	20NOV3:337SC3O
MSL Code	_	379GLBR-325	379GLBR-337	379GLBR-340	379GLBR-342	379GLBR-344	379GLBH-350	379GLBH-351	3/9GLBH-352	C1 DD 257	379GLBR-357 379GI 88-360

		Some in the supplemental i	16.Ku c						
			Benzo[a]-		Benzo(b)-	Benzo(k)-	Benzo[a]-		Indeno [1,2,3-cd]-
MSL Code	Sponsor ID	Pyrene	anthracene	Chrysene	Fluoranthene	Fluoranthene	pyrene		pyrene
	BINC								
376CI DD 33E	000000000000000000000000000000000000000	0	(						
3/9GLBH-325	19NOV4:5045CZO	208	148	250	305	196	112		160
379GLBH-337	20NOV8:157SC20	886	601	950	1446	# 2773#	682		009
379GLBR-340	20NOV11:443SC3O	851	398	555	616	449	511		335
379GLBR-342	20NOV1:003SC3O	1156	299	728	828	614	596		465
379GLBR-344	20NOV1:553SC3O	808	396	530	618	457	404	:	357
379GLBR-350	20NOV3:154SC30	434	223	378	457	289	255		208
379GLBR-351	20NOV3:154SC3O	448	276	386	476	316	279		261
379GLBR-352	20NOV3:154SC30	528	330	449	554	389	368		314
379GLBR-357	20NOV3:337SC30	2972 D	2064 D	4345 D	3580		2510 D		886
379GLBR-360	20NOV3:278SC3O	315	235	382	533	281			243
	BIN D								
379GLBR-19	07OCT2:041SDO	980	490	672	815	515	592		451
379GLBR-24	07OCT2:121SDO	1000	494	969	830	527	587		444
379GLBR-46	08OCT5:132SD3O	25732 D	13327 D	14210 D	13802	D 11813 D	11 52	_	7382 D
379GLBR-46-R	08OCT5:132SD3O	946	444	620	621	486			
379GLBR-51	08OCT5:402SD1O	7635 D	3449 D	3480 D	5527	D 2849	3303		2363
379GLBR-53	08OCT5:302SD20	7165 D	3517	3367			3564		2233
	21NOV12:003SD10	1078	543	656	802	533	632		451
Яөр	21NOV12:003SD10	824	408	543	652	448	485		376
379GLBR-376, Rep 3	21NOV12:003SD10	860	422	548	657	443	475		374
379GLBR-378	21NOV1:353SD10	4717 D	2147 D	2736 D	2658	D 1901 D	2778 D		1395
379GLBR-380	21NOV2:433SD10	673	332	440	528	351	344		292
379GLBR-384	21NOV5:078SD10	532	481	784	1514	821	504		559
379GLBR-388	21NOV5:107SD10	2867 D	1597 D	2794 D	6742	<b>N</b> 9	1418 #		1386
379GLBR-388-R	21NOV5:107SD10	3297	2155	3345	5641	17 U	1616		1147
379GLBR-395	21NOV5:224SD10	75	52	100	233	G	41		44
379GLBR-396	21NOV5:224SD10	4 8	31	26	09	32	^		7 7
379GLBR-397	21NOV5:224SD10	34	23	46	85	3 U	. <del>4</del>		12
								. · .	<b>!</b>

		Oile complete to	:		% Surre	% Surrogate Recovery	
MSL Code	Sponsor ID	anthracene	Benzolgnij perylene	d8 Naph- thalene	d10 Acena- phthene	D10- Fluorene	D14 Dibenzo-
	BINC			·			
379GLBR-32 <b>5</b>	19NOV4:504SC2O	69	160	<b>707</b>	7007	900	
379GLBR-337	20NOV8:157SC2O	245	631	2 2	e : :	%00	71%
379GLBR-340	20NOV11:443SC3O	110	- 6	/4%	71%	<b>88%</b>	105%
379GI BB-342	20NOV1-0096C2O	9 (	3 to 1	74%	%02	<b>%06</b>	100%
370CLDD 344	2014OV 1.0035C3O	169	447	21%	54%	86%	. 114%
37 30LBn-344	SUNOVI:353SC3O	66	342	49%	45%	74%	%PO
3/9GLBH-350	20NOV3:154SC30	19	225	44.	73%	05%	% <del>**</del> **
379GLBR-351	20NOV3:154SC30	95	251	20%	46%	7.2%	%601
379GLBR-352	20NOV3:154SC3O	115	307	38°C	* 7000	977	%C9
379GLBR-357	20NOV3:337SC3O	661	1960	<b>9</b> 000	%2% 74%	%L8	%16
379GLBR-360	20NOV3-278SC3O	<b>1</b>		9/7/	%!/	95%	131%
	0000017010107	C D	592	<b>64%</b>	<b>%</b> 59	83%	82%
	2 110						
379GI BB.19	070779-0446-DO						
379G1 BB 24	070012:041300	178	412	81%	%29	95%	131%
379C1 BB 46	0/06/2:12/300	165	398	%06	72%	104%	133%
370C1 DD 46 D	08OC15:132SD3O	2276 D	w	87%	65%	%66	%/CC-
37.9GLBH-46-M	08OCT5:132SD3O	92	373	73%	%26	%0a	% <del>* </del>
3/9GLBH-51	08OCT5:402SD1O	978	1997	38%	3.7%	% 60 u	%66 
	08OCT5:302SD20	892	2029	% 5 6	750	% ? <del>*</del>	%99 
3/9GLBR-376, Rep 1	21NOV12:003SD10	164	787	7603		<b>%</b> / :	. %291
379GLBR-376, Rep 2	21NOV12:003SD10	136	363	%0c	% ? %	94%	112%
379GLBR-376, Rep 3	21NOV12:003SD10	134	9 6	18%	45%	77%	106%
379GLBR-378	21NOV1-3535010	- 40	- 60	48%	42%	80%	82%
379GI BB.380	Ordocca: Volum	- BC	200	78%	72%	95%	104%
379GI BB-384	24NOVE:4333D10	5 ( )	281	22%	43%	<b>%98</b>	105%
379GL BB. 300	01/10/07:0785/D10	237	603	75%	71%	88%	128%
379GLDD 388 D	21NOV3:10/2010	293	1538	%99	72%	83%	161%
379GI BB 30E	OLUS/OLISCONIS	521	1273	72%	101%	85%	103%
379GI BB 206	21NOV3:2245D10	23	4 4	%69	%29	84%	%08'
379Cl BD 307	Z1NOV5:2245D10	<b>~</b>	11	25%	32%	73%	40%
20 20 ED - 23/	Z1NOV5:Z245U10	<b>~</b>	œ	20%	. %22	65%	41%

MSL Code	Sponsor ID	Naph- thalene	Acenaph- thylene	Acenaph- thene	Flourene	Dibenzo- thiophene	Phenan- threne	Anthra- cene	Fluoran- thene
Blank-1		57	7 U	12 U	5	11.6	ď	-	
Blank-2		22	20 U	34 U	27 U	18.0	1.5	2 0	• · ·
Blank-3		141	110		16 U	10 0	2 0	2 5	) ;; 
Blank-4		16	12 U		20 U	13 U	1.0	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	) = }
Blank-5		46	⊃ 8	13 U	110	⊃ 8	7	) = 0 0 0	) - «
Blank-H		16		13 U	<b>∩</b> 6	0 Z	9	) ) 9	2 0
Biank-Dijuted		91 U	J 80 U	134 U	N 66	70 U	55 U	70 U	53 0
STANDARD REFERENCE MATERIAL	ENCE MATERIAL								•
SRM-1 (HS-2) (1)		250	157	0.7	ć	Č			
SRM-2 (HS.2)		9 6	5 .	6	802	122	2/20	278	6622
SBM.3 (HS.2)		85.	148	87	175	188	2495	269	5588
(2-CU) C-MUS		92	136	62	177	179	2411 E	243	
(2-CL) + MUS	•	154	123	89	174	172	2181	212	
(2-CL) C-MUC		201	151	78	225	225	2916 E	307	6482 E
	HSD#		10%	18%	12%	12%	11%	14%	* % * * * * * * * * * * * * * * * * * *
		872		44 U	7.8	99	519	785	400
NIST 1941, Hep 2		75 U	140	112 U	46	64	514	193	1097
NO 1941, Nep 3				0 99	64	7.1	574	207	1202
	certified value			<b>V</b>	NAN	¥Z	577	202	1220
							#39	±42	±240

	<i>o)</i>	(Concentrations in ng/g)	s in ng/g)			# # # # # # # # # # # # # # # # # # #	. * . 4 	
MSL Code	Sponsor ID	Pyrene	Benzo[a]- anthracene	Chrysene F	Benzo(b)- Fluoranthene	Benzo(k)- Fluoranthene	Benzo[a]-	Indeno [1,2,3-cd]- ovrene
Blank-1 Blank-2 Blank-3 Blank-4 Blank-5 Blank-R		3 t t 0 t 0 t 8 t 0 t 0 t 0 t 0 t 0 t 0 t	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	2 0 0 0 C C C	2 4 8 4 U A 8 U U A 8 U U A 8 U U A 8 U U U B U U U U U U U U U U U U U U U	5 U 6 U 6 U 7 U 7 U 7 U 7 U 7 U 7 U 7 U 7	3 U & & U & & C & C & C & C & C & C & C &
STANDARD REFERENCE MATERIAL	VCE MATERIAL							•
SRM-1 (HS-2) (1) SRM-2 (HS-2) SRM-3 (HS-2) SRM-4 (HS-2) SRM-5 (HS-2)	RSD%	4121 3513 3501 E 3375 E 4127 E	1800 1568 1642 1447 1770 E 9%	2170 1930 1919 E 1704 E 2217 E	2024 1765 2118 E 1745 2487 E	1415 1510 1506 1404 1798	793 971 973 986 1159	867 779 894 759 925
NIST 1941, Rep 1 NIST 1941, Rep 2 NIST 1941, Rep 3	certified value	938 940 1024 1080 ±200	435 450 488 550 179	590 612 663 NA	825 842 935 780 ±190	611 603 638 444 ±49	457 460 499 670 ±130	453 440 487 140

-							% Surro	% Surrogate Recovery		
	!	<u> </u>	Dibenzo(a,h)-	Benzo[ghi]		d8 Naph-	d10 Acena-	D10-	014	Dibenzo-
MSL Code	Sponsor ID		anthracene	perylene		thalene	phthene	Fluorene	(a,h)Anthracene	racene
Blank-1			4	4		71%	<del>,</del>	84%		160/
Blank-2			7 (			63%	31%	71%		, oc 4
Blank-3			4	4	<b>.</b>	. %!	14%	46%		, 70 8, 20,
Blank-4			7 (	) / (	_	51%	12%	71%		20%
Blank-5			4	J		71%	%29	85%		%96 8
Blank-R			<u>.</u>	3 (	•	72%	81%	79%		%9Z
Blank-Diluted			321	J 28 (		. %0	14% •	40%		48%
STANDARD REFERENCE MATERIA	NCE MATERIAL		•							
SRM-1 (HS-2) (1)			365	850		71%	53%	81%		%16
SHM-2 (HS-2)			295	682		28%	30%	%99		74%
SHM-3 (HS-2)			358	711		46%	29%	79%		95%
SPM-4 (HS-2)			303	653		72%	63%	78%		95%
0HM-5 (HS-Z)			357	896		71%	%89	88%		113%
	• <b>5</b>	HSD%	<b>10%</b>	14%		NA	<b>V</b>	¥.		X X
NIST 1941, Rep 1	, ,		142	463		64%	78%	73%		71%
			139	454		. %	%89	49%		75%
NIST 1941, Rep 3			156	501		• %6	85%	<b>%</b> 99		86%
	certified v	value	Y X	516		¥	AN A	¥ Z		Z Z
	۰		Y Y	183		AN A	¥N	A Z		¥

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			,	77					
MSL Code	Sponsor ID	Naph-	Acenaph-	Acenaph-	i	Dibenzo-	Phenan-	Anthra-	Fluoran-
	2 22	BIBIBI	eu Aireue	Inene	Flourene	thiophene	threne	cene	thene
SPIKE RESULTS						•			
Amount Soiked		167	101						
Blank.4		)	/91	_	167	167	167	167	167
Diak 4 . Call.		9	120		20 U	13 U	110	1311	
Didiin-4 + Spike		120	53	103	133	-8	137		- 1
Amount Recovered		104	53		133			* *	
Percent Recovery		%29	32%		200	10	13/	4 4	187 E
			8 1	<b>9</b> / 70	<b>9</b> 0.2 <b>9</b>	49%	82%	. %92	112%
Amount Spiked		167	167		167			!	•
Blank-5		46	-		3	\ <u>0</u>	16/	167	167
Blank-5+ Spike		2 4	0 (	2 5		⊃ ®	_	⊃ ®	σ,
Amount Becouping		90	139	151	161	146	159	107	186
Doront Hecovered		123	139	151	161	146	152	107	128
reicelli necovery		73%	83%	<b>%</b> 06	<b>%96</b>	87%	91%	76,4	0/-
٠						: ;	5	*	%/01
Amount Spiked		167	167	167	167	167		!	
Blank-5		46	======================================	13.11		3	/o-	16/	167
Blank-5+ Spike	DUPLICATE	8	107		- 6	ב פ	•	n 8	<b>co</b>
Amount Recovered		9 . 5	2 0	8 ·	128	18	130	93	158
Percent Becovery		74	) O I	118	128	118	123	693	150
		75%	64%	71%	11%	71%	74%	26%	%06
Amount Spiked		187	•	,					<b>?</b>
Blank-R			; ·	<b>\9</b>	167	167	167	167	167
Blank-R + Snike		0 0	O /	130	⊃ 6	<b>1</b> 0 2	ø	<b>1</b> 9	= 40
Amount Recovered	·	800	124	141	135	152	166	153	171
Percent Recovery		771	124	141	135	152	160	153	171
		<b>%</b> 5/	/4%	84% %	81%	91%	%96	95%	103%
Amount Spiked		167	167	187					
Blank-R		4	1 2			) o l	167	167	167
Blank-R + Spike	DUPLICATE	137	) v c +		⊃ ຄ	) 1	ဖ	N 9	5 U
Amount Recovered		70.	000		148	158	169	145	176
Percent Recovery		121	133	152	148	158	163	145	176
		9.71	818 81%		<b>%68</b>	95%	%86	87%	105%

		0)	ncentrations in ng/g	111 113	76/							
				ć			ć	ָּבָּ בַּ				ouepul
MSL Code	Sponsor ID		Pyrene	Benzolaj- anthracene	olaj- ene	Chrysene	Benzo(b)- Fluoranthene		Benzo(k)- Fluoranthene		Benzolaj- pyrene	[1,2,3-caj- pyrene
SPIKE RESULTS												•
Amount Spiked			167		167	167	•	167	167		167	167
Blank-4	. *		10 U		10 U		_	∩ 6	<b>~</b>	9 0	10 U	∩ 9 •
Blank-4 + Spike			148 E		130	147		95	186		11 U	121
Amount Recovered			148 E		130	147	_	195	186		110	121
Percent Recovery			102%	-	78%	88%	=	117%	111%	<b>,</b> 0	¥	72%
Amount Spiked			167		167	167		167	167	~	167	167
Blank-5	•		6		က	-		13	7		2 C	S
Blank-5+ Spike			168		150	155		220	210	-	136	117
Amount Recovered			160		145	144		207	203	· •	136	112
Percent Recovery			<b>%</b> 96		87%	%98	12	124%	121%	•	85%	%19
Amount Chilod			167		127	167		167	184			167
Blacks			<u> </u>		·	<u> </u>		5 -			101	) -
Blank-5+ Snike	DUPLICATE		144		134	136		78.	æ	. σ	122	127
Amount Recovered			135		129	125		175	181	· ·	122	123
Percent Recovery		•	81%		71%	75%	9	105%	109%		73%	73%
Amount Spiked			167		167	167		167	167		167	167
Blank-R			5	_	<b>4</b> ∪	4	<b>-</b>	2	n	0 E	4	Ωe
Blank-R + Spike			168		157	159		167	167	7	140	164
Amount Recovered			168		157	159		162	16		140	164
Percent Recovery			100%		94%	82%		%/6	100%	٠,	84%	%86
Amount Spiked			167		167	167		167	9-		167	167
Blank-R			5 U	_	4 )	4	n	S		3 U	4 U	3 U
Blank-R + Spike	DUPLICATE		167		158	161	•-	186	187	7	139	178
Amount Recovered			167		158	161		167	18	7	139	178
Percent Recovery			100%		95%	<b>%</b> 96	7	100%	112%	<b>,</b>	83%	107%

						"Sour	% Surrogate Recovery	
MSL Code	Sponsor ID	Dibenzo(a,h)- anthracene		Benzo[ghi] perylene	d8 Naph- thalene	d10 Acena-	D10-	D14 Dibenzo-
SPIKE RESULTS								and
Amount Spiked			167	167	ΨN	***	2	
Blank-4			7 U	7 11	<u> </u>	<b>₹</b> ?	≨ ;	¥N
Blank-4 + Spike					%10	12%	71%	20%
Amount Recovered			7.7	- T	<b>4</b> 9%	45%	%99	78%
Percent Recovery		•	104%	6	<b>≨</b> :	₹	₹	NA .
			5	<b>%</b> CC	₹	₹	¥	<b>AN</b>
Amount Spiked		•	167	167	AN A	<b>₽</b>	¥¥	
Blank-5			<b>4</b> ⊃	ις ·	71%	%29	\$ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	NA NA
Blank-5+ Spike			170	117	62%	61%	78%	%96 
Amount Hecovered			170	112	Ą	NA NA	%	88%
Percent Recovery		•	102%	%19	<b>₹</b>	<u> </u>	<b>₹ ₹</b>	₹:
4					•		<b>§</b>	<b>&amp;</b> 2
Amount Spiked			167	167	¥	₹	¥.	42
Blank E. Caika			4	က	71%	%29	85%	%90
Amount Descript	DOPLICALE		142	97	31%	21%	75%	85%
Daroont Decovered			142	95	¥	ž	¥ Z	V N
reicelli necovery			82%	22%	Ž	¥	. ≨	C Z
Amount Spiked			167	167	Ą	Ν	¥ X	
Blank-H			ე ც	3 U	72%	81%	<b>7</b> 0%	AN N
Amount Dominged			145	127	71%	82%	83%	%9/ 84%
Percent Boomen			145	127	¥	¥	ž	<b>8</b> 7 7
			%/8	%92	¥ ¥	₹	Ž	¥ Z
Amount Spiked			167	167	Ą	₩.		
Blank-R			ດ ອ	3 C	72%	8 8	<b>5</b> 000	AN S
Blank-H + Spike	DUPLICATE		160	138	70%	83%	/6/ 0E/	%9/
Amount Hecovered			160	138	¥	<b>8</b> 2	% CO	%88 %88
rercent Hecovery		-	<b>%</b> 96	83%	¥	₹	\$ <b>\$</b>	<b>Y</b>
							•	3

MSL Code	Sponsor ID	Naph- thalene	Acenaph- thylene	Acenaph- thene	Flourene	Dibenzo- thiophene	Phenan- threne	Anthra-	Fluoran- thene
SPIKE RESULTS									
Amount Spiked		303	303	303	303	303	303	303	303
379GLBR-111-R	220CT5:563SA20	36 (	1 44	53 U	46	32	446	၉၀	978
379GLBR-111-R + 3	Spike	272	277	314	310	326	767	382	1333
Amount Recovered		262	233	314	264	294	321	289.	355
Percent Recovery		87%	<b>%</b> 22	104%	81%	%26	106%	%96	117%
Amount Spiked		312	312	312	312	312	312	312	312
379GLBR-111-R	220CT5:563SA20	36 (	) 44	53 U	4 6	32	446	6	978
379GLBR-111-R + Spike DUPLICATE	pike DUPLICATE	94	314	396	308	347	1128	426	2111
Amount Recovered		94	270	396	260	315	683	333	1132
Percent Recovery		30%	81%	127%	83%	101%	219%	107%	. %696
Amount Spiked		86	86		86	86	86	80	<b>6</b> 0
379GLBR-247	310CT2:384SB30	21	12 U		14 U	16	06	13	166
379GLBR-247 + Spike	¥e	73	47		69	92	157	54	255
Amount Recovered		25	47		69	09	29	4 1	68
Percent Recovery		23%	48%	170%	<b>%</b> 0 <i>L</i>	61%	%89	45%	91%
Amount Spiked		100	100	100	100	100	100	100	100
379GLBR-247	310CT2:384SB30	21	12 L		14 U	16	06	13	166
379GLBH-247 + Spike	ike DUPLICATE	29	40		63	9.2	139	52	210
Amount Hecovered		46	40		63	09	49	39	4
Percent Hecovery		<b>46%</b>	40%		<b>%</b> E9	%09	49%	38%	44%
Amount Spiked		154	154	154	154	154	154	154	154
	310CT2:384SB30	45 (	) 39 U	U 89	∩ 6	21	141	18	171
	Spike	139	93	131	127	147	261	127	359
Amount Hecovered		139	6	131	127	126	119	109	187
Percent Hecovery		<b>%</b> 06	<b>%</b> 09	85%	85%	82%	77%	71%	122%

S R A + Spik sred ery			anthracene	Chrysene	Fluoranthene	rinoranthene	Dyrene	DATEN
Spik		٠.				£.		
Spik		303	303	303		303	303	303
379GLBR-111-R + Spike Amount Recovered Percent Recovery	220CT5:563SA20	737	339	487	507	373	372	294
Amount Recovered Percent Recovery		1069	643	795		664	643	632
Percent Hecovery		332	304	308		290	270	600
		109%	100%	102%		<b>%</b> 96	89%	112%
Amount Spiked		312	312	312	312	310	310	
379GLBR-111-R 22	22OCT5:563SA2O	737	339	487	507	373	372	200
379GLBR-111-R + Spike DUPLICATE	DUPLICATE	1654	1009	1277	1264	1031	977	8 44
Amount Recovered		916	671	790	757	657	604	550
Percent Recovery		294%	215%	253%	243%	211%	194%	176%
		80	86 *	86	<b>8</b> 0	86	80	œ
	310CT2:384SB30	109	73	132	253	U 4 U	53	29
3/9GLBH-247 + Spike		177	142	207	225	171	20	118
Amount Recovered		89	69	75	-28	171	e-	51
Percent Hecovery		%69	70%	71%	-29%	174%	.3%	52%
		100	100	100	100	100	100	
379GLBR-247 31	310CT2:384SB30	109	73	132	253	4	53	29
3/9GLBH-247 + Spike DUPLICATE	JPLICATE	152	123	174	184	141	32	83
Amount Recovered	`	43	20	42	69-	141	-21	16
Percent Recovery		43%	20%	45%	<b>%</b> 69-	142%	-21%	16%
		154	154	154	164	154	154	154
:	31OCT2:384SB30	121	87	156	262	3 U	09	69.
3/9GLBH-247-H + Spike		278	215	282	309	237	154	165
Amount Recovered		157	129	126	47	234	94	107
reicent necovery		102%	84%	82%	31%	152%	%19	%69

					% Surro	% Surrogate Recovery	
MSL Code	Sponsor ID	Dibenzo[a,h]- anthracene	Benzo[ghi] perylene	d8 Naph- thalene	d10 Acena- phthene	D10- Fluorene	D14 Dibenzo- (a,h)Anthracene
SPIKE RESULTS							
Amount Spiked		303	303	₹	\$	<b>.</b> ₹	¥Z
379GLBR-111-R	220CT5:563SA20	74		33%	72%	<b>65%</b>	91%
379GLBR-111-R + Sp	Spike	404		%29	85%	83%	%56
Amount Recovered	ms .	330	285	¥	¥	₹	<b>A</b> N
Percent Recovery		109%	94%	<b>\frac{\frac{1}{2}}</b>	₹	¥	<b>4 2</b>
Amount Spiked		312	312	ž	<b>Y</b> Z	Ž	
379GLBR-111-R	220CT5:563SA20	42		33%	72%	65%	91%
379GLBR-111-R + Spike DUPLICATE	ike DUPLICATE	506	759	21%	%56	75%	95%
Amount Recovered		432	465	¥	₹	¥	AN.
Percent Recovery		139%	. 149%	ž	<b>\frac{1}{2}</b>	<b>\frac{1}{2}</b>	<b>V</b>
Amount Spiked		86	60	₹	\$	¥	42
379GLBR-247	310CT2:384SB30	32		20%	* %68	55%	<b>%</b> 29%
379GLBR-247 + Spike	•	97	92	20%	45%	28%	93%
Amount Recovered		65		₹	ž	<b>\( \)</b>	<b>A</b> N
Percent Recovery		<b>%99</b>	. 75%	₹	¥	<b>*</b>	NA NA
Amount Spiked		100		<b>≨</b>	Ž	¥	<b>Y</b> Z
379GLBR-247	31OCT2:384SB3O	32	64	20%	. %68	25%	63%
379GLBR-247 + Spike	<ul><li>BUPLICATE</li></ul>	7.8		43%	40%	23%	55%
Amount Recovered		46		¥	¥	Ž	¥
Percent Recovery		46%	-3%	¥	Ž	₹	<b>Y</b> Z
Amount Spiked		154		₹	₹	₹	<b>A</b> Z
379GLBR-247-R	310CT2:384SB30	30		• %1	131%	52%	%19
379GLBR-247-R + Spike	pike	136	142	%19	75%	74%	<b>63%</b>
Amount Recovered		106		¥	¥	ž	<b>V</b>
Percent Recovery		<b>%</b> 69	25%	ž	¥	¥ Y	<b>V</b> N

MSL Code	Sponsor ID	Naph-	Acenaph-	Acenaph-		Dibenzo-	Phenan-	Anthra-	Fluoran-
SPIKE RESULTS					riourene	thiophene	threne	Cene	thene
Amount Spiked 379GLBR-247-R 379GLBR-247-R + Spike DUPLICATE Amount Recovered Percent Recovery	31OCT2:384SB3O ke DUPLICATE	142 455 NA NA	142 39 U 97 97 69%	142 68 U 193 193 136%	142 9 U 79 79	142 21 151 130 92%	142 141 282 141 99%	142 18 129 111	142 171 341 170
Amount Spiked 379GLBR-268 379GLBR-268 + Spike Amount Recovered Percent Recovery	1NOV10:208SB3O	109 81 133 52 48%	109 8 U 61 61	109 15 U 82 82 76%	109 34 112 78 71%	109 74 142 68 62%	109 364 390 26 24%	109 60 101 41	109 763 757 .6
Amount Spiked 379GLBR-268 379GLBR-268 + Spike Amount Recovered Percent Recovery	1NOV10:208SB3O DUPLICATE	96 81 141 59 62%	96 8 U 56 56 58%	96 15 U 80 80 83%	96 34 123 88 92%	96 74 154 80 83%	96 364 444 80 84%	96 60 111 51 53%	96 763 865 102 106%
Amount Spiked 379GLBR-388 379GLBR-388 + Spike Amount Recovered Percent Recovery	21NOV5:107SD10	107 103 186 83 78%	107 24 112 88 82%	107 41# 140 99	107 168 281 113 105%	107 276 352 76	107 1455 1501 D 46 43%	107 267 311 45	107 3825 D 3923 D 98 92%

			Benzo[a]-		Benzo(b)-	Benzo(k)-	Benzo[a]-	Indeno [1,2,3-cd]-	-
MSL Code	Sponsor ID	Pyrene	anthracene	Chrysene	Fluoranthene	Fluoranthene	pyrene	ругеле	
SPIKE RESULTS									
Amount Spiked		142	142	142	142	142	142	142	
379GLBR-247-R	31OCT2:384SB30	121	87	156	262	3 U	09	69	
379GLBR-247-R + Spike DUPLICATE	(e DUPLICATE	270	213	289	303	229	149	163	
Amount Recovered		149	127	132	41	227	68	105	
Percent Recovery		105%	89%	83%	78%	160%	<b>97.9</b>	74%	
Amount Spiked		109	109	109	109		109	109	
379GLBR-268	1NOV10:208SB3O	475	360	562	808		281	249	
379GLBR-268 + Spike		495	395	563	760		264	300	
Amount Recovered		20	35	<b>-</b>	-47		-18	51	
Percent Recovery		18%	32%	*	-43%	• 52%	-16%	47%	
Amount Spiked		96	96	96	96	96	96	96	
379GLBR-268	1NOV10:208SB3O	475	360	562	808	422#	281	249	
379GLBR-268 + Spike DUPLICATE	DUPLICATE	559	435	637	878	206	282	323	
Amount Recovered		84	75	75	72	84	<b>~</b>	74	
Percent Recovery		<b>88</b> %	78%	78%	75%	88%	. %1	11%	
Amount Spiked		107		107		107	107	107	
379GLBR-388	21NOV5:107SD10	2867		2794	٥	<b>∩9</b>	1418#	1386	
379GLBR-388 + Spike		2954 D	1695 D	2921	D 7409	∩ s	1572 #	1655	
Amount Recovered		87		127		5	154	269	
Percent Recovery		81%		119%	-	¥	144%	251%	_

						% Surro	% Surrogate Recovery	
MSL Code	Sponsor ID	Dibenzo[a,h]- anthracene	l]- Benzo[ghi]	<u> </u>	d8 Naph- thalene	d10 Acena-	D10-	D14 Dibenzo-
SPIKE RESULTS								
				٠.				
Amount Spiked		14		8	¥	₹	₹	<b>V</b>
379GLBR-247-R	31OCT2:384SB30	30	0 62	8	• %1	131%	52%	%29
379GLBR-247-R + Spike DUPLICATE	(e DUPLICATE	13		<u>.</u>	• %1	118%	51%	20%
Amount Recovered		10		·	<b>₹</b>	ž	ž	¥N.
Percent Recovery		2		*	¥	<b>₹</b>	ž	<b>A</b> N
Amount Spiked		•					:	•
379GI RB-268	000000000000000000000000000000000000000	- •		<b>D</b>	₹ ;	<b></b>	₹	AN.
31 34LBH-268		<b>0</b> .		₹.	61%	31%	71%	64%
3/9GLBH-268 + Spike		209		9	26%	52%	%89	<b>16%</b>
Amount Recovered		10	1 19	6	ž	¥	ž	YN.
Percent Recovery		85%		• %	<b>\( \)</b>	\$	₹	AN N
Amount Spiked		<b>6</b>		ec ec	NA	<b>8</b>	Y I	
379GLBR-268	1NOV10:208SB3O	10		•	61%	318	7 5	Y Y
379GLBR-268 + Spike	DUPLICATE	222	2 267	7	63%	26%	% % & & & & & & & & & & & & & & & & & &	84% 84%
Amount Recovered		1		*	¥	₹	Y Y	AN AN
Percent Recovery		119%		<b>%</b>	Ž	\$	<b>\S</b>	Ž
Amount Spiked		107		<b>^</b>	Ą	<b>A</b> N	ΨN	
379GLBR-388	21NOV5:107SD10	593			%99	72%	%E6	161%
379GLBR-388 + Spike		. 943	3 1778		71%	72%	85%	167%
Amount Recovered		350			¥	<b>\</b>	¥	₹ V
Percent Recovery		327%	•	• %	¥	<b>Y</b>	ž	Y Z

		Naph-	Acenaph-	Acenaph-		Dibenzo-	Phenan-	Anthra-	Fluoran-
MSL Code	Sponsor ID	thalene	thylene	thene	Flourene	thiophene	threne	cene	thene
SPIKE RESULTS					•				
Amount Spiked		117	117	117	117	117	117	117	117
379GLBR-388	21NOV5:107SD10	103	24	4 - 4	168	276	1455	267	3825 D
379GLBR-388 + Spike DUPLICATE	DUPLICATE	194	126	160	296	370	1503 D	316	3853 D
Amount Recovered		91	101	118	128	95	48	49.	28
Percent Recovery		77%	81%	101%	110%	81%	41%	45%	24%
Amount Spiked		200	200		200	200	200	200	200
379GLBR-388-R	21NOV5:107SD10	187	46 U	_	173	289	1785	483	4220
379GLBR-388-R + Spike	ike	549	470		661	800	2263	915	4951
Amount Recovered		362	470		488	511	478	432	732
Percent Recovery		72%	94%		%86	102%	%96	86%	146%
Amount Spiked		385	385	385	385	385	385	385	385
379GLBR-388-R	21NOV5:107SD10	187	46 U		173	289	1785	483	4220
379GLBR-388-R + Spike	ike DUPLICATE	378	325		511	664	2080	777	4828
Amount Recovered		191	325		338	375	295	294	609
Percent Recovery		20%	84%		88%	%26	77%	<b>16%</b>	158%
REPLICATE ANALYSIS	SII								
379GLBR-182, Rep 1	250CT2:294SB10	27	7.6			=	146	18	274
379GLBR-182, Rep 2	250CT2:294SB10	22	111			18	191	32	356
379GLBR-182, Rep 3	250CT2:294SB10	26	110	1 72#		<b>*</b>	143	29	277
	RSD %	1,8	¥ V			25%	17%	32%	15%
379GLBR-199, Rep 1		62	31	52	74	4	503	91	1123
379GLBR-199, Rep 2	200CT3:573SB20	49	29	42	29	40	424	8	931
379GLBR-199, Rep 3	200CT3:573SB20	59	23	40	61	4	472	66	892
	RSD %	12%	15%	14%	13%	10%	<b>%</b> 6	ž	13%

			75.5						
			Benzolal-		Renzo(h).	Bonzo (k)	Dozofol	onebul	
MSL Code	Sponsor ID	Pyrene	anthracene	Chrysene	Fluoranthene	Fluoranthene	Denzolaj- pyrene	, z, 3-caj- pyrene	
SPIKE RESULTS									
Amount Spiked		117	117	117	117	117	117	•	,
379GLBR-388		2867 D	1597 D		D 6742	3	1418 *	111	
379GLBR-388 + Spike	DUPLICATE	2927 D			7141	E 5 1	1545	1550	o e
Amount Recovered		9	85	131	399	) va	127		
Percent Recovery		21%	73%	112%	341%	¥.	108%	160%	•
Amount Spiked		200	200	200	200	<b>1</b>	ŭ		
379GLBR-388-R	21NOV5:107SD10	3297	2155	3345	5641	200	000	000	1 C
379GLBR-388-R + Spike	ke ke	3889	2583	3543	3969	* 1222 *	1965	114/	
Amount Recovered	•	592	428	198	-1672	2271 #	348	- 0 / -	- LC
Percent Recovery		118%	86%	40%	-334%	454%	70%	111%	, .e
Amount Spiked		385	385	385	382	<b>1</b> 000	285	000	u
379GLBR-388-R	Ξ.	3297	2155	3345	5641	17.0	1616	114	. ^
3/9GLBH-388-R + Spike	( DUPLICATE	3802	2484	3547	3889		1876	1563	
Amount Hecovered		208	329	201	-1752	2005	260	41	
Percent Hecovery		132%	85%	25%	-455%	521%	%29	108%	
REPLICATE ANALYSIS									
379GLBR-182, Rep 1	250CT2:294SB10	173	86	187	243	147	66	7	_
Яер Г	250CT2:294SB10	254	145	217	239	154	26	101	• •
3/9GLBH-182, Hep 3	250CT2:294SB10	196	122	195	231	137	76	60 +	
	RSD %	20%	19%	8%	*	<b>%</b> 9	52%	3,8	
379GLBR-199, Rep 1	200CT3:573SB20	833	376	517	634	16.7	,		
379GLBR-199, Rep 2	200CT3:573SB20	808	000	- 6		/C#	44	355	_
379GLBR-199, Rep 3	20OCT3-573SR2O	9 9	325	5.4	499	378	383	295	
<u>.</u>	/* C3B	7 6	967	410	470	335	343	268	_
	* Och	* 2	12%	12%	16%	16%	13%	15%	

						rus %	% Surrogate Recovery	
MSL Code	Sponsor ID	Dibenzo[a,h]- anthracene	Benzo[ghi] perylene		d8 Naph- thalene	d10 Acena- phthene	D10- Fluorene	D14 Dibenzo-
SPIKE RESULTS	-							
Amount Spiked		117	117		¥	₹	\$	<b>V</b>
379GLBR-388	21NOV5:107SD10	593	1538		%99	72%	93%	161%
379GLBR-388 + Spike	DUPLICATE	914	1700		63%	<b>%</b> 69	87%	154% •
Amount Recovered		322	162		Ž	₹	¥	<b>A</b> N
Percent Recovery		275%	138%		₹	<b>A</b> Z	¥	¥Z
Amount Spiked		200	200		¥	¥	Ž	<b>4</b> 2
379GLBR-388-R	21NOV5:107SD10	521	1273		72%	101%	85%	103%
379GLBR-388-R + Spike	k⊕	1067	1748	•	<i>1</i> 1%	91%	95%	109%
Amount Recovered		546	476		¥	₹	¥	<b>A</b> N
Percent Recovery		109%	%56		¥	₹	\$	¥
Amount Spiked		385	385		\$	¥	<b>A</b>	<b>A</b> N
379GLBR-388-R	Σ.	521	1273		72%	101%	85%	103%
379GLBR-388-R + Spike	(e DUPLICATE	952	1657		63%	81%	83%	108%
Amount Recovered		431	384		₹	<b>₹</b>	₹	Ž
Percent Recovery	• •	112%	100%		<b>\( \)</b>	<b>V</b>	<b>\frac{1}{2}</b>	NA
REPLICATE ANALYSIS	<b>6</b>							
379GLBR-182, Rep 1	250CT2:294SB10	48	06		62%	45%	78%	%68
Rep	250CT2:294SB10	51	66		47%	43%	64%	73%
3/9GLBH-182, Rep 3	250CT2:294SB10		96		%99	62%	78%	81%
	RSD %	**	% %		Y Y	¥	<b>V</b>	NA
379GLBR-199, Rep 1	200CT3:573SB20	130	353		87%	73%	94%	105%
Rep	200CT3:573SB20	106	291		74%	<b>62%</b>	78%	87%
379GLBR-199, Rep 3	200CT3:573SB20	96	253		%02	61%	78%	89%
	RSD %	16%	17%		<b>4</b>	¥	Y Y	Y.

#### PAH ANALYSIS IN SEDIMENT SAMPLES BUFFALO RIVER PILOT PROJECT (#378)

MSL Code	Sponsor ID	Naph- thalene	Acenaph- thylene	Acenaph- thene	Flourene	Dibenzo- thiophene	Phenan- threne	Anthra-	Fluoran- thene
REPLICATE ANALYSIS	ဟ							v	
379GLBR-18, Rep 1	070CT1:331SCO	147	99	92	147	105	923	264	1938
379GLBR-18, Hep 2	0/OC11:331SCO	9 <del>.</del>	4 1	29	95	7.5	615	167	1343
System-16, nep 3	0.0011331500	125	23	91	131	100	835	237	1793
	% OSH	. %22	73%	17%	21%	17%	20%	23%	18%
379GLBR-323, Rep 1	19NOV4:504SC2O	36	7 U	. 12 U	10 U		128	20	. 267
379GLBD 323, Rep 2	19NOV4:504SC20	<del>.</del> .	10	10 C	13	28	174	28	379
3/ 3/2/ DE 13/23, UBP 3	USINOVA:SU4SCZO	E 3	0 Z	11 U	∩ 6		125	20	265
	R OCH	*	¥	Y X	¥ X	12%	19%	21%	22%
379GLBR-376, Rep 1	21NOV12:003SD10	61	34	7	104	77	703	173	1426
3/90LBH-3/6, Hep 2	21NOV12:003SD10	33	31	46	0.2	22	520	130	1067
Staden-ste, nep s	O10350035010	68		54	4	52	525	132	1117
	% OSH	34%	<b>%</b>	22%	21%	15%	18%	17%	16%

Recoveries outside of QC limits.

U - Detected at or below detection limit.

R - Rerun samples.

D = Sample diluted 1:10.

E - Value out of calibration range.

<sup># =</sup> Ion ratio out of specification.

<sup>(1) =</sup> HS-2 is not certified for PAHs. However, RSD values give an indication of relative precision of PAH measurements between batches.

NA - Not applicable/analyzed.

RSD% - Relative Standard Deviation

(Concentrations in ng/g)

Indeno [1,2,3-cd]- pyrene	621	438	583	18%	137	180	141	16%	451	376	374	<b>1</b> %
Benzo[a]-   pyrene	912	601	852	21%	131	189	123	24%	632	485	475	17%
Benzo(k)- Fluoranthene	777	513	695	20%	4	229	174	27% •	533	448	443	* = %
Benzo(b)- Fluoranthene	1039	166	1033	16%	484	361	308	24%	805	652	657	12%
Chrysene	957	664	893	18%	238	296	240	13%	656	543	548	<b>= * * * * * * * * * *</b>
Benzo[a]- anthracene	785	528	747	20%	131	178	126	20%	543	408	422	16%
Pyrene	1554	1077	1436	18%	189	277	180	25%	1078	824	860	15%
Sponsor ID	07OCT1:331SCO	07OCT1:331SCO	070CT1:331SCO	RSD %	19NOV4:504SC2O	19NOV4:504SC2O	19NOV4:504SC2O	RSD %	21NOV12:003SD10	21NOV12:003SD10	21NOV12:003SD10	RSD %
MSL Code	379GLBR-18, Rep 1	379GLBR-18, Rep 2	379GLBR-18, Rep 3		379GLBR-323, Rep 1	379GLBR-323, Rep 2	379GLBR-323, Rep 3		379GLBR-376, Rep 1	379GLBR-376, Rep 2	379GLBR-376, Rep 3	

- Recoveries outside of QC limits.

U - Detected at or below detection limit.

R - Rerun samples.

D - Sample diluted 1:10.

E - Value out of calibration range.

# - Ion ratio out of specification.

(1) - HS-2 is not certified for PAHs. However, RSD values give an indication

of relative precision of PAH measurements between batches.

NA - Not applicable/analyzed.

RSD% - Relative Standard Deviation

#### PAH ANALYSIS IN SEDIMENT SAMPLES BUFFALO RIVER PILOT PROJECT (#379)

					% Surr	% Surrogate Recovery	
MSL Code	Sponsor ID	Dibenzo(a,h)- anthracene	Benzo[ghi] perylene	d8 Naph- thalene	d10 Acena- phthene	D10- Fluorene	D14 Dibenzo-
REPLICATE ANALYSIS	•			·			
379GLBR-18, Rep 1 379GLBR-18, Rep 2	070CT1:331SC0	251	602	64%	29%	89%	123%
379GLBR-18, Rep 3	07OCT1:331SCO RSD %	241	505 22% •	72% 72% NA	61% 888 88	84% 96% NA	121% • 133% • NA
379GLBR-323, Rep 1 379GLBR-323, Rep 2 379GLBR-323, Rep 3	19NOV4:504SC2O 19NOV4:504SC2O 19NOV4:504SC2O	54 71 55 15%	144 189 146 16%	86% 84% 83%	77% 76% 74% NA	89% 91% 88%	96% 101% 99%
379GLBR-376, Rep 1 379GLBR-376, Rep 2 379GLBR-376, Rep 3	21NOV12:003SD10 21NOV12:003SD10 21NOV12:003SD10 RSD %	164 136 134	434 363 361	50% 18% • 38% •	54% 42% NA	94% 77% 80% NA	112% 106% 95% NA

<sup>-</sup> Recoveries outside of QC limits.

U - Detected at or below detection limit.

R = Rerun samples.

D = Sample diluted 1:10.

E - Value out of calibration range.

<sup># =</sup> lon ratio out of specification.

<sup>(1) -</sup> HS-2 is not certified for PAHs. However, RSD values give an indication of relative precision of PAH measurements between batches.

NA = Not applicable/analyzed. RSD% = Relative Standard Deviation

				Concentrations in ng/L	is in ng/L		% Surrogate Recovery	Recovery
MSL Code	Dii.	Sponsor ID	Sample Amount (L)	Aroclor 1242/1248	Aroclor 1254	Aroclor 1260	Tetrachloro- m-Xylene	Octachloro- naphthalene
		BIN A						
379GLBR-97	(1:10)	210CT6:1810LA10	0.810	21,111 D	500 U	500 U	36.1%	. 52 7%
379GLBR-97 ~	•	210CT6:2010L	0.800	26,368	20 U	50 U		38.6%
379GLBR-97 ~	(1:10)		0.800	22,742 D	500 U	500 U	_	77.4%
379GLBR-128	(1:10)		0.720	24,698 D(a)	200 U	200 U	103.1%	33.3%
379GLBR-132	(1:10)	230CT5:2010LA20	0.675	0 068'09	5,294 E	500 U	23.0%	. %9.96
379GLBR-160	(1:10)	250CT10:1810LA30	0.700	21,020 D	200 U	500 U	113.6%	77.9%
379GLBR-161	(1:10)	250CT10:1910LA30	0.760	33'666 D	200 U	500 U	135.7%	68 5%
379GLBR-164	(1:10)		0.650	69,074 D	200 U	200 O	%2.69	59.2%
379GLBR-204		300CT4:206LA30	0.800	200 U	20 U	20 U	76.1%	105.0%
		e Nie						
379GLBR-187	(1:10)		0.750	27,605 D	500 U	500 U	103.0%	83.3%
379GLBR-226	(1:10)		0.850	2,000 U	200 U	500 U	54.6%	33.1%
379GLBR-227	(1:10)		0.825	2,000 U	200 U	500 U	%9.99	45.4%
379GLBR-252	(1:10)		0.825	2,000 U	200 U	500 U	113.5%	58.4%
379GLBR-253	(1:10)		0.775	2,000 U	200 U	500 U	92.3%	20.0%
379GLBR-256	(1:10)		0.750	8,107 D	200 U	500 U	72.5%	85.5%
379GLBR-257	(1:10)	31OCT3:0010LB3O	0.650	16,922 D	500 U	200 U	%2.69	47.9%
		BINC	•					
379GLBR-286	(1:10)	•	0.775	25,956 D	200 U	500 U	116.9%	47.9%
379GLBR-326	(1:10)		0.800	39,269 D	200 U	500 U	65.8%	44.5%
379GLBR-331			0.650	17,890 D	200 U	500 U	61.8%	54.9%
	(1:10)	19NOV5:0510LC2O	0.785	11,157 D	200 U	500 U	63.1%	58.3%
3/9GLBH-331 DUP 2			0.800	8,028 D	200 U	200 U	56.2%	53.8%
3/9GLBH-361			0.800	200 U	20 N	50 U	38.8%	52.8%
3/9GLBH-366	(1:10)		0.800		200 U	200 U		20.3%
3/9GLBH-3/0	(01:10	20NOV3:0110LC3O	0.726	19,471 D	200 U	500 U	42.6%	21.8%
				Page 1				

Concentrations in ng/L % Surrogate Recovery	Aroclor Tet		500 U 500 U 45.7% 51.3% 500 U 500 U 49.4% 27.3%		%65 . %8% 105 nos n	J 50 U 50 U 62.4% 96.4%		7,143 NS NA NA S.294 E NS 53.0% 36.6% • 13,287 NS 43.6% 49.5% 7.993 NS NS NA
Concent	Sample Aroclor Amount (L) 1242/1248		0.757 5.304 D 0.705 7,193 D		0.825 200 U	0.500 200 U		3 3 3 S
	MSL Code Dil. Sponsor ID	BIN D	379GLBR-398 (1:10) 21NOV3:2610LD1O 379GLBR-404 (1:10) 21NOV4:169LD1O	DILUTION WATER	379GLBR-275 6NOV12:003LO	379GLBR METHOD BLANK	MATRIX SPIKE RESULTS	Amount Spiked 380GLBR-132 (1:10) 23OCT5:2010LA2O 380GLBR-132 + Spike Amount Recovered

				Concentrations in ng/L	ins in ng/L		% Surrogate Recovery	3 Recovery
			Sample	Aroclor	Aroclor	Aroclor	Aroclor Tetrachloro-	Octachloro-
MSL Code	Dil.	Dit. Sponsor ID	Amount (L)	Amount (L) 1242/1248	1254	1260	m-Xylene	naphthalene
REPLICATE ANALYSIS	ري دن							
379GLBR-331	(1:10)	(1:10) 19NOV5:0510LC2O		17,890 D	200 U	500 U	61.8%	54.9%
379GLBR-331 DUP 1 (1:10) 19NOV5:0510LC2	(1:10)	19NOV5:0510LC2O		11,157 D	200 U	500 U	63.1%	58.3%
379GLBR-331 DUP 2 (1:10) 19NOV5:0510LC2O	(1:10)	19NOV5:0510LC2O		8,028 D	200 U	200 U	56.2%	53.8%
			RSD%	41%	Y Y	Y V	NA	<b>V</b>

Field replicate.

U = Not detected at detection limit shown.

D = Results from diluted sample extract.

(a) = Aroclor quantified with one peak; other peaks may have been present, but not quantifiable.

E = Estimated/most likely due to residual peaks of primary aroclor.

NS = Not spiked.

NA = Not applicable.

• = Recoveries were outside laboratory control limts (40-120%).

\*\* = RSD exceeded QC limit of 20%.

			•	Con	centrations in	Concentrations in ng/g dry weight	ht	% Surrogate Recovery	3 Recovery	
MSL Code	Sponsor ID	Extraction Date	Dry Wt. (%)	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Tetrachloro- m-Xylene	Octachloro- naphthalene	
	BIN A	_				15				
379GLBR-58	09OCT11:382SA2O	2/19/92	60.44	50 11		9511	11 30	00	• 60 00	
379GLBR-104	220CT11:317SA10	2/19/92	65,53	50 U	0	25.0	25.0	65.1%	135.8%	
379GLBR-107	220CT11:378SA10	2/19/92	97.72	50 U		25 U	25 U	70.8%	108.2%	
379GLBR-108	220CT4:203SA20	2/19/92	52.78	50 U	50 U	25 U		71.2%	106.5%	
379GLBR-123	230CT4:274SA20	2/19/92	99.79	90 O	50 U	25 U	25 U	%2.56	143.2%	
379GLBR-136	240CT10:457SA20	2/19/92	90.15	50 U	50 U	25 U	25 U	58.9%	103 0%	
379GLBR-139	24OCT10:508SA2O	2/24/92	77.20	0 0 O	009	35 U	35 U	84.5%	133.6%	
379GLBR-145	240CT6:203SA3O	2/24/92	56.46	O 09	0 0 O	120	35 U	98.5%	142.6%	
379GLBR-153	250CT9:214SA30	2/24/92	99.12	009	O 09	35 U	35 U	81.9%	141.6%	
3/9GLBH-166	250CT9:307SA3O	2/24/92	91.48	O 09	201	201	35 U	91.5%	125.9%	
3/9GLBH-167	250CT9:368SA30	2/24/92	99.41	O 09	0 0 0 o	67	35 U	87.1%	124.2%	
	BIN B		<del>-</del>							
379GLBR-65	09OCT9:542SB1O	2/19/92	62.26	50 11	50.11	95 II		707.07	•	
379GLBR-174	250CT12:153SB10	2/24/92	62.01	0 0 0 0	1040	0 0	2 2 2 2	75.0%	149.2%	
379GLBR-181	250CT2:254SB10	2/24/92	99.00	000	09	9 6		79.6%	125.4%	
379GLBR-193	250CT3:527SB10	2/24/92	95.93	009	327	262		00.9% 00.6%	100.7%	
379GLBR-196	250CT3:578SB10	2/24/92	99.10	0 0 9	81	75		105.0%	169.1%	
Яөр		2/24/92	63.20	0 09	350	37.1	35 U	73.3%	138 0%	
Rep G		2/24/92	63.20	09	92	96	35 U	68.5%	125.7%	
379GLBH-199, Hep 3	300CT3:573SB20	2/24/92	63.20	0 0 0	0 0 O	48	35 U	96.1%	169.1%	
3/9GLBH-210	310C19:027SB20	2/24/92	87.81	0 09	319	158	35 U	117.1%	145.8%	
379GLBR-213	310C19:0/8SB20	2/24/92	99.79	0 09	0 0 O	35 U	35 U	112.5%	222.2%	
370GLBB 243	310C19:244SB20	2/24/92	99.81	O 09	0 0 9	35 U	35 U	65.4%	167.6%	
379G1 BB.249	310C111:5035B30	2/24/92	62.88	O 09	120	6	35 U	%9'86	164.5%	
379GI BB.268	310C12.3345B30	2/24/92	99.60	0 0 0	09 09	35 U	35 U	70.0%	182.4%	
379G1 BB.260	1NOV10:2085B3O	2/24/92	99.60	O 09	09 -	35 U	35 U	%2'99	152.9%	
	11VOV 10.137 SESO	2/24/92	97.78	0 0 0	O 09	176	35 U	100.3%	145.0% *	

				Con	centrations in	Concentrations in ng/g dry weight	əight	% Surrogate Recovery	Recovery
		Extraction	Dry Wt.		Aroclor	Aroclor	0 1	Tetrachloro-	Octachloro-
MSL Code	Sponsor ID	Date	(%)	1242	1248	1254	1260	m-Xylene	naphthalene
		r							
	BINC								
369GLBR-73	09OCT4:562SC1O	2/19/92	62.20	50 U	50 U	113	25 U	87.1%	125.3% *
379GLBR-282	18NOV3:503SC1O	2/24/92	62.71	0 0 0	232	35 U	35 U	%0.96	175.7%
379GLBR-288	18NOV6:1510LC10	2/24/92	73.20	09	975	35 U	35 U	104.9%	137.4% •
379GLBR-302	19NOV8:594SC1O	3/4/92	99.66	009	09	17	35 U	103.1%	115.4%
379GLBR-307	19NOV9:23ISC10	3/4/92	98.79	O 09	09	35 U	35 U	71.5%	122.0%
379GLBR-311	19NOV11:303SC2O	3/4/92	69.87	O 09	209	35 U	35 U		119.8%
379GLBR-323, Rep 1	19NOV4:504SC2O	3/4/92	99.79	09 O	133	35 U			88.5%
379GLBR-323, Rep 2	19NOV4:504SC2O	3/4/92	99.79	0 0 9	119	35 U	35 U	101.0%	96.4%
	19NOV4:504SC2O	3/4/92	99.79	0 0 9	114	35 U	35 U	95.3%	136.7%
379GLBR-337	20NOV8:157SC20	3/4/92	95.62	09 09	284	35 U	35 U	102.6%	188.1%
379GLBR-340	20NOV11:443SC3O	3/4/92	55.58	09 n	163	35 U	35 U	67.5%	119.3%
379GLBR-350	20NOV3:154SC3O	3/4/92	95.97	O 09	109	35 U	35 U	72.5%	. 143.8%
379GLBR-357	20NOV3:337SC30	3/4/92	77.29	09 O	738	500 U	. 35 U	125.7%	90.1%
379GLBR-360	20NOV3:278SC3O	3/4/92	99.58	09 n	09	35 U	35 U	75.8%	153.3%
		_							
	BIND								
379GLBR-46	08OCT5:132SD3O		60.26	50 U	50 U	25 U	25 U	76.8%	130.3%
379GLBR-378	21NOV1:353SD10	3/4/92	57.63	O 09	320	35 U	35 U	71.7%	199.9%
379GLBR-384	21NOV5:073SD10	3/4/92	100.00	0 0 O	251	35 U	35 U	%2.96	104.6%
379GLBR-388	21NOV5:107SD10	3/4/92	93.10	O 09	674	35 U	35 U	103.6%	129.0%
379GLBR-395	21NOV5:224D10	3/4/92	100.00	09	O 09	35 U	35 U	86.4%	169.3%
Blank-1		2/19/92	ž	50 U	50 U	25 U	25 U	46.1%	86.5%
Blank-2		2/24/92	ž	O 09	0 0 O	35 U	35 U	77.7%	146.6%
Blank-3		3/4/92	ž	O 09	O 09	32 N	35 U	%E'98	126.9%

				Con	centrations in	Concentrations in ng/g dry weight	eig <b>ht</b>	% Surrogate Recovery	Recovery
MSL Code Sp	Sponsor ID	Extraction Date	Dry Wt. (%)	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor	Tetrachloro-	Octachloro-
CTANDADO OCCUPACO							2021	Allei Avalli	паришанене
STANDARD REFERENCE MATERIAL	MAIERIAL								
		2/19/92	¥	200	50 U	262	25 U	67.6%	104 20%
		2/24/92	₹	09	0 0 9	261	35 U		114.4%
SHM-3 HS-2		3/4/92	¥	0 0 9	0 0 O	381	35 U		180 9%
	certified		¥	2	2	111.8	2	₹	R N
SPIKE RESULTS	•njeA		ş	2	2	±2.5	2	¥.	₹
			•					•	
Amount Spiked				2	9	2500	92	₹	AN A
Amount Doggest	JOU J			92	2	3173	92	%8.09	132.9%
Amount Recovered				2	22	3173	92	ž	AN A
ב פוכפווו עפכסאפול				<b>2</b>	22	127%	92	ž	Ž
Amount Spiked			,75 K.,	82	2	2500	92	<b>V</b> Z	ĄN
379GI BD. DISH 9 Called		3/4/92		<del>2</del>	2	35 U	2	86.3%	126 9%
	100			22	9	2767	92	78.2%	96.2%
Percent Recovery				2	9	2767	92	¥	<b>\</b>
Alekson Heads				92	2	111%	\$2	¥	¥
Amount Spiked				22	92	2500	9	<b>V</b>	Ν
379GI BB.Block 3. Collection	9	3/4/92		2	9	35 U	92	86.3%	126.9%
Amount Becovered				2	<u>\$</u>	5149	92	73.8%	243.0%
Percent Recovery				<b>9</b>	2	5149	92	¥	Ž
				<del>2</del>	2	506%	22	<b>₹</b>	¥

				Co	oncontrations	Concentrations in ng/g dry weight	/eight	% Surrogate Recovery	э Весоивгу
		Extraction	Dry Wit.	Aroclor	Aroclor	Aroclor	Aroclor	Tetrachloro-	Octachloro-
MSL Code	Sponsor ID	Date	(%)	1242	1248	1254	1260	m-Xylene	naphthalene
Amount Sniked				¥	¥	7.73	¥	4.4	2
379GLBR-46	08OCT5:132SD3O	2/19/92	60.26	9	2 2	25.1	2 4	76 8%	130 3%
379GLBR-46 + Spike				2	2	455	2	83.0%	e Z
Amount Recovered				92	92	455	22	Ž	¥.
Percent Recovery	•			22	92	85%	2	₹	¥
•				!				;	
Amount Spiked				2	9	714	2	≨	₹
379GLBR-46	08OCT5:132SD3O	2/19/92	60.26	2	92	25 U	2	76.8%	130.3%
•	DUP			2	92	517	92	85.0%	126.8%
Amount Recovered				2	92	517	92	¥	¥
Percent Recovery				2	92	72%	9	¥	¥
Amount Spiked				2	92	547	9	Ž	Ą
379GLBR-268	1NOV10:208SB3O	2/24/92	99.60	92	92	62	2	66.7%	152.9%
379GLBR-268 + Spike				2	<u>9</u>	732	2	63.6%	137.6%
Amount Recovered				92	92	670	2	₹	¥
Percent Recovery				<u>\$</u>	92	122%	22	₹	¥
Amount Spiked				Q.	<u>u</u>	007	9		
				2	3	204	2	Ž	≨
3/9GLBH-268		2/24/92	99.60	22	<u>8</u>	62	9	%2.99	152.9%
3/9GLBH-268 + Spike	DUP			<del>2</del> 2	<del>2</del>	969	92	75.7%	138.2%
Amount Recovered				92	92	634	92	¥	¥
Percent Recovery				\$	\$	132%	22	¥	₹

			•	Š	Concentrations in ng/g dry weight	in ng/q dry	weight	Surrocate Document	000000
		Extraction	Dry Wt.	Aroclor	Aroclor	Aroclor	Aroclor	Tetrachloro-	Octachloro-
MSL Code	Sponsor ID	Date	(%)	1242	1248	1254	1260	m-Xylene	naphthalene
Amount Spiked				<u>9</u>	2	534	2	¥2	₹N
379GLBR-388	21NOV5:107SD10	3/4/92	93.10	9	2	674	92	103.6%	129 0%
379GLBR-388 + Spike	_			9	2	1157	92	115.8%	106.4%
Amount Recovered				92	2	483	92	¥	NA NA
Percent Recovery				2	92	<b>%</b> 06	92	2	<b>\frac{8}{2}</b>
Amount Coiked				<b>S</b>	<u> </u>	1		•	
Allouin Spined				2	2	585	9	¥	ž
3/90LBH-388		3/4/92	93.10	2	9	674	SZ	103.6%	129.0%
3/9GLBH-388 + Spike	לם ה			2	9	1141	9	115.0%	70 0%
Amount Hecovered				2	9	467	92	AN	S O O
Percent Recovery				\$	92	%08	8	₹	≨ ₹
REPLICATE ANALYSIS	S.								
379GLBR-199, Rep 1	30OCT3:573SB2O	2/24/92	63.20	N 09	350	371	35.	90 00	
379GLBR-199, Rep 2	30OCT3:573SB2O	2/24/92	63.20	O 09	92	9	2 S S S S S S S S S S S S S S S S S S S	60.5%	138.9%
379GLBR-199, Rep 3	30OCT3:573SB2O	2/24/92	63.20	09	U 09	8 4	35 U	96.3%	125.7%
•		RSD %		Y Y	117%	* %68	N N	NA NA	
379GLBR-323, Rep 1	19NOV4:504SC2O	3/4/92	99.79	09	133	63	35.1	07.2%	č
379GLBR-323, Rep 2	19NOV4:504SC2O	3/4/92	99.79	09	119	51	35 U	101 0%	96.5%
379GLBR-323, Rep 3	19NOV4:504SC2O	3/4/92	99.79	0 0 O	114	51	35 U		126 76/
		RSD%		Y V	%8 8	13%	NA	Y N	« Y.

U = Not detected at detection limit shown.

J = Detected below detection limit.

D = Detected Aroclor, but undetected pattern due to low levels.

<sup>• =</sup> Outside of QC limits. • = Matrix interference.

NC - Not certified. NS = Not Spiked.

NA = Not Applicable.

RSD % = Relative Standard Deviation.

		1		(cor	ncentrations i	(concentrations in ng/g dry weight)	eight)	% Surroga	% Surrogate Recovery
MSL Code	Sponsor ID	Extraction Date	Dry Wt. (%)	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor	Tetrachloro- m-Xylana	Octachloro-
יין אין מטויסטנט									
379GLBH-13, Hep 1	0/OC11:212SCO	10/10/91	29.0	73 E	217	3 6 E	20 U	53.9%	85.1%
379GLBR-15, Hep 2	0/OC11:212SCO	10/10/91	29.0		236	108 E	20 U	26.8%	89.2%
379GI BB-17	0/0C11:2125C0		29.0	73 E	239	20 U	. 20 U	26.9%	95.9%
379GI BB-24	070CT12:091SAO	_	57.9	20 N	85	20 U	20 U	%6.09	93.2%
379GLBB-21	0/OC112:5315BO	•	. 55.2	20 N	20 U	20 U	20 0	%6.99	107.3%
77-U20-10	0/0011:521500	10/10/91	58.7	20 U	179 E	202	20 U	%2'99	100.6%
Blank		10/10/91	¥	20 U	20 U	20 U	20 U	82.9%	127.4% •
STANDARD REFERENCE MATRIAL	NCE MATRIAL								
SRM-1 (1941)	certified value	10/10/91	₹	20 U	395	315	153	77.9%	123.1%
SPIKE RESULTS				<b>?</b>	₹	<b>≩</b>	2	₹	₹
Amount Spiked 379GLBR-22	07OCT1-5216DO			9	2	880	<b>9</b>	¥	<b>≨</b>
E79GLBR-22 + Snike		18/01/01	28.7	<u>9</u>	92	202	92	%2'99	100.6%
Amount Recovered				<b>9</b>	\$2	689	22	76.7%	121.3% •
Percent Recovered				9 2	<u>\$</u>	487	<u>\$</u>	¥	₹
				92	2	22%	22	¥	₹

			•	(co	ncentrations i	(concentrations in ng/g dry weight)	/eight)	% Surroga	% Surrogate Becovery
MSL Code	Sponsor ID	Extraction Date	Dry Wt. (%)	Aroclor 1242	Aroclor 1248	Aroclor 1254	Aroclor 1260	Aroclor Tetrachloro-	Octachioro-
REPLICATE ANALYSIS	SIS								All Brown
379GLBR-15, Rep 1 379GLBR-15, Rep 2 379GLBR-15, Rep 3	07OCT1:212SCO 07OCT1:212SCO 07OCT1:212SCO	10/10/91 10/10/91 10/10/91 RSD %	59.0 59.0 59.0	73 E 79 E 73 E 5%	217 236 239 5%	99 E 108 E 20 U 9%	20 U 20 U 20 U NA	53.9% 56.9% 56.9%	85.1% 89.2% 95.9% NA

U = Not detected at detection limit shown.

E = Estimated/most likely due to residual peaks of primary aroctor.

\* = Outside of taboratory control limits of 40-120%.

NA = Not Applicable.

NS = Not Spiked. NC = Not certified.

RSD % = Relative Standard Deviation.